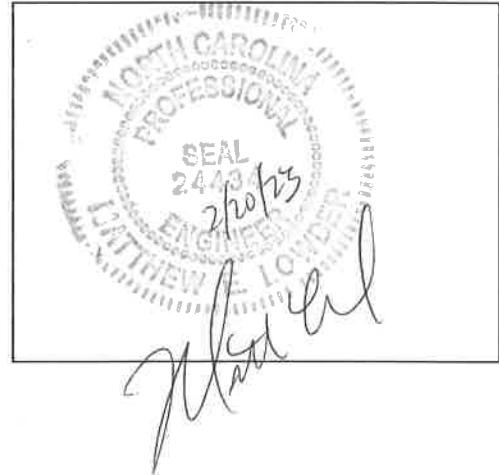


*Storm Water & Erosion Control  
Design Calculations*

*February 20, 2023*

Tractor Supply  
Old US Highway 264  
Zebulon, NC  
Wake County

Prepared for:  
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FIRM# F-1445

**Bowman**

## OVERVIEW

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SOILS SURVEY & SOIL INFORMATION  
USGS TOPOGRAPHIC MAP  
FEMA FIRM MAP  
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SURFACE WATER CLASSIFICATIONS  
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DOWNSTREAM IMPACT ANALYSIS

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100 SYSTEM  
200 SYSTEM  
400 SYSTEM

### EROSION CONTROL CALCULATIONS

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DRAINAGE AREA MAP  
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## OVERVIEW

### Background

This report contains the storm water management and erosion control calculations for the proposed Tractor Supply retail site. The project site is located on Old US Highway 264, Zebulon in Wake County and is undeveloped open and wooded area. The proposed project site consists of 3.766 acres and approximately 5.69 acres will be disturbed as part of this project for the construction of the site improvements.

The development of the site will result in an impervious area of 109,774sf (2.52 ac - 66.91% impervious).

The proposed parcel is not located within a FEMA designated flood zone as shown on FEMA FIRM Panel 3720270500K with an effective date of July 19, 2022

There are no wetland features on the proposed property.

There are proposed storm water management facilities (wet pond and level spreader-filter strip) on site. The design includes the Tractor Supply site (164,059 sf-3.766 ac) and the 2.52 ac parcel to the west and assumes 80% impervious (90,769 sf-2.08 ac). The SCM outlined in this report has been designed for post-development peak attenuation and water quality. The SCM is designed to capture a drainage area of 5.57 ac with an impervious area of 4.62 ac. A level spreader-filter strip will be used as a secondary SCM receiving the 1.0" storm from the stormwater wetland pond, and it will be adjacent to a riparian buffer. The level spreader is designed to treat a 0.75" storm event. The outlet control structure has been designed so that only the 1" stormwater runoff is discharging to the level spreader-filter strip. The site grading and storm drainage systems are designed to convey stormwater runoff from the impervious areas of the site to the wet pond and level spreader-filter strip. The site is not located within a coastal county, therefore the design storm for water quality is a 1.0" storm event. The SCMs are designed per the Town of Zebulon stormwater UDO.

A downstream impact analysis is included per the 10% rule. The StreamStats analysis point has a drainage area of approximately 50.2 acres, a little less than 10% of the proposed development drainage area, and a 10-year peak flood flow of 64.8 cfs. The Pre-Developed flow for the 10-year storm event is 15.39 cfs (per hydrographs). The Post-Developed to Pond flow for the 10-year storm event of the site going through the SCM is 14.526 cfs (per hydrographs). The difference in flow is 0.864 cfs. This incorporates the proposed development. Since the 10-yr storm event is being attenuated through the wet pond, there is a net decrease in peak

flow from the pre-developed to post-developed condition. Therefore, there will be no impacts downstream.

#### Erosion Control

Erosion control measures have been designed in accordance with Wake County and NCDEQ erosion control standards and regulations to minimize sediment laden runoff from exiting the site. Silt fence will be installed along the low sides of the site prior to construction. The construction entrance will be installed prior to construction commencing. Two skimmer basins will be used to treat stormwater runoff prior to leaving the site. Skimmer basin #1 has been designed to include the entire drainage area, including when the post-developed conditions have been constructed. Skimmer basin #2 will be removed when the drainage system has been constructed. Accumulated sediment within the project site will need to be removed and the pond constructed to final design conditions prior to final acceptance of the project.

#### Soils

The County Soils Survey indicates that Vance and Helena Sandy Loam soils are present on the site.

#### Site Stabilization

After final grading is completed, permanent vegetation shall be applied in accordance with the seeding requirements and landscape plan for this site.

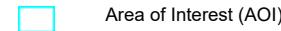
## Hydrologic Soil Group—Wake County, North Carolina



Natural Resources  
Conservation Service

Web Soil Survey  
National Cooperative Soil Survey

4/11/2022  
Page 1 of 4

**MAP LEGEND****Area of Interest (AOI)****Soils****Soil Rating Polygons**

	A
	A/D
	B
	B/D
	C
	C/D
	D
	Not rated or not available

**Soil Rating Lines**

	A
	A/D
	B
	B/D
	C
	C/D
	D
	Not rated or not available

**Soil Rating Points**

	A
	A/D
	B
	B/D

**C****C/D****D****Not rated or not available****Water Features****Streams and Canals****Transportation****Rails****Interstate Highways****US Routes****Major Roads****Local Roads****Background****Aerial Photography****MAP INFORMATION**

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Wake County, North Carolina

Survey Area Data: Version 22, Jan 21, 2022

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Oct 22, 2018—Oct 25, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.



## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
ChA	Chewacla and Wehadkee soils, 0 to 2 percent slopes, frequently flooded	B/D	1.8	5.2%
HeB	Helena sandy loam, 2 to 6 percent slopes	D	3.5	10.0%
Ur	Urban land		2.0	5.7%
VaB	Vance sandy loam, 2 to 6 percent slopes	D	13.2	37.7%
VaC	Vance sandy loam, 6 to 10 percent slopes	D	14.5	41.5%
<b>Totals for Area of Interest</b>			<b>35.1</b>	<b>100.0%</b>

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

**Group A.** Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

**Group B.** Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

**Group C.** Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

**Group D.** Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff:* None Specified

*Tie-break Rule:* Higher

1 Mile

5000 Feet

Scale 1:15840

(Joins sheet 43)

0

1,000

2,000

3,000

4,000

5,000

6,000

