STORMWATER CALCULATIONS

401 WEST GANNON AVENUE

Zebulon, North Carolina



Prepared By:

The Nau Company, PLLC
PO Box 810
Rolesville, North Carolina, 27571
(919) 625-3090
jeakins@thenauco.com
NCBELS License # P-0751

INTRODUCTION AND GENERAL INFORMATION

This report presents calculations for the stormwater impacts for the proposed 401 West Gannon Avenue project located at the intersection of West Gannon Avenue and North Rotary Drive in Zebulon, North Carolina.

The proposed development is comprised of approximately 0.99 acres of land and is currently vacant. At full build out the project will consist of 11 condominium units with infrastructure to support the proposed development as well as one SCM to meet the Town's stormwater requirements.

REQUIREMENTS

Sections 151.35.D and 151.36 of the Zebulon Code of Ordinances specify the stormwater requirements for high density development. The relevant requirements of the Code are summarized below:

- The measures shall control and treat runoff from the first inch of rain. Runoff volume drawdown time shall be a minimum of 48 hours, but not more than 120 hours.
- All structural stormwater treatment systems used to meet these requirements shall be designed to have a minimum of 85% average annual removal for total suspended solids (TSS).
- All development and redevelopment projects shall provide permanent on-site BMPs to lower
 the nitrogen export amounts as part of the stormwater management plan and accompany the
 land-disturbing plan submittal. BMPs are to be in accordance with and as specified in the Design
 Manual.
- Structural and non-structural BMPs shall be used to ensure there is no net increase in peak flow leaving the site from the pre-development conditions for the one-year, 24-hour storm. Runoff volume drawdown time shall be a minimum of 48 hours, but not more than 120 hours.
- The downstream impact analysis must be performed in accordance with the "10% rule"

METHODOLOGY

Drainage Areas and SCS Curve Numbers

Drainage areas were delineated based on proposed and existing topography using CAD software. Land use types were measured using CAD software and SCS curve numbers were applied to each land use type within the drainage area to calculate a weighted, composite SCS Curve Number. Curve numbers for the various land use types were taken from NRCS TR-55 and are included as an appendix to this report.

Drainage areas, curve number, times of concentration as well as design pond contour data for the overall drainage area to the analysis point and SCM bypass are the same as those presented in the design calculations for the preliminary plat.

Times of Concentration

The minimum time of concentration used for calculation of peak flows was 5 minutes. For times of concentration more than 5 minutes, a simplified TR-55 method was used. The simplified method calculates the time of concentration only using sheet flow time and channel flow time — shallow concentrated flow time is disregarded. Since channel dimensions vary along the channel flow path,

channel parameters were selected for the entire length of channel flow that yield a flow velocity of approximately 4.5 feet per second. A flow velocity of 4.5 feet per second is greater than or equal to actual flow velocities expected in the pipes or open channels along the flow path and therefore will yield a runoff higher that what would be expected at the analysis point.

Runoff and Pond Routing

Runoff flowrates and volumes for the proposed SCM were calculated using the Hydrology Studio software program. The software utilizes the SCS Methodology to determine peak flow rates and performs routing calculations to determine detention results by the Storage-Indication method.

Rainfall Depths

The following rainfall depths used in the calculations for this report were taken from the NOAA Precipitation Frequency Data Server (PFDS). A printout of this rainfall data is included as an appendix to this report.

Rainfall event	Rainfall Depth (inches)
1-year, 24-hour	2.83
2-year, 24-hour	3.42
10-year, 24-hour	4.94
25-year, 24-hour	5.84
100-year, 24-hour	7.27

Notes:

1. Only the 1-year and 10-year rainfall events were analyzed for runoff flowrates. Additional rainfall events were used to check for pond overtopping.

Pre-Development and Post-Development Drainage Areas

Drainage area maps showing the pre-development and post-development drainage areas are included as an attachment to this report. Note that the drainage areas are based on GIS topography.

RESULTS

Peak Flow Attenuation

Peak flow attenuation is required for the 1-year, 24-hour storm and 10-year 24-hour storm. The tables below summarize the pre-development and post-development data for these design storms. Detailed routing information can be found in the appendix to this report.

Project Site					
Development condition	Drainage area (acres)	SCS CN	Time of concentration (min(Q(1) cfs	Q10 (cfs)
Pre-Development discharge	0.99	61	5.0	0.4	2.4
Post-Development SCM bypass	0.31	68	5.0	0.3	1.1
Post-Development to SCM	0.69	80	5.0	1.4	3.6
Post-Development SCM outflow				0.1	0.1
Post-Development discharge				0.3	1.2

SCM Surface Area

The required bioretention surface area was determined based on a maximum ponding depth of 12 inches and a volume determined by the simple method. The SCM surface area data is summarized in the table below.

Drainage area	0.69 acres
Impervious area	0.36 acres
Impervious percentage	52.3%
Runoff volume	1,298 CF
Ponding depth	12 inches
Required bioretention area	1,298 SF
Bioretention area provided	1,603 SF

SCM surface area calculations are included in the Appendix to this report.

Riser Anti-Flotation Device

An anti-flotation device was designed to counteract the buoyant forces on the pond riser. The riser anti-flotation block was sized to provide a factor of safety for buoyancy of at least 1.5. Calculations for the anti-flotation block are included in the Appendix to the report.

Nutrient Loading

Nutrient loading calculations were performed with the SNAP Tool v4.2, which is provided by NCDEQ. The output from this tool is included in the Appendix to this report.

The weighted average calculated by the spreadsheet for nutrient loading is summarized in the table below:

Post-BMP TN Loading	2.00 lb/ac/yr
Post-BMP TP Loading	0.37 lb/ac/yr

CONCLUSION

Based on the results of this analysis, we believe that the Town of Zebulon requirements will be met for the proposed development. Additional details can be found in the Appendix.

APPENDICES

Appendix A – Drainage Area Maps

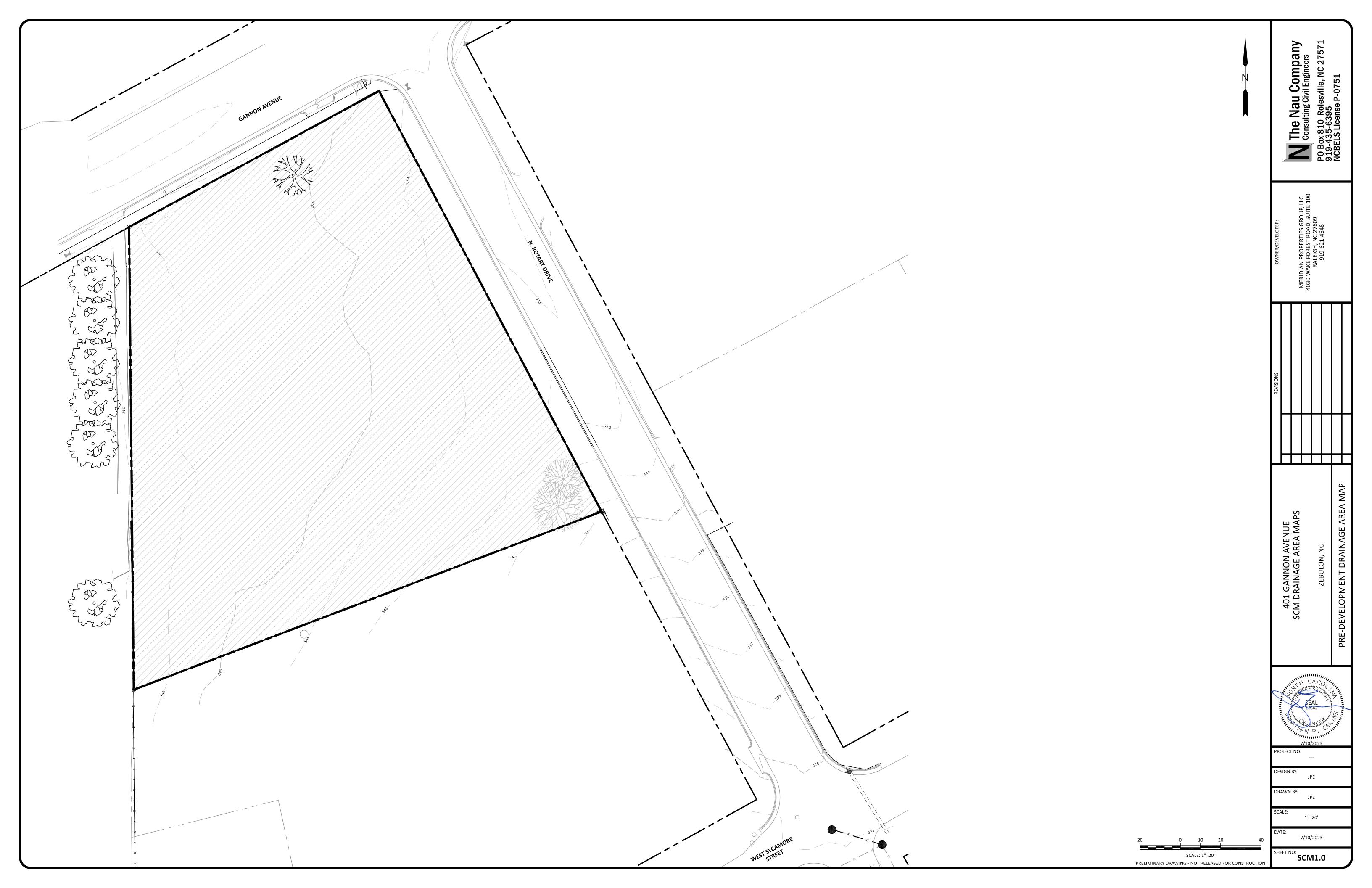
Appendix B – Hydrology Studio Output

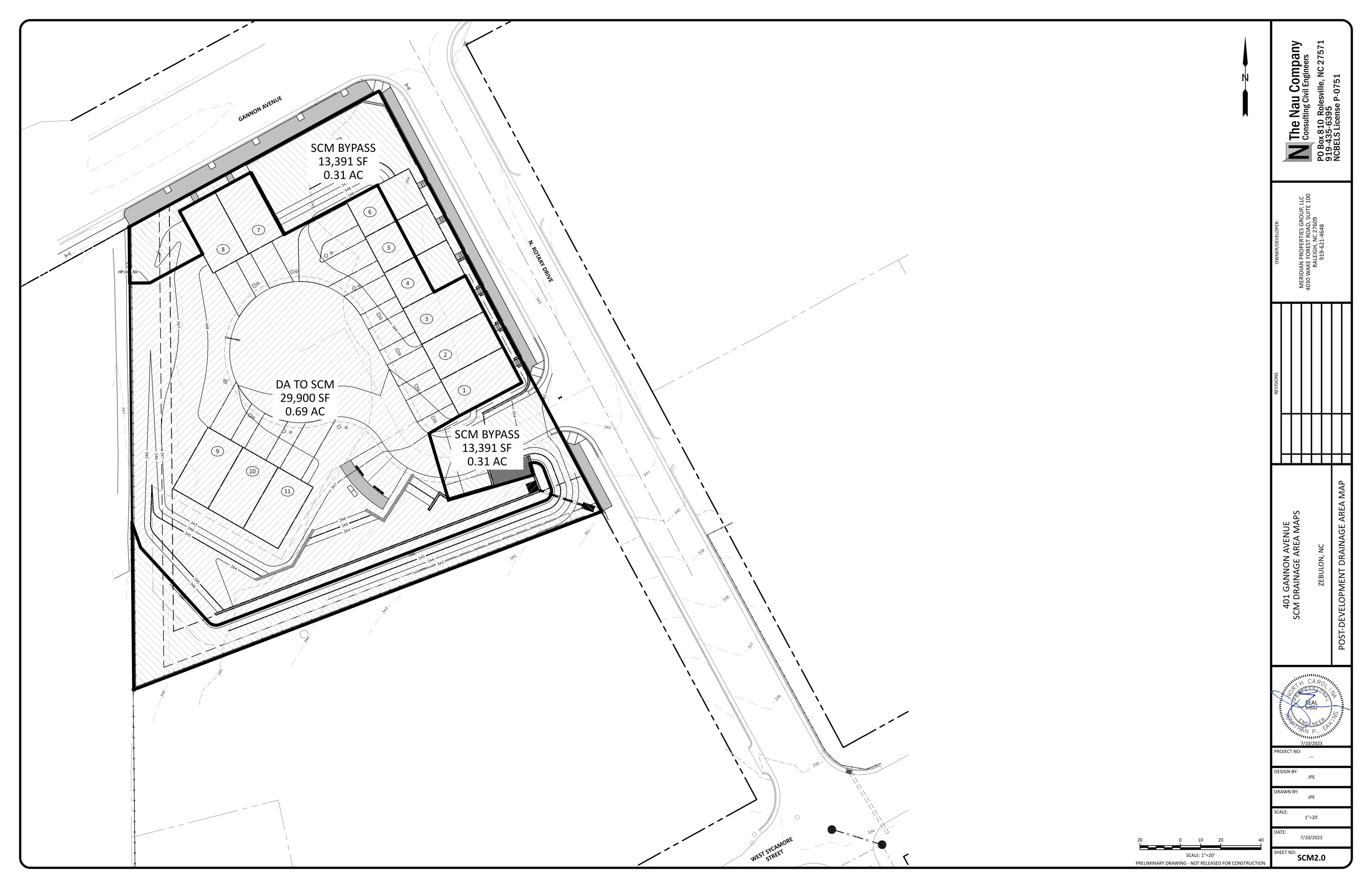
Appendix C – Bioretention Area Calculations

Appendix D – SNAP Tool Output

Appendix E – Supporting Documentation

APPENDIX A DRAINAGE AREA MAPS

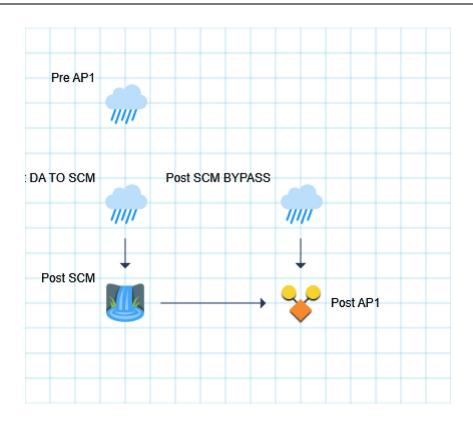




APPENDIX B HYDROLOGY STUDIO OUTPUT

Basin Model

07-10-2023 Hydrology Studio v 3.0.0.27



Project Name:

Hydrograph by Return Period

07-10-2023

Hyd.	Hydrograph	Hydrograph	Peak Outflow (cfs)							
No.	Туре	Name	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr
1	NRCS Runoff	Pre AP1	0.369	0.828			2.390			5.348
2	NRCS Runoff	Post DA TO SCM	1.445	2.020			3.585			6.092
3	Pond Route	Post SCM	0.054	0.066			0.121			4.666
4	NRCS Runoff	Post SCM BYPASS	0.280	0.474			1.060			2.085
4 5	NRCS Runoff Junction	Post SCM BYPASS Post AP1	0.280	0.474			1.060			2.085

Project Name:

Hydrograph 1-yr Summary Hydrology Studio v 3.0.0.27

07-10-2023

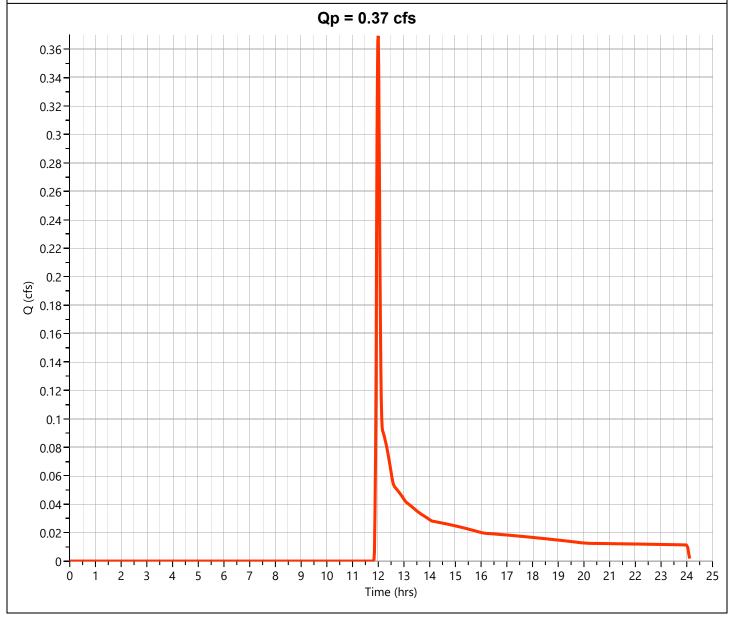
Pre AP1 Hyd. No. 1

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.369 cfs
Storm Frequency	= 1-yr	Time to Peak	= 12.00 hrs
Time Interval	= 1 min	Runoff Volume	= 1,123 cuft
Drainage Area	= 0.99 ac	Curve Number	= 61*
Tc Method	= User	Time of Conc. (Tc)	= 5.0 min
Total Rainfall	= 2.83 in	Design Storm	= Type II
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 0.99 61 Composite CN

0.99 61 Weighted CN Method Employed



Post DA TO SCM

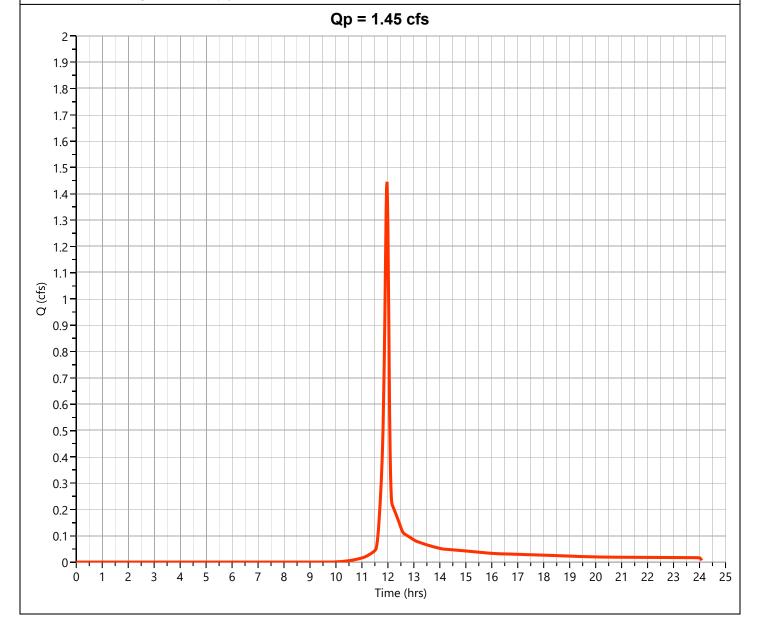
Hyd. No. 2

Hydrograph Type	= NRCS Runoff	Peak Flow	= 1.445 cfs
Storm Frequency	= 1-yr	Time to Peak	= 11.97 hrs
Time Interval	= 1 min	Runoff Volume	= 2,903 cuft
Drainage Area	= 0.69 ac	Curve Number	= 80*
Tc Method	= User	Time of Conc. (Tc)	= 5.0 min
Total Rainfall	= 2.83 in	Design Storm	= Type II
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 0.69 80 Composite CN

0.69 80 Weighted CN Method Employed

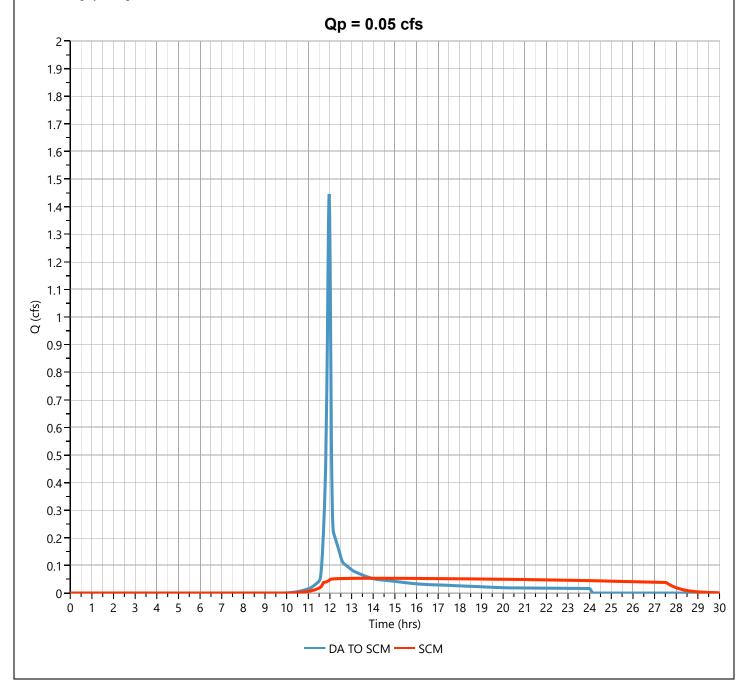


Post SCM Hyd. No. 3

Hydrograph Type	= Pond Route	Peak Flow	= 0.054 cfs			
Storm Frequency	= 1-yr	Time to Peak	= 13.93 hrs			
Time Interval	= 1 min	Hydrograph Volume	= 2,901 cuft			
Inflow Hydrograph	= 2 - DA TO SCM	Max. Elevation	= 344.22 ft			
Pond Name	= Bioretention	Max. Storage	= 1,497 cuft			
Routing Option	= Wet Pond	Wet Pond Elevation	= 343.50 ft			
David Parties by Steman Indication Mathed						

Pond Routing by Storage Indication Method

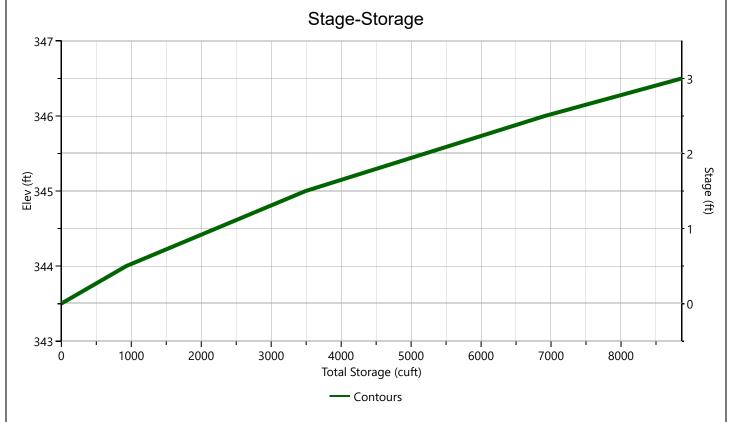
Center of mass detention time = 5.33 hrs



Bioretention

Stage-Storage

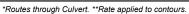
User Defined Contou	rs	Stage / Storage Table						
Description	Input	Stage (ft)	Elevation (ft)	Contour Area (sqft)	Incr. Storage (cuft)	Total Storage (cuft)		
Bottom Elevation, ft	343.50							
Voids (%)	100.00	0.00	343.50	1,603	0.000	0.000		
	100.00	0.50	344.00	2,114	929	929		
Volume Calc	None	1.50	345.00	3,013	2,564	3,493		
		2.50	346.00	3,825	3,419	6,912		
		3.00	346.50	4,000	1,956	8,868		

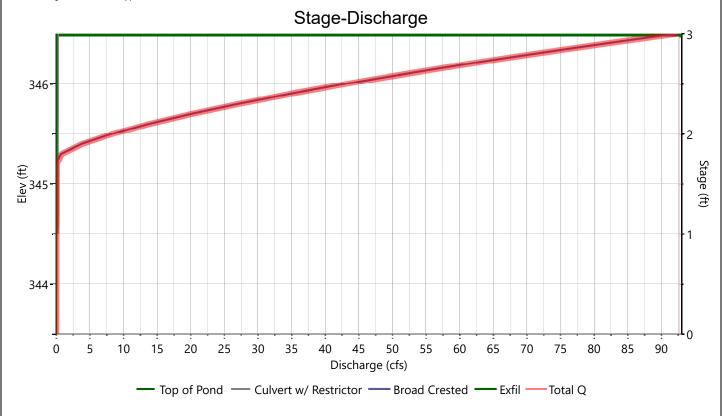


Bioretention

Stage-Discharge

0.14/0.15	Culvert w/		Orifices		O. C. C. Divis		
Culvert / Orifices	Restrictor Plate	1 2 3		3	Orifice Plate		
Rise, in	12				Orifice Dia, in		
Span, in	12				No. Orifices		
No. Barrels	1				Invert Elevation, ft		
Invert Elevation, ft	Culv: 341.90 1 in Orif: 341.90				Height, ft		
Orifice Coefficient, Co	0.60				Orifice Coefficient, Co		
Length, ft	100						
Barrel Slope, %	.5						
N-Value, n	0.013						
Waira	Riser*		Weirs		Ancillary		
Weirs	Kiser	1	2	3			
Shape / Type	Box	Broad Crested			Exfiltration, in/hr	1.00**	
Crest Elevation, ft	344.5	345.25					
Crest Length, ft	8	20					
Angle, deg							
Weir Coefficient, Cw	3.3	3.3					





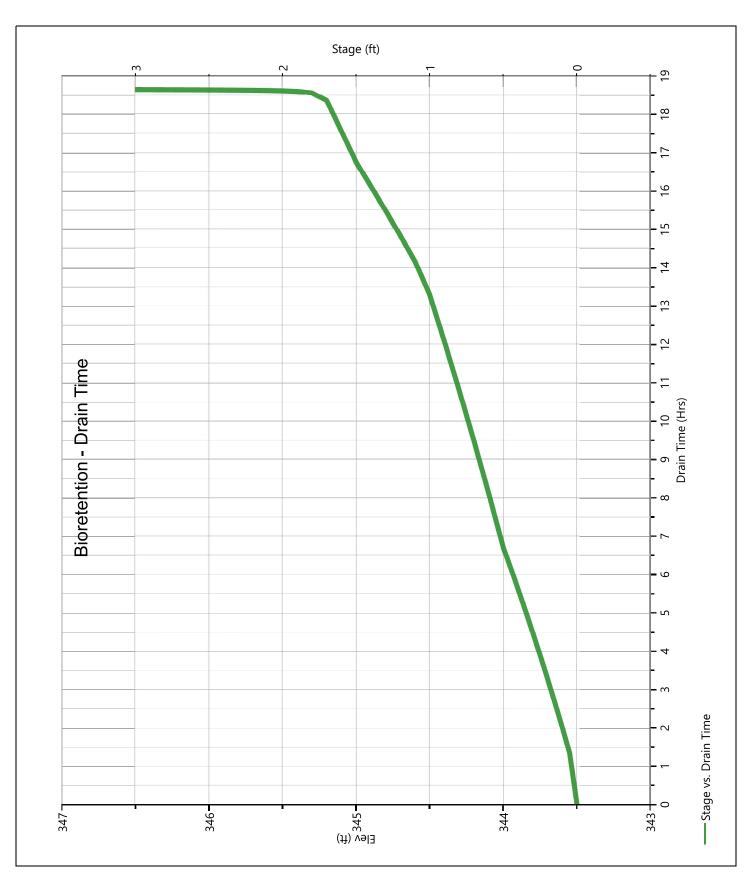
Bioretention

Stage-Storage-Discharge Summary

Stage	Elev.	Storage	Culvert	(Orifices, cf	s	Riser		Weirs, cfs	i	Pf Riser	Exfil	Exfil User	Total
(ft)	(ft)	(cuft)	(cfs)	1	2	3	(cfs)	1	2	3	(cfs)	(cfs)	(cfs)	(cfs)
0.00	343.50	0.000	0.000				0.000	0.000				0.000		0.000
0.50	344.00	929	0.000 ic				0.000	0.000				0.049		0.049
1.50	345.00	3,493	0.046 ic				0.000	0.000				0.070		0.116
2.50	346.00	6,912	0.053 ic				0.000	42.87				0.089		43.01
3.00	346.50	8,868	0.056 ic				0.000	92.24				0.093		92.39

Bioretention

Pond Drawdown



Post SCM BYPASS

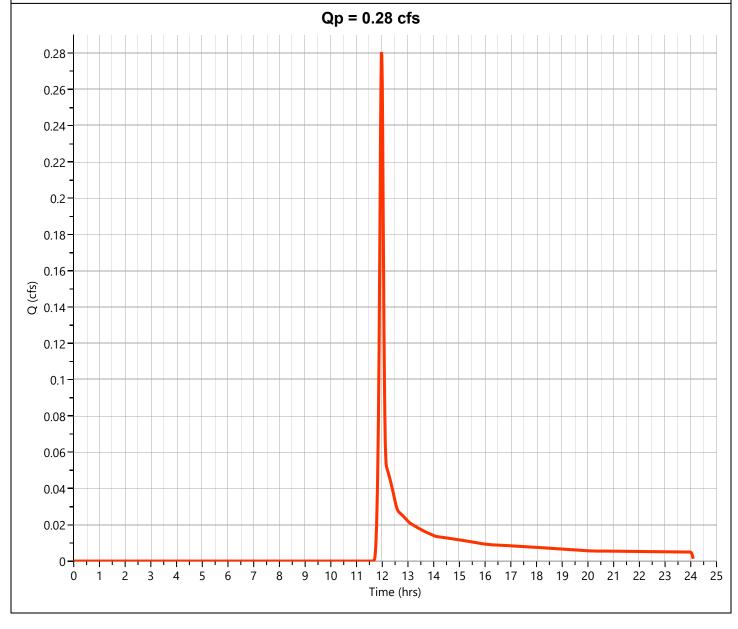
Hyd. No. 4

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.280 cfs
Storm Frequency	= 1-yr	Time to Peak	= 11.97 hrs
Time Interval	= 1 min	Runoff Volume	= 628 cuft
Drainage Area	= 0.31 ac	Curve Number	= 68*
Tc Method	= User	Time of Conc. (Tc)	= 5.0 min
Total Rainfall	= 2.83 in	Design Storm	= Type II
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 0.31 68 Composite CN

0.31 68 Weighted CN Method Employed



Post AP1 Hyd. No. 5

Hydrograph Type	= Junction	Peak Flow	= 0.327 cfs
Storm Frequency	= 1-yr	Time to Peak	= 11.97 hrs
īme Interval	= 1 min	Hydrograph Volume	= 3,529 cuft
nflow Hydrographs	= 3, 4	Total Contrib. Area	= 0.31 ac
	Qp = 0.33 cfs		
0.32			
0.3			
0.28			
0.26			
0.24			
0.22			
0.2			
0.18 - (§) - 0 0.16 -			
0.14			
0.12			
0.1			
0.08			
0.06			
0.04			
0.02			
0 1 2 3	4 5 6 7 8 9 10 11 12 13 14 15 16 17 Time (hrs)	18 19 20 21 22 23 24	25 26 27 28 29

Project Name:

Hydrograph 2-yr Summary Hydrology Studio v 3.0.0.27

07-10-2023

Hyd Hydrograph Hydrograph Peak Time to Hydrograph Inflow Maximum Maximum	yurology stu	ıdio v 3.0.0.27							07-10-202
2 NRCS Runoff Post DA TO SCM 2.020 11.97 4,063 3 Pond Route Post SCM 0.066 14.08 4,061 2 344.52 2,250 4 NRCS Runoff Post SCM BYPASS 0.474 11.97 992	Hyd.	Hydrograph		Flow	Peak	Volume	Inflow Hyd(s)	Elevation	Maximum Storage (cuft)
3 Pond Route Post SCM 0.066 14.08 4,061 2 344.52 2,250 4 NRCS Runoff Post SCM BYPASS 0.474 11.97 992	1	NRCS Runoff	Pre AP1	0.828	11.98	1,991			
4 NRCS Runoff Post SCM BYPASS 0.474 11.97 992	2	NRCS Runoff	Post DA TO SCM	2.020	11.97	4,063			
	3	Pond Route	Post SCM	0.066	14.08	4,061	2	344.52	2,250
5 Junction Post AP1 0.525 11.97 5,053 3,4	4	NRCS Runoff	Post SCM BYPASS	0.474	11.97	992			

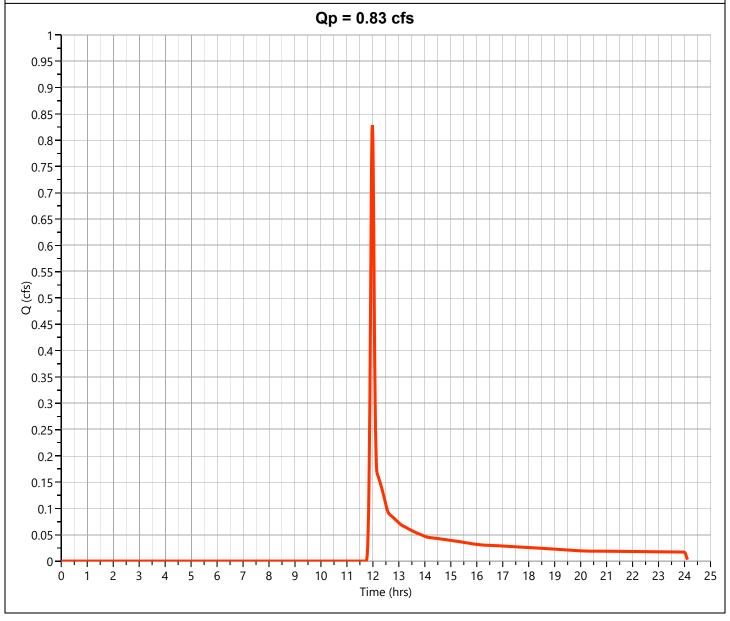
Pre AP1 Hyd. No. 1

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.828 cfs
Storm Frequency	= 2-yr	Time to Peak	= 11.98 hrs
Time Interval	= 1 min	Runoff Volume	= 1,991 cuft
Drainage Area	= 0.99 ac	Curve Number	= 61*
Tc Method	= User	Time of Conc. (Tc)	= 5.0 min
Total Rainfall	= 3.42 in	Design Storm	= Type II
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 0.99 61 Composite CN

0.99 61 Weighted CN Method Employed



Post DA TO SCM

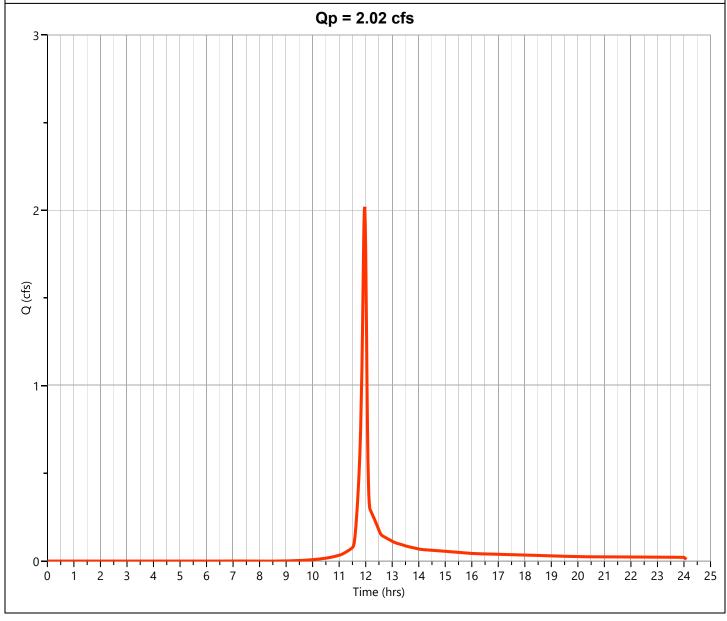
Hyd. No. 2

Hydrograph Type	= NRCS Runoff	Peak Flow	= 2.020 cfs
Storm Frequency	= 2-yr	Time to Peak	= 11.97 hrs
Time Interval	= 1 min	Runoff Volume	= 4,063 cuft
Drainage Area	= 0.69 ac	Curve Number	= 80*
Tc Method	= User	Time of Conc. (Tc)	= 5.0 min
Total Rainfall	= 3.42 in	Design Storm	= Type II
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 0.69 80 Composite CN

0.69 80 Weighted CN Method Employed



Post SCM Hyd. No. 3

Hydrograph Type	= Pond Route	Peak Flow	= 0.066 cfs
Storm Frequency	= 2-yr	Time to Peak	= 14.08 hrs
Time Interval	= 1 min	Hydrograph Volume	= 4,061 cuft
Inflow Hydrograph	= 2 - DA TO SCM	Max. Elevation	= 344.52 ft
Pond Name	= Bioretention	Max. Storage	= 2,250 cuft
Routing Option	= Wet Pond	Wet Pond Elevation	= 343.50 ft
Pond Routing by Storage Ind	lication Method	Center of mass	s detention time = 7.20 hrs
2-	Qp = 0.07 cfs		
2-			
7 (cfs) Q			
-			
0 2 4	6 8 10 12 14 16 18 20 Time (hrs)	22 24 26 28	30 32 34

Post SCM BYPASS

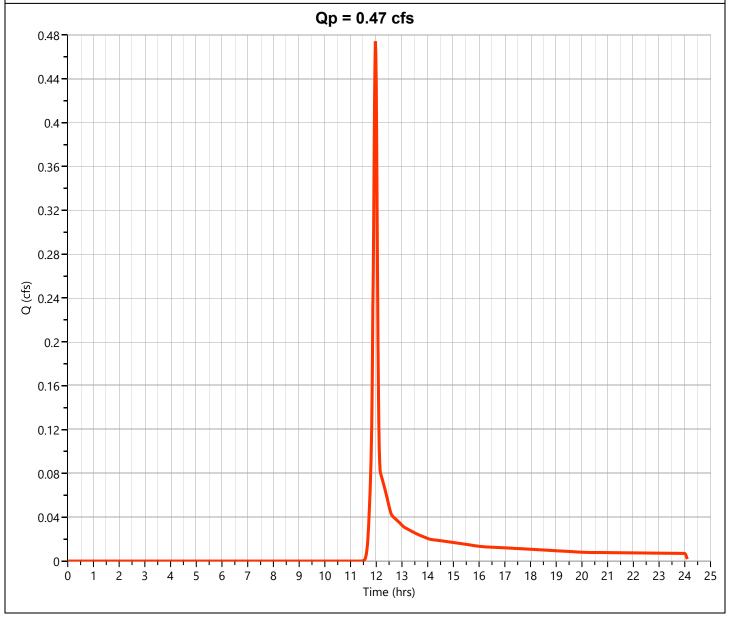
Hyd. No. 4

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.474 cfs
Storm Frequency	= 2-yr	Time to Peak	= 11.97 hrs
Time Interval	= 1 min	Runoff Volume	= 992 cuft
Drainage Area	= 0.31 ac	Curve Number	= 68*
Tc Method	= User	Time of Conc. (Tc)	= 5.0 min
Total Rainfall	= 3.42 in	Design Storm	= Type II
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

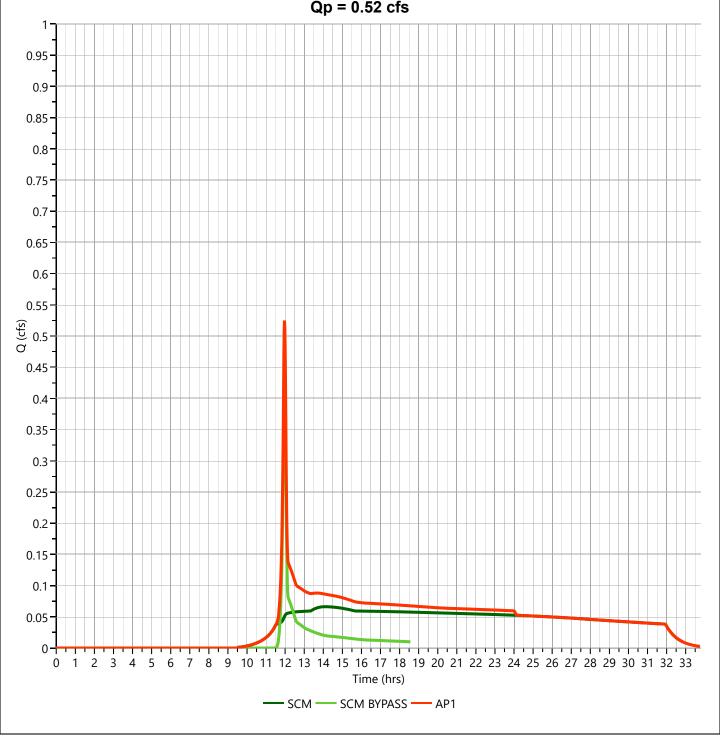
AREA (ac) CN DESCRIPTION 0.31 68 Composite CN

0.31 68 Weighted CN Method Employed



Post AP1 Hyd. No. 5

				-
Hydrograph Type	= Junction		Peak Flow	= 0.525 cfs
Storm Frequency	= 2-yr		Time to Peak	= 11.97 hrs
Time Interval	= 1 min		Hydrograph Volume	= 5,053 cuft
Inflow Hydrographs	= 3, 4		Total Contrib. Area	= 0.31 ac
		Qp = 0.52 cfs		
0.95				



Project Name:

Hydrograph 10-yr Summary Hydrology Studio v 3.0.0.27

07-10-2023

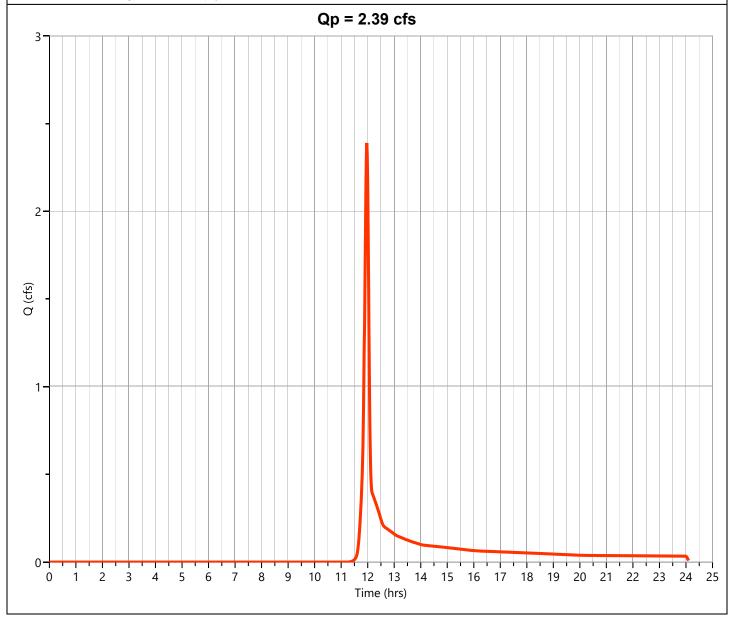
Pre AP1 Hyd. No. 1

Hydrograph Type	= NRCS Runoff	Peak Flow	= 2.390 cfs
Storm Frequency	= 10-yr	Time to Peak	= 11.97 hrs
Time Interval	= 1 min	Runoff Volume	= 4,941 cuft
Drainage Area	= 0.99 ac	Curve Number	= 61*
Tc Method	= User	Time of Conc. (Tc)	= 5.0 min
Total Rainfall	= 4.94 in	Design Storm	= Type II
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 0.99 61 Composite CN

0.99 61 Weighted CN Method Employed



Post DA TO SCM

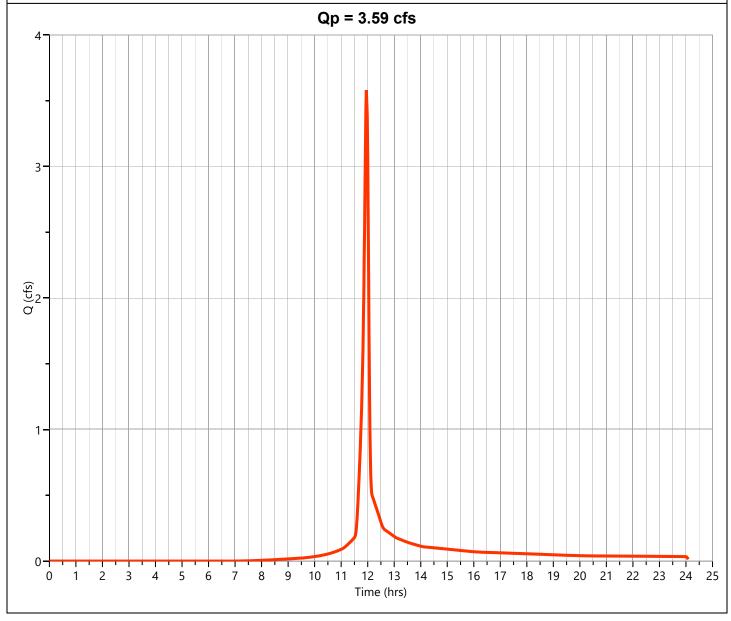
Hyd. No. 2

Hydrograph Type	= NRCS Runoff	Peak Flow	= 3.585 cfs
Storm Frequency	= 10-yr	Time to Peak	= 11.97 hrs
Time Interval	= 1 min	Runoff Volume	= 7,337 cuft
Drainage Area	= 0.69 ac	Curve Number	= 80*
Tc Method	= User	Time of Conc. (Tc)	= 5.0 min
Total Rainfall	= 4.94 in	Design Storm	= Type II
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 0.69 80 Composite CN

0.69 80 Weighted CN Method Employed



Post SCM Hyd. No. 3

lydrograph Type	= Pond Route	Peak Flow	= 0.121 cfs
lydrograph Type storm Frequency	= Pond Route = 10-yr	Time to Peak	= 0.121 cis = 13.87 hrs
ime Interval	= 1 min	Hydrograph Volume	= 7,335 cuft
nflow Hydrograph	= 2 - DA TO SCM	Max. Elevation	= 345.19 ft
ond Name	= Bioretention	Max. Storage	= 4,140 cuft
Routing Option	= Wet Pond	Wet Pond Elevation	= 343.50 ft
ond Routing by Storage Ind		Center of mas	s detention time = 7.60 h
	Qp = 0.12 cfs		
4	·		
1			
3			
4			
52			
1			
1			
1-			
1			
0			

— DA TO SCM — SCM

Post SCM BYPASS

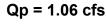
Hyd. No. 4

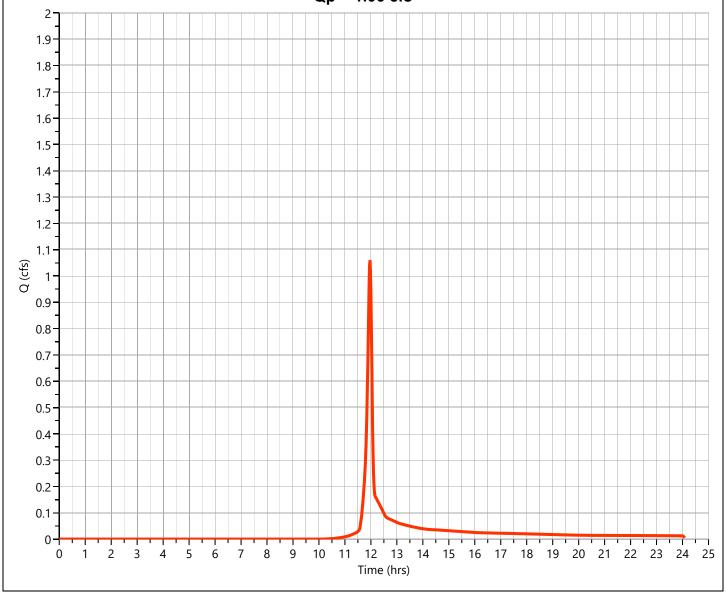
Hydrograph Type	= NRCS Runoff	Peak Flow	= 1.060 cfs
Storm Frequency	= 10-yr	Time to Peak	= 11.97 hrs
Time Interval	= 1 min	Runoff Volume	= 2,132 cuft
Drainage Area	= 0.31 ac	Curve Number	= 68*
Tc Method	= User	Time of Conc. (Tc)	= 5.0 min
Total Rainfall	= 4.94 in	Design Storm	= Type II
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 0.31 68 Composite CN

0.31 68 Weighted CN Method Employed





Post AP1 Hyd. No. 5

Hydrograph Type			Peak Flow	= 1.152 cfs = 11.97 hrs = 9,467 cuft = 0.31 ac	
Storm Frequency			Time to Peak		
Time Interval	= 1 min				
Inflow Hydrographs	= 3, 4		Total Contrib. Area		
	Qp =	: 1.15 cfs			
2					
1.9					
1.8					
1.7					
1.6					
1.5					
1.4					
1.3					
-					
1.2	•				
1.1					
(\$\frac{1}{2}\)					
0.9					
0.8					
0.7					
0.6					
0.5					
4					
0.4					
0.3					
0.2					
0.1					
0					

Project Name:

Hydrograph 100-yr Summary

07-10-2023

Hyd. No.	Hydrograph Type	Hydrograph Name	Peak Flow (cfs)	Time to Peak (hrs)	Hydrograph Volume (cuft)	Inflow Hyd(s)	Maximum Elevation (ft)	Maximum Storage (cuft)
1	NRCS Runoff	Pre AP1	5.348	11.97	10,741			
2	NRCS Runoff	Post DA TO SCM	6.092	11.95	12,771			
3	Pond Route	Post SCM	4.666	12.02	12,768	2	345.42	4,915
4	NRCS Runoff	Post SCM BYPASS	2.085	11.97	4,212			
							345.42	4,915

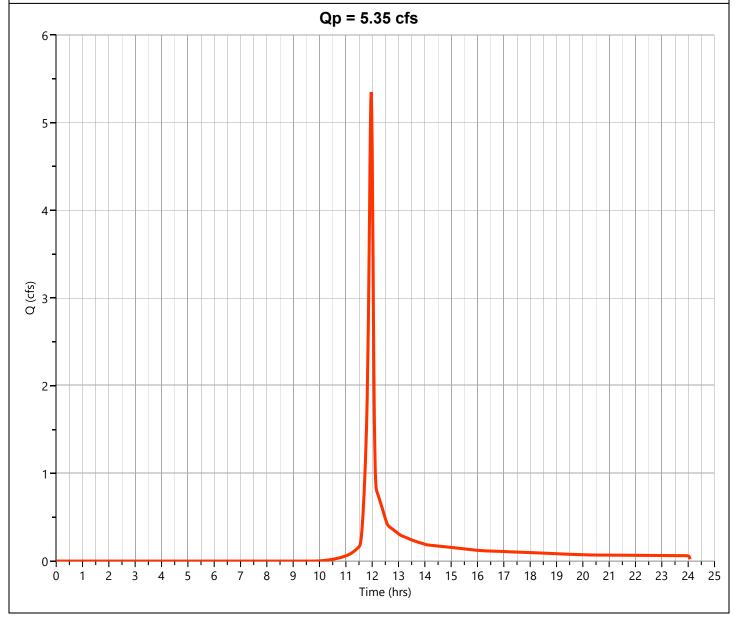
Pre AP1 Hyd. No. 1

Hydrograph Type	= NRCS Runoff	Peak Flow	= 5.348 cfs
Storm Frequency	= 100-yr	Time to Peak	= 11.97 hrs
Time Interval	= 1 min	Runoff Volume	= 10,741 cuft
Drainage Area	= 0.99 ac	Curve Number	= 61*
Tc Method	= User	Time of Conc. (Tc)	= 5.0 min
Total Rainfall	= 7.27 in	Design Storm	= Type II
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 0.99 61 Composite CN

0.99 61 Weighted CN Method Employed



Hydrology Studio v 3.0.0.27 07-10-2023

Post DA TO SCM

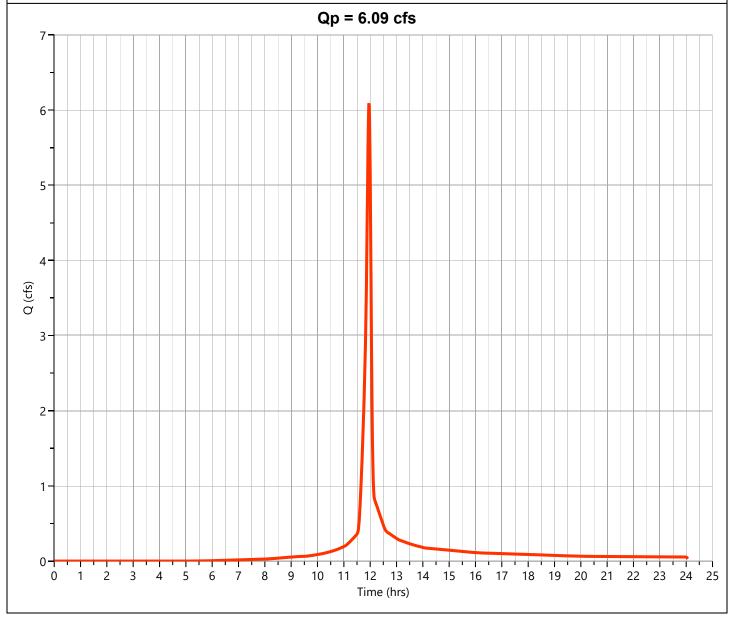
Hyd. No. 2

Hydrograph Type	= NRCS Runoff	Peak Flow	= 6.092 cfs
Storm Frequency	= 100-yr	Time to Peak	= 11.95 hrs
Time Interval	= 1 min	Runoff Volume	= 12,771 cuft
Drainage Area	= 0.69 ac	Curve Number	= 80*
Tc Method	= User	Time of Conc. (Tc)	= 5.0 min
Total Rainfall	= 7.27 in	Design Storm	= Type II
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 0.69 80 Composite CN

0.69 80 Weighted CN Method Employed



5-

4-

2-

1-

Q (cfs)

Hydrology Studio v 3.0.0.27 07-10-2023

Post SCM			Hyd. No. 3
Hydrograph Type	= Pond Route	Peak Flow	= 4.666 cfs
Storm Frequency	= 100-yr	Time to Peak	= 12.02 hrs
Time Interval	= 1 min	Hydrograph Volume	= 12,768 cuft
Inflow Hydrograph	= 2 - DA TO SCM	Max. Elevation	= 345.42 ft
Pond Name	= Bioretention	Max. Storage	= 4,915 cuft
Routing Option	= Wet Pond	Wet Pond Elevation	= 343.50 ft
Pond Routing by Storage Ind	dication Method	Center of mass	s detention time = 4.61 hrs
	Qp = 4.67 cfs		
6-			

18 20 22 24

Time (hrs) DA TO SCM — SCM 1 26

i 28

i 30

i 32

1 10

12

14

Hydrology Studio v 3.0.0.27 07-10-2023

Post SCM BYPASS

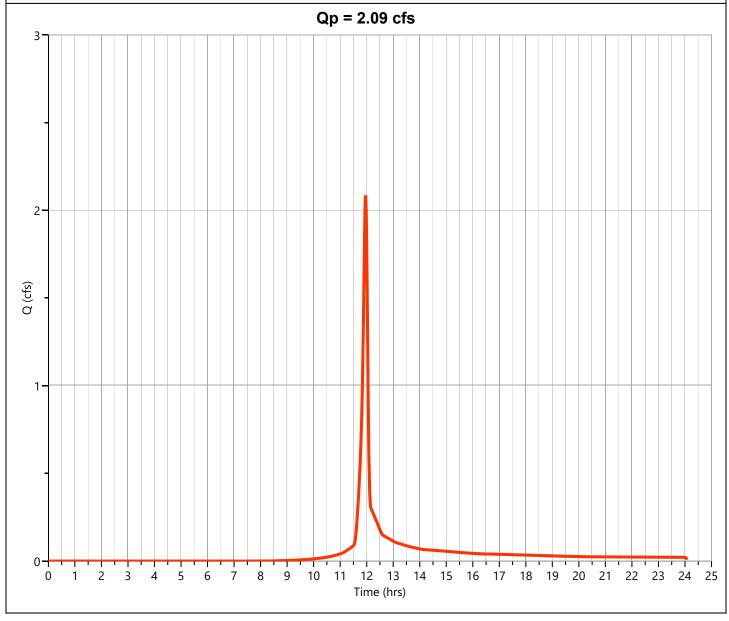
Hyd. No. 4

Hydrograph Type	= NRCS Runoff	Peak Flow	= 2.085 cfs
Storm Frequency	= 100-yr	Time to Peak	= 11.97 hrs
Time Interval	= 1 min	Runoff Volume	= 4,212 cuft
Drainage Area	= 0.31 ac	Curve Number	= 68*
Tc Method	= User	Time of Conc. (Tc)	= 5.0 min
Total Rainfall	= 7.27 in	Design Storm	= Type II
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 0.31 68 Composite CN

0.31 68 Weighted CN Method Employed



Hydrology Studio v 3.0.0.27 07-10-2023

Post AP1 Hyd. No. 5

lydrograph Type	= Junction	Peak Flow	= 6.292 cfs
torm Frequency	= 100-yr	Time to Peak	= 12.00 hrs
ime Interval	= 1 min	Hydrograph Volume	= 16,981 cuft
nflow Hydrographs	= 3, 4	Total Contrib. Area	= 0.31 ac
	Qp = 6.29 cfs		
7			
6-			
-			
5			
-			
4			
4			
- (cis)			
α			
3			
-			
2			
1			
4			
0 1 2 2 4 5	6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	24.25.26.27.20.20.20.21.2	2 22 24 25 26 27 29
0 1 2 3 4 5	Time (hrs)	24 23 20 21 20 29 30 31 3.	∠ 33 34 33 30 3 <i>1</i> 30
	— SCM — SCM BYPASS — AP	1	

APPENDIX C BIORETENTION AREA CALCULATIONS

APPENDIX C

BIORETENTION AREA SUPPORTING CALCULATIONS

401 GANNON AVENUE

July 10, 2023

SCS CN CALCULATIONS

PRE-DEVELOPMENT			E	ntire Si	te
401 GANNON AVENUE July 10, 2023 Hydrologic Soil Group B			This data reflects the pre-development conditions of the entire site drainage area		
ONSITE LAND COVERS			ONSIT	E DRAINAC	GE AREA
IMPERVIOUS LAND COVERS	SCS CN	Aug 9/ Imp	Are	_	Woightod CN
Road (pavement only)	SCS CIV	Avg % Imp	[sq ft] 0	[ac] 0.00	Weighted CN 0
Parking			0	0.00	0
Roof			0	0.00	0
Driveway	98		0	0.00	0
Sidewalk	36		0	0.00	0
Deck/patio			0	0.00	0
Other impervious			0	0.00	0
Other impervious			0 Are	0.00	0
PERVIOUS LAND COVERS	SCS CN	Avg % Imp	[sq ft]	ac]	Weighted CN
Lawn/grass/open space	61		0	0.00	0
Grass (within R/W)	61		43,291	0.99	61
Woods	55		0	0.00	0
Natural wetland	55		0	0.00	0
Riparian buffer	55		0	0.00	0
Other pervious Other pervious	0 0		0 0	0.00 0.00	0 0
	U		Are		U
COMPOSITE LAND COVERS	SCS CN	Avg % Imp	[sq ft]	[ac]	Weighted CN
Commercial area	92	85	0	0.00	0
Industrial area	88	72	0	0.00	0
Residential area (<1/8 acre lot)	85	65	0	0.00	0
Residential (1/4 acre lot)	75	38	0	0.00	0
Residential (1/3 acre lot)	72	30	0	0.00	0
ONSITE TOTALS			43,291	0.99	61
TOTAL ONSITE IMPERVIOUS			0	0.00	
OTHER ONSITE LAND COVERS	SCS CN	Aug 0/ Iman	Are		Maightad CN
SCM	3C3 CN	Avg % Imp	[sq ft] 0	[ac] 0.00	Weighted CN
Open Water			0	0.00	
OFFSITE LAND COVERS			OFFSIT	E DRAINA	GE AREA
			Are	ea	
COMPOSITE LAND COVERS	SCS CN	Avg % Imp	[sq ft]	[ac]	Weighted CN
Impervious	98		0	0.00	0
Pervious	74		0	0.00	0
Road R/W	98	100	0	0.00	0
Road R/W	96	90	0	0.00	0
Commercial area Industrial area	93 91	80 70	0	0.00 0.00	0
Residential area (<1/8 acre lot)	88	70 60	0 0	0.00	0 0
Residential (1/4 acre lot)	86	50	0	0.00	0
Residential (1/3 acre lot)	84	40	0	0.00	0
OFFSITE TOTALS			0	0.00	0
			Are	22	
TOTAL DDAWN 07 17 -			[sq ft]	a [ac]	Composite CN
TOTAL DRAINAGE ARA					
			43,291	0.99	61

POST-DEVELOPMENT TO	TAL POND D	A		DA1.1	
401 GANNON AVENUE			DA to SCM		
July 10, 2023 Hydrologic Soil Group		В			
ONSITE LAND COVERS		b	ONSIT	E DRAINA	GE AREA
IMPERVIOUS LAND COVERS			Are		
Road (pavement only)	SCS CN	Avg % Imp	[sq ft] 5,550	[ac] 0.13	Weighted CN 18
Parking			3,330 0	0.13	0
Roof			6,650	0.15	22
Driveway			3,275	0.08	11
Sidewalk	98		175	0.00	1
Deck/patio			0	0.00	0
All impervious			0	0.00	0
Other impervious			0	0.00	0
PERVIOUS LAND COVERS	SCS CN	A 0/ J	Are		Mainhead CA
Lawn/grass/open space	5C5 CN 61	Avg % Imp	[sq ft] 14,250	[ac] 0.33	Weighted CN 29
Grass (within R/W)	61		0	0.00	0
Woods	55		0	0.00	0
Natural wetland	55		0	0.00	0
Riparian buffer	55		0	0.00	0
Other pervious	61		0	0.00	0
Other pervious	61		0	0.00	0
COMPOSITE LAND COVERS	SCS CN	Avg % Imp	Are [sq ft]	ea [ac]	Weighted CN
Commercial area	92	85	[sq 1t] 0	0.00	vveignted civ
Industrial area	88	72	0	0.00	0
Residential area (<1/8 acre lot)	85	65	0	0.00	0
Residential (1/4 acre lot)	75	38	0	0.00	0
Residential (1/3 acre lot)	72	30	0	0.00	0
ONSITE TOTALS			29,900	0.69	80
TOTAL ONSITE IMPERVIOUS			15,650	0.36	
OTHER ONSITE LAND COVERS	SCS CN	Avg % Imp	Are [sq ft]	ea [ac]	Weighted CN
SCM	3C3 CN	Avg // IIIIp	1,600	0.04	Weighted CN
Open Water			0	0.00	
OFFSITE LAND COVERS				E DRAINA	GE AREA
OTTOTTE LAND COVERS			Are		OL AREA
COMPOSITE LAND COVERS	SCS CN	Avg % Imp	[sq ft]	[ac]	Weighted CN
mpervious	98		0	0.00	0
Pervious	61		0	0.00	0
Road R/W	98	100	0	0.00	0
Road R/W	94	90	0	0.00	0
Commercial area	91	80	0	0.00	0
Industrial area	87	70 60	0	0.00	0
Residential area (<1/8 acre lot)	83	60 50	0	0.00	0
Residential (1/4 acre lot) Residential (1/3 acre lot)	80 76	50 40	0 0	0.00 0.00	0 0
	70	40			-
OFFSITE TOTALS			0	0.00	0
			Are [sq ft]	ea [ac]	Composite CN
TOTAL DRAINAGE ARA					-
			29,900	0.69	80

POST-DEVELOPMENT TO	TAL POND DA	A		DA1.2	
401 GANNON AVENUE			SCM Bypass		
July 10, 2023 Hydrologic Soil Group		В			
ONSITE LAND COVERS			ONSIT	E DRAINA	GE AREA
IMPERVIOUS LAND COVERS	SCS CN	Ava % Imp	Ard [sq ft]		Weighted CN
Road (pavement only)	SCS CIV	Avg % Imp	1,225	[ac] 0.03	weighted CN
Parking			0	0.00	0
Roof			1,050	0.02	8
Driveway			0	0.00	0
Sidewalk	98		125	0.00	1
Deck/patio			0	0.00	0
All impervious			0	0.00	0
Other impervious			0	0.00	0
PERVIOUS LAND COVERS			Ar		
	SCS CN	Avg % Imp	[sq ft]	[ac]	Weighted CN
Lawn/grass/open space	61		10,991	0.25	50
Grass (within R/W)	61		0	0.00	0
Woods	55		0	0.00	0
Natural wetland	55		0	0.00	0
Riparian buffer	55		0	0.00	0
Other pervious Other pervious	61 61		0 0	0.00 0.00	0 0
COMPOSITE LAND COVERS	-		Ar	ea	-
COMI OSITE LAND COVERS	SCS CN	Avg % Imp	[sq ft]	[ac]	Weighted CN
Commercial area	92	85	0	0.00	0
ndustrial area	88	72	0	0.00	0
Residential area (<1/8 acre lot)	85	65	0	0.00	0
Residential (1/4 acre lot) Residential (1/3 acre lot)	75 72	38 30	0 0	0.00 0.00	0 0
ONSITE TOTALS	,,,	30	13,391	0.31	68
TOTAL ONSITE IMPERVIOUS			2,400	0.06	
OTHER ONSITE LAND COVERS			Are		
	SCS CN	Avg % Imp	[sq ft]	[ac]	Weighted CN
SCM			0	0.00	
Open Water			0	0.00	
OFFSITE LAND COVERS			OFFSIT	E DRAINA	GE AREA
COMPOSITE LAND COVERS	CCC CN	A = 0/ I	Are		\\\-:- -+ C\
mnonvious	SCS CN	Avg % Imp	[sq ft]	[ac]	Weighted CN
mpervious	98 61		0	0.00 0.00	0
Pervious Road R/W	98	100	0 0	0.00	0 0
Road R/W	98 94	90	0	0.00	0
Commercial area	91	80	0	0.00	0
ndustrial area	87	70	0	0.00	0
Residential area (<1/8 acre lot)	83	60	0	0.00	0
Residential (1/4 acre lot)	80	50	0	0.00	0
Residential (1/3 acre lot)	76	40	0	0.00	0
OFFSITE TOTALS			0	0.00	0
			Ar		
TOTAL DRAINAGE ARA			[sq ft]	[ac]	Composite Cl
IOIAL DIIAINAUL AIIA			13,391	0.31	68

RUNOFF VOLUME BY SIMPLE METHOD

401 GANNON AVENUE Bioretention Area

Runoff Volume by the Simple Method taken from NCDEQ Stormwater Design Manual Part B

Input Data

Impervious fraction	la	0.523
Drainage area	Α	0.69 acres
Design storm rainfall depth	Rd	1.00 inches

Output

Runoff coefficient	Rv	0.52
Runoff volume	V	1,298 cubic feet

$$R_v = 0.05 + 0.9 \times I_A$$

$$V = 3630 \times R_D \times R_{V \times} A$$

BIORETENTION AREA SIZING

401 GANNON AVENUE Bioretention Area

TOI GAINION A	LINGE		Diorete
Drainage area		29,900 SF	
Impervious area		15,650 SF	_
Percent imperviou	IS	52.3%	_
Runoff volume to	treat	1,298 CF	(from simple method)
Bioretention Cell [Design Data		
Design ponding de		12.00 inches	
Surface area of bio	·	1,300 SF	
Elev at bottom of		256.00	
Elev at bottom of	soil media	253.00	_
Elev of underdrain	ı	252.00	_
Underdrain diame	ter	4.00 in.	_
Underdrain slope		0.0100 ft/ft	_
Underdrain manni	ng's n	0.011	_
	te factor of safety (FS)	10	_
Infiltration rate of	cell media	2.0 in/hr	_
Void ratio of soil n	nedia	50.0%	_
	ing Flowrate Thru Soil Media		
Volume above gro		1,300 CF	<u> </u>
Volume in soil me		1,950 CF	<u> </u>
Total volume to de		3,250 CF	<u> </u>
-	rom infiltration rate	24.0 hrs	<u> </u>
Flowrate thru med		0.04 cfs	<u> </u>
Flowrate thru med	lia to underdrain w/ FS	0.38 cfs	_
	ing Flowrate Thru Underdrain		g full)
Cross sectional are		0.09	<u> </u>
Wetted perimeter		1.05	<u> </u>
Hydraulic radius		0.083	<u> </u>
Underdrain capaci	ty	0.22 cfs	_
Outflow Calculation	on and Cell Dewatering Time		
	dia to underdrain w/ FS	0.38 cfs	
Underdrain capaci	•	0.22 cfs	_
Outflow limited by	•	underdrain	
Dewatering time		0.17 days	_
2112121116			

Note: outflow should be limited by the soil media infiltration rate



401 GANNON AVENUE Bioretention Area

Elevation at WQ Volume 344.14
Calculated surface pond surface area at above elevation 2,240 SF
Calculated pond volume at above elevation 1,288 CF
Calculated WQ Volume from simple method 1,298 CF

	POND ELEVATION AND CONTOUR DATA						
343.5	1,603 SF	0.0	0	0			
344	2,114 SF	0.5	929 CF	929 CF			
345	3,013 SF	1.5	2,564 CF	3,493 CF			
346	3,825 SF	2.5	3,419 CF	6,912 CF			
346.5	4,000 SF	3.0	1,956 CF	8,868 CF			

ANTI FLOTATION BLOCK CALCULATIONS

401 GANNON AVENUE Bioretention Area

Constants

Unit weight of water 62.4 lb/cf
Unit weight of concrete 144.0 lb/cf

Riser Data

	Length	Width	Area
Inside domensions	4.00 ft	4.00 ft	16.0 SF
Outside dimensions	5.00 ft	5.00 ft	25.0 SF

Cross sectional riser area 9.0 SF
Riser inside height 3.5 ft
Volume of concrete in riser 32 CF

Riser base area 25.0 SF (same as riser outside dimensions)

Riser base thickness 0.5 ft

13 CF

Total volume of concrete in riser+base 44 CF
Total bouyant weight of riser 3,590 lbs

Water displaced by riser 88 CF
Weight of water displaced 5,460 lbs

Anti-Flotation Block Data

Volume of concrete in base

Length of anti-flotation block
Width of anti-flotation block
Thickness of anti-flotation block

Volume of anti-flotation block

54 CF

Volume of anti-flotation block54 CFTotal weight of anti-flotation block7,776 lbs

Factor of Safety

Weight of riser+anti-flotation block11,366 lbsWeight of water displaced by riser5,460 lbsFactor of safety against flotation2.08

APPENDIX D SNAP TOOL OUTPUT

Project Information

Complete this sheet if required by your reviewing authority. Contact them for any questions. Grey boxes/text are optional.

SNAP v4.2.0

LOCATION

Project Name (optional):	401 W Gannon Ave		P
Submission Date (optional):		date	N
Local Jurisdiction / Reviewing Agency:	Zebulon	menu	
Project Latitude Coordinates (optional):		N	
Project Longitude Coordinates (optional):		W	

Parcel ID (optional):		
Nutrient Management Watershed:	Neuse	menu
Subwatershed:	Neuse-Upper	menu
Phosphorus Delivery Zone:	Neuse - Upper 03020201	menu
Nitrogen Delivery Zone:	Neuse - Upper 03020201	menu

PROJECT DETAILS

Development Land Use Type:	Multi-Family Residential	menu
Part of Common Development Plan?	no	y/n
Designated Downtown Area?	no	y/n
Public Linear Road/Sidewalk Project?	no	y/n
Project Owner Type:	Private	menu

	Disturbed Area:	43,291	ft ²
	Project Activity:	New Development	menu
1	Project Drains to SA Waters?	no	y/n
1	Pre-Project Land Use:	fallow/open	menu
1	Project Description (optional):		

STORMWATER DETAILS

(Falls ONLY) Onsite Reduction % Req.	1%	%
Existing BUA/Development Onsite?	no	y/n
Local Gov't cutoff date for Existing BUA:	01/01/1901	date
Nitrogen Export Rate Target:	2.20	lb/ac/yr
Phosphorus Export Rate Target:	0.33	lb/ac/yr

Project Uses LID/Runoff Volume Match?	no	y/n
Local Gov't nutrient req's same as State?	yes	y/n
Project Drains to Regional SCM?	no	y/n
Total Nitrogen Offset Credits Needed:	0.0	lb/yr
Total Phosphorus Offset Credits Needed:	0.0	lb/yr

Project Area and Offsite Land Cover Characteristics

Precipitation
Station:

Raleigh

Copy & Paste VALUES ONLY for Best Results

Click here to scroll down to error messages on this sheet.

PROJECT AREA LAND COVERS	TN EMC (mg/L)	TP EMC (mg/L)	Pre-Project Area (ft ²)	Post-Project Area (ft ²)	Change pre-to-post (ft ²)
Roof	1.18	0.11		7,700	7,700
Roadway	1.64	0.34		6,775	6,775
Parking/Driveway/Sidewalk	1.42	0.18		3,575	3,575
Protected Forest	0.97	0.03			0
Managed Pervious/Landscaping	2.48	1.07	43,291	23,641	-19,650
Offsite or Existing Roof	1.18	0.11			0
Offsite or Existing Roadway	1.64	0.34			0
Offsite or Existing Parking/Driveway/Sidewa	1.42	0.18			0
Offsite Protected Forest	0.97	0.03			0
Offsite Managed Pervious	2.48	1.07			0
CUSTOM LAND COVER 1					0
CUSTOM LAND COVER 2					0
CUSTOM LAND COVER 3					0
LAND TAKEN UP BY SCM	1.18	0.11		1,600	1,600
	Total (Regulate	d & UnReg) Area	43,291.00	43,291.00	
	Project ((Regulated) Area	43,291.00	43,291.00	

Stormwater Control Measure (SCM) Characteristics

Click here to go to SCM101's Land Cover Data

SNAP v4.2.0

Copy & Paste VALUES ONLY for Best Results

Catchment ID SCM ID	1 101	ins to 102 Dra	1 103
Type of SCM	Bioretention w/IWS		
Hydrologic soil group at SCM location	В		
SCM Description	scм		
Design Storm Size (inches/24hrs)	1.00		
Percent of Full Size	100%		
% Annual Effluent	27%	0%	0%
% Annual Overflow	6%	0%	0%
% Annual ET/Infiltrated	67%	0%	0%
Custom % Annual Effluent			
Custom % Annual Overflow			
Custom % Annual ET/Infiltrated			
SCM Effluent TP EMC (mg/L)	0.08	0.00	0.00
SCM Effluent TN EMC (mg/L)	0.68	0.00	0.00
Custom Effluent TP EMC			
Custom Effluent TN EMC			
SCM Land Cover TP EMC (mg/L)	0.11	0.00	0.00
SCM Land Cover TN EMC (mg/L)	1.18	0.00	0.00
This SCM Drains to Numbered SCM	0	0	0
Catchment Routing	Catchments Draining to SCM 101	Catchments Draining to SCM 102	Catchments Draining to SCM 103
Catchment 1			
Catchment 2			
Catchment 3			
Catchment 4			
Catchment 5			
Catchment 6			
Error Check - Missing SCM Area:			

SCM Characteristics

Error Check - Min/Max Size:			
Error Check - Hydrology:			
Error Check - Missing SCM Info:			
Error Check - Drainage Data w/o SCM:			
Error Checks - SCM Type:			
SCM ID:	101	102	103
SCM Drainage Area Land Covers	Area Draining Directly to SCM 101 (ft2)	Area Draining Directly to SCM 102 (ft2)	Area Draining Directly to SCM 103 (ft2)
Roof	6,650		
Roadway	5,725		
Parking/Driveway/Sidewalk	3,350		
Protected Forest			
Managed Pervious/Landscaping	12,425		
Managed Pervious/Landscaping Offsite or Existing Roof	12,425		
	12,425		
Offsite or Existing Roof			
Offsite or Existing Roof Offsite or Existing Roadway			
Offsite or Existing Roof Offsite or Existing Roadway Offsite or Existing Parking/Driveway/Sidew			
Offsite or Existing Roof Offsite or Existing Roadway Offsite or Existing Parking/Driveway/Sidew Offsite Protected Forest			
Offsite or Existing Roof Offsite or Existing Roadway Offsite or Existing Parking/Driveway/Sidew Offsite Protected Forest Offsite Managed Pervious			
Offsite or Existing Roof Offsite or Existing Roadway Offsite or Existing Parking/Driveway/Sidew Offsite Protected Forest Offsite Managed Pervious CUSTOM LAND COVER 1			
Offsite or Existing Roof Offsite or Existing Roadway Offsite or Existing Parking/Driveway/Sidew Offsite Protected Forest Offsite Managed Pervious CUSTOM LAND COVER 1 CUSTOM LAND COVER 2			
Offsite or Existing Roof Offsite or Existing Roadway Offsite or Existing Parking/Driveway/Sidew Offsite Protected Forest Offsite Managed Pervious CUSTOM LAND COVER 1 CUSTOM LAND COVER 2 CUSTOM LAND COVER 3	ralk	0	0

SCM Characteristics

Error Check - Min/Max Size:			
Error Check - Hydrology:			
Error Check - Missing SCM Info:			
Error Check - Drainage Data w/o SCM:			
Error Checks - SCM Type:			
SCM ID:			
SCM Drainage Area Land Covers	Total Land Use Area Treated By All SCMs (ft ²)	Allowable Total Land Use Area to be Treated Based on Post-Project Areas (ft ²)	Post-Project Untreated Land Area (ft ²)
Roof	6,650	7,700	1,050
Roadway	5,725	6,775	1,050
Parking/Driveway/Sidewalk	3,350	3,575	225
Protected Forest	0	0	0
Managed Pervious/Landscaping	12,425	23,641	11,216
Offsite or Existing Roof	0	0	0
Offsite or Existing Roadway	0	0	0
Offsite or Existing Parking/Driveway/Sidew	0	0	0
Offsite Protected Forest	0	0	0
Offsite Managed Pervious	0	0	0
CUSTOM LAND COVER 1	0	0	0
CUSTOM LAND COVER 2	0	0	0
CUSTOM LAND COVER 3	0	0	0
LAND TAKEN UP BY SCM	1,600	1,600	0
TOTAL AREA DRAINING TO SCM (ft ²):	29,750	43,291	13,541

CATCHMENT AREA (ft²):

Nutrient Export Summary

Landcover & SCM Data Review

Errors / Advisories

Avg Annual precip (in) =	46.22	
Total (Regulated + Unregulated) Area (ft²) =	43,291	
Project (Regulated) Area (ft²) =	43,291	
Net BUA (Project Area BUA only ft ²) =	18,050	Net BUA indicates new development or expansion.
Custom Landcovers are present:	no	
Total Nitrogen Export Target Scaled to Project Area (lb/yr):		2.19

Nutrient Export Summary	Total Area (Onsite + Offsite) P <u>re-Project</u>	Project Area (Onsite Only) <u>Pre-Project</u>	Total Area Post-Project before Treatment	Project Area Post-Project before Treatment
Area (All Landcover Types) (acres)	0.9938	0.9938	0.9938	0.9938
Percent Built-Upon Area (BUA) (%)	0%	0%	42%	42%
Built-Upon Area (BUA) (sqft)	0	0	18,050	18,050
Annual Runoff Volume (ft ³ /yr)	7,503	7,503	69,086	69,086
Annual Runoff % Change			821%	821%
Total Runoff Change (cuft/yr)			61,582	61,582
Total Nitrogen EMC (mg/L)	2.48	2.48	1.45	1.45
Total Nitrogen Load Leaving Site (lb/yr)	1.16	1.16	6.24	6.24
Total Nitrogen Loading Rate (lb/ac/yr)	1.17	1.17	6.28	6.28
Total Nitrogen % Change Pre-to-Post			437%	437%
Total Nitrogen Change (lb/yr) Pre-to-Post			5.08	5.08
Total Phosphorus EMC (mg/L)	1.07	1.07	0.25	0.25
Total Phosphorus Load Leaving Site (lb/yr)	0.50	0.50	1.09	1.09
Total Phosphorus Loading Rate (lb/ac/yr)	0.50	0.50	1.10	1.10
Total Phosphorus % Change Pre-to-Post			118%	118%
Total Phosphorus Change (lb/yr)Pre-to-Post			0.59	0.59

SCM/Catchment Summary

SCM ID and Type	Volume Reduction (%)	TN Reduction (%)	TP Reduction (%)	TN Out (lbs/ac/yr)	TP Out (lbs/ac/yr)
Catchment 1	66.74%	80.97%	84.58%	1.47	0.19
101: Bioretention w/IWS	66.74%	80.97%	84.58%	1.47	0.19
102: NA	0.00%	0.00%	0.00%	0.00	0.00
103: NA	0.00%	0.00%	0.00%	0.00	0.00
Catchment 2	0.00%	0.00%	0.00%	0.00	0.00
201: NA	0.00%	0.00%	0.00%	0.00	0.00
202: NA	0.00%	0.00%	0.00%	0.00	0.00
203: NA	0.00%	0.00%	0.00%	0.00	0.00
Catchment 3	0.00%	0.00%	0.00%	0.00	0.00
301: NA	0.00%	0.00%	0.00%	0.00	0.00
302: NA	0.00%	0.00%	0.00%	0.00	0.00
303: NA	0.00%	0.00%	0.00%	0.00	0.00
Catchment 4	0.00%	0.00%	0.00%	0.00	0.00
401: NA	0.00%	0.00%	0.00%	0.00	0.00
402: NA	0.00%	0.00%	0.00%	0.00	0.00
403: NA	0.00%	0.00%	0.00%	0.00	0.00
Catchment 5	0.00%	0.00%	0.00%	0.00	0.00
501: NA	0.00%	0.00%	0.00%	0.00	0.00
502: NA	0.00%	0.00%	0.00%	0.00	0.00
503: NA	0.00%	0.00%	0.00%	0.00	0.00
Catchment 6	0.00%	0.00%	0.00%	0.00	0.00
601: NA	0.00%	0.00%	0.00%	0.00	0.00
602: NA	0.00%	0.00%	0.00%	0.00	0.00
603: NA	0.00%	0.00%	0.00%	0.00	0.00

Errors / Advisories

SCM Area (ft ²) =	1,600	
SCM Treated Area (ft ²) =	29,750	
Catchment Routing:	No errors	
Treating Runoff from Existing BUA or Offsite:		
Disturbed Area (ft²) = 43,291		
Total Phosphorus Export Target Scaled to Project Area (lb/yr):		0.33

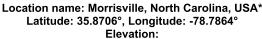
Total Area Post-Project after Treatment	Project Area Post-Project after Treatment	Total Area Post-Project SCM-Treated Area Only	Project Area Post-Project SCM-Treated Area Only	Total Area Post-Project Untreated Areas	Project Area Post-Project Untreated Areas
0.9938	0.9938	0.6830	0.6830	0.3109	0.3109
42%	42%	53%	53%	17%	17%
18,050	18,050	15,725	15,725	2,325	2,325
29,385	29,385	19,785	19,785	9,601	9,601
292%	292%				
21,882	21,882				
1.08	1.08	0.81	0.81	1.63	1.63
1.98	1.98	1.00	1.00	0.98	0.98
1.99	1.99	1.47	1.47	3.14	3.14
70%	70%				
0.82	0.82				
0.20	0.20	0.11	0.11	0.39	0.39
0.37	0.37	0.13	0.13	0.24	0.24
0.37	0.37	0.19	0.19	0.76	0.76
-27%	-27%				
-0.13	-0.13				

Falls Lake ONLY: Onsite Reduction Compliance Check

	Nitrogen	Phosphorus
Onsite % Reduction Requirement		
Export Target Scaled to Area (lb/yr)	2.19	0.33
Export Load Post-Project Before Treatment	6.24	1.09
Total Reduction Need (lb/yr)		
Onsite Reduction Need (lb/yr)		
Onsite Export Target (lb/yr)		
Project Area Post-Project After Treatment	1.98	0.37

APPENDIX E SUPPORTING DOCUMENTATION

NOAA Atlas 14, Volume 2, Version 3 RALEIGH **DURHAM WSFO AP** Station ID: 31-7069







POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M.Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PD	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹									nes) ¹
Duration				Avera	ge recurren	ce interval (years)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.394 (0.362-0.429)	0.461 (0.423-0.503)	0.530 (0.487-0.577)	0.587 (0.539-0.639)	0.647 (0.591-0.703)	0.689 (0.626-0.748)	0.727 (0.657-0.789)	0.758 (0.682-0.825)	0.792 (0.707-0.862)	0.819 (0.724-0.892)
10-min	0.630 (0.578-0.686)	0.738 (0.677-0.804)	0.848 (0.780-0.924)	0.939 (0.861-1.02)	1.03 (0.941-1.12)	1.10 (0.998-1.19)	1.16 (1.04-1.25)	1.20 (1.08-1.31)	1.25 (1.12-1.36)	1.29 (1.14-1.41)
15-min	0.787 (0.723-0.857)	0.927 (0.850-1.01)	1.07 (0.987-1.17)	1.19 (1.09-1.29)	1.31 (1.19-1.42)	1.39 (1.26-1.51)	1.46 (1.32-1.59)	1.52 (1.36-1.65)	1.58 (1.41-1.72)	1.62 (1.43-1.76)
30-min	1.08 (0.991-1.18)	1.28 (1.18-1.40)	1.53 (1.40-1.66)	1.72 (1.58-1.87)	1.94 (1.77-2.10)	2.09 (1.90-2.27)	2.24 (2.02-2.43)	2.36 (2.12-2.57)	2.51 (2.24-2.73)	2.62 (2.32-2.86)
60-min	1.35 (1.24-1.47)	1.61 (1.47-1.75)	1.96 (1.80-2.13)	2.24 (2.06-2.44)	2.58 (2.35-2.80)	2.84 (2.58-3.08)	3.08 (2.78-3.35)	3.31 (2.98-3.60)	3.60 (3.21-3.92)	3.83 (3.38-4.17)
2-hr	1.56 (1.42-1.71)	1.86 (1.71-2.04)	2.29 (2.09-2.51)	2.65 (2.40-2.90)	3.08 (2.78-3.36)	3.43 (3.09-3.74)	3.76 (3.36-4.11)	4.09 (3.64-4.46)	4.51 (3.97-4.92)	4.84 (4.23-5.29)
3-hr	1.65 (1.51-1.81)	1.98 (1.81-2.17)	2.44 (2.23-2.68)	2.84 (2.59-3.10)	3.33 (3.02-3.64)	3.75 (3.38-4.09)	4.15 (3.71-4.53)	4.56 (4.06-4.97)	5.11 (4.49-5.57)	5.55 (4.83-6.06)
6-hr	2.00 (1.84-2.18)	2.39 (2.20-2.61)	2.95 (2.72-3.22)	3.44 (3.15-3.74)	4.06 (3.70-4.40)	4.57 (4.14-4.96)	5.09 (4.57-5.51)	5.62 (5.00-6.08)	6.33 (5.56-6.85)	6.92 (6.01-7.50)
12-hr	2.37 (2.19-2.58)	2.84 (2.62-3.09)	3.52 (3.24-3.82)	4.11 (3.78-4.47)	4.89 (4.46-5.30)	5.56 (5.03-5.98)	6.22 (5.58-6.70)	6.93 (6.13-7.45)	7.88 (6.87-8.47)	8.69 (7.46-9.35)
24-hr	2.83 (2.65-3.04)	3.42 (3.20-3.67)	4.27 (3.99-4.58)	4.94 (4.61-5.29)	5.84 (5.43-6.25)	6.55 (6.08-7.01)	7.27 (6.73-7.80)	8.01 (7.39-8.60)	9.01 (8.28-9.69)	9.79 (8.97-10.6)
2-day	3.26 (3.04-3.50)	3.92 (3.66-4.22)	4.86 (4.53-5.23)	5.58 (5.19-6.00)	6.55 (6.08-7.05)	7.31 (6.76-7.86)	8.07 (7.45-8.70)	8.85 (8.14-9.54)	9.90 (9.06-10.7)	10.7 (9.77-11.6)
3-day	3.45 (3.22-3.70)	4.14 (3.86-4.44)	5.10 (4.76-5.48)	5.86 (5.46-6.29)	6.87 (6.38-7.38)	7.67 (7.11-8.24)	8.47 (7.83-9.12)	9.29 (8.55-10.0)	10.4 (9.53-11.2)	11.2 (10.3-12.1)
4-day	3.63 (3.40-3.90)	4.35 (4.07-4.67)	5.35 (5.00-5.73)	6.13 (5.73-6.58)	7.19 (6.69-7.72)	8.03 (7.45-8.61)	8.88 (8.21-9.54)	9.73 (8.97-10.5)	10.9 (9.99-11.7)	11.8 (10.8-12.7)
7-day	4.21 (3.96-4.50)	5.02 (4.72-5.36)	6.10 (5.73-6.51)	6.95 (6.52-7.42)	8.10 (7.57-8.65)	9.01 (8.40-9.63)	9.94 (9.23-10.6)	10.9 (10.1-11.7)	12.2 (11.2-13.1)	13.2 (12.1-14.2)
10-day	4.79 (4.50-5.11)	5.69 (5.35-6.07)	6.83 (6.41-7.29)	7.72 (7.24-8.23)	8.92 (8.35-9.52)	9.86 (9.20-10.5)	10.8 (10.1-11.6)	11.8 (10.9-12.6)	13.1 (12.1-14.0)	14.1 (12.9-15.1)
20-day	6.39 (6.01-6.82)	7.54 (7.09-8.04)	8.90 (8.36-9.50)	9.98 (9.36-10.7)	11.5 (10.7-12.2)	12.6 (11.8-13.5)	13.8 (12.8-14.8)	15.0 (13.9-16.0)	16.6 (15.3-17.8)	17.8 (16.3-19.2)
30-day	7.93 (7.48-8.44)	9.33 (8.78-9.92)	10.8 (10.2-11.5)	12.0 (11.3-12.8)	13.5 (12.7-14.4)	14.7 (13.8-15.7)	15.9 (14.8-17.0)	17.1 (15.9-18.2)	18.6 (17.3-20.0)	19.8 (18.3-21.3)
45-day	10.1 (9.61-10.7)	11.8 (11.3-12.5)	13.6 (12.9-14.3)	14.9 (14.1-15.7)	16.6 (15.7-17.5)	17.9 (16.9-18.9)	19.2 (18.1-20.4)	20.5 (19.2-21.7)	22.1 (20.7-23.5)	23.4 (21.8-24.9)
60-day	12.2 (11.6-12.8)	14.2 (13.5-14.9)	16.0 (15.2-16.8)	17.4 (16.5-18.3)	19.2 (18.2-20.2)	20.5 (19.4-21.7)	21.8 (20.6-23.1)	23.1 (21.8-24.4)	24.7 (23.2-26.2)	25.9 (24.3-27.5)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

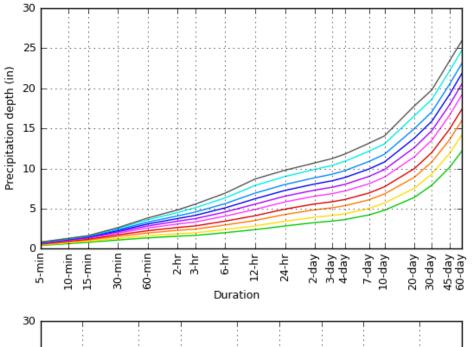
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

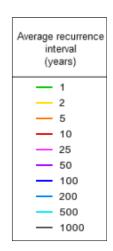
Please refer to NOAA Atlas 14 document for more information.

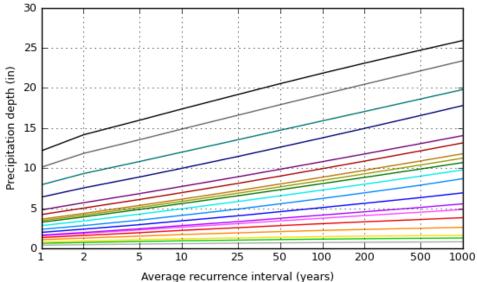
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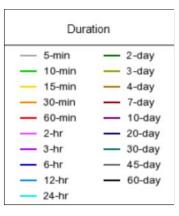
PF graphical

PDS-based depth-duration-frequency (DDF) curves Latitude: 35.8706°, Longitude: -78.7864°









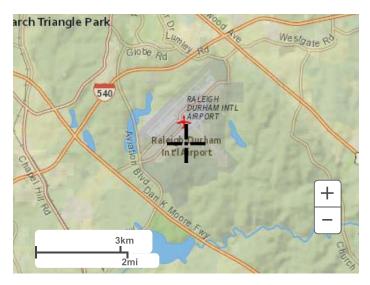
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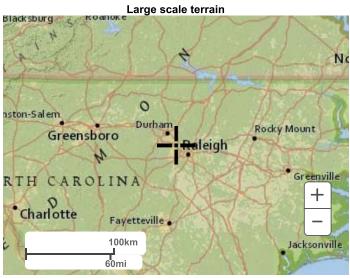
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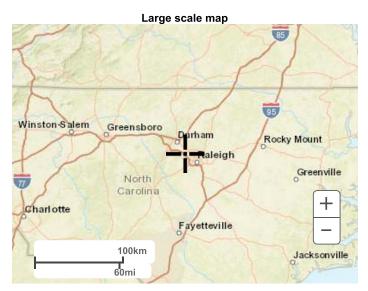
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Maps & aerials

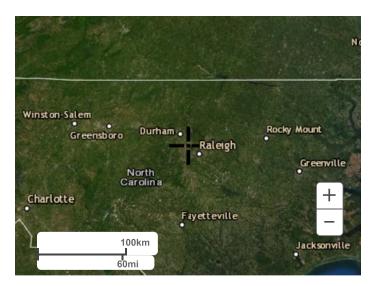
Small scale terrain







Large scale aerial



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US Department of Commerce

National Oceanic and Atmospheric Administration

National Weather Service
National Water Center

1325 East West Highway
Silver Spring, MD 20910

Questions?: HDSC.Questions@noaa.gov

Disclaimer

Table 2-2a Runoff curve numbers for urban areas 1/2

Cover description	Curve numbers forhydrologic soil group				
	Average percent				
Cover type and hydrologic condition	impervious area 2/	A	В	С	D
Fully developed urban areas (vegetation established)					
Open space (lawns, parks, golf courses, cemeteries, etc.) 3/:					
Poor condition (grass cover < 50%)		68	79	86	89
Fair condition (grass cover 50% to 75%)	•••••	49	69	7 9	84
Good condition (grass cover > 75%)		39	61	74	80
Impervious areas:					
Paved parking lots, roofs, driveways, etc.					
(excluding right-of-way)		98	98	98	98
Streets and roads:					
Paved; curbs and storm sewers (excluding					
right-of-way)		98	98	98	98
Paved; open ditches (including right-of-way)		83	89	92	93
Gravel (including right-of-way)		76	85	89	91
Dirt (including right-of-way)	•••••	72	82	87	89
Western desert urban areas:					
Natural desert landscaping (pervious areas only) 4/		63	77	85	88
Artificial desert landscaping (impervious weed barrier,					
desert shrub with 1- to 2-inch sand or gravel mulch					
and basin borders)		96	96	96	96
Urban districts:					
Commercial and business	85	89	92	94	95
Industrial	72	81	88	91	93
Residential districts by average lot size:					
1/8 acre or less (town houses)	65	77	85	90	92
1/4 acre		61	75	83	87
1/3 acre	30	57	72	81	86
1/2 acre	25	54	70	80	85
1 acre	20	51	68	79	84
2 acres		46	65	77	82
Developing urban areas					
Newly graded areas			0.0	0.4	
(pervious areas only, no vegetation) 5/		77	86	91	94
Idle lands (CN's are determined using cover types					
similar to those in table 2-2c).					

 $^{^{\}rm 1}\,$ Average runoff condition, and I_a = 0.2S.

² The average percent impervious area shown was used to develop the composite CN's. Other assumptions are as follows: impervious areas are directly connected to the drainage system, impervious areas have a CN of 98, and pervious areas are considered equivalent to open space in good hydrologic condition. CN's for other combinations of conditions may be computed using figure 2-3 or 2-4.

³ CN's shown are equivalent to those of pasture. Composite CN's may be computed for other combinations of open space cover type.

⁴ Composite CN's for natural desert landscaping should be computed using figures 2-3 or 2-4 based on the impervious area percentage (CN = 98) and the pervious area CN. The pervious area CN's are assumed equivalent to desert shrub in poor hydrologic condition.

⁵ Composite CN's to use for the design of temporary measures during grading and construction should be computed using figure 2-3 or 2-4 based on the degree of development (impervious area percentage) and the CN's for the newly graded pervious areas.

Table 2-2c Runoff curve numbers for other agricultural lands [⊥]

Cover description		Curve numbers for hydrologic soil group			
Cover type	Hydrologic condition	A	В	С	D
Pasture, grassland, or range—continuous	Poor	68	79	86	89
forage for grazing. 2/	Fair Good	49 39	69 61	79 74	84 80
Meadow—continuous grass, protected from grazing and generally mowed for hay.	_	30	58	71	78
Brush—brush-weed-grass mixture with brush the major element. 3/	Poor Fair Good	48 35 30 4/	67 56 48	77 70 65	83 77 73
Woods—grass combination (orchard or tree farm). 5/	Poor Fair Good	57 43 32	73 65 58	82 76 72	86 82 79
Woods. 6/	Poor Fair Good	45 36 30 4/	66 60 55	77 73 70	83 79 77
Farmsteads—buildings, lanes, driveways, and surrounding lots.	_	59	74	82	86

¹ Average runoff condition, and $I_a = 0.2S$.

² *Poor:* <50%) ground cover or heavily grazed with no mulch.

Fair: 50 to 75% ground cover and not heavily grazed.

Good: > 75% ground cover and lightly or only occasionally grazed.

³ *Poor*: <50% ground cover.

Fair: 50 to 75% ground cover.

Good: >75% ground cover.

 $^{^4}$ $\,$ Actual curve number is less than 30; use CN = 30 for runoff computations.

⁵ CN's shown were computed for areas with 50% woods and 50% grass (pasture) cover. Other combinations of conditions may be computed from the CN's for woods and pasture.

⁶ Poor: Forest litter, small trees, and brush are destroyed by heavy grazing or regular burning.

Fair: Woods are grazed but not burned, and some forest litter covers the soil.

Good: Woods are protected from grazing, and litter and brush adequately cover the soil.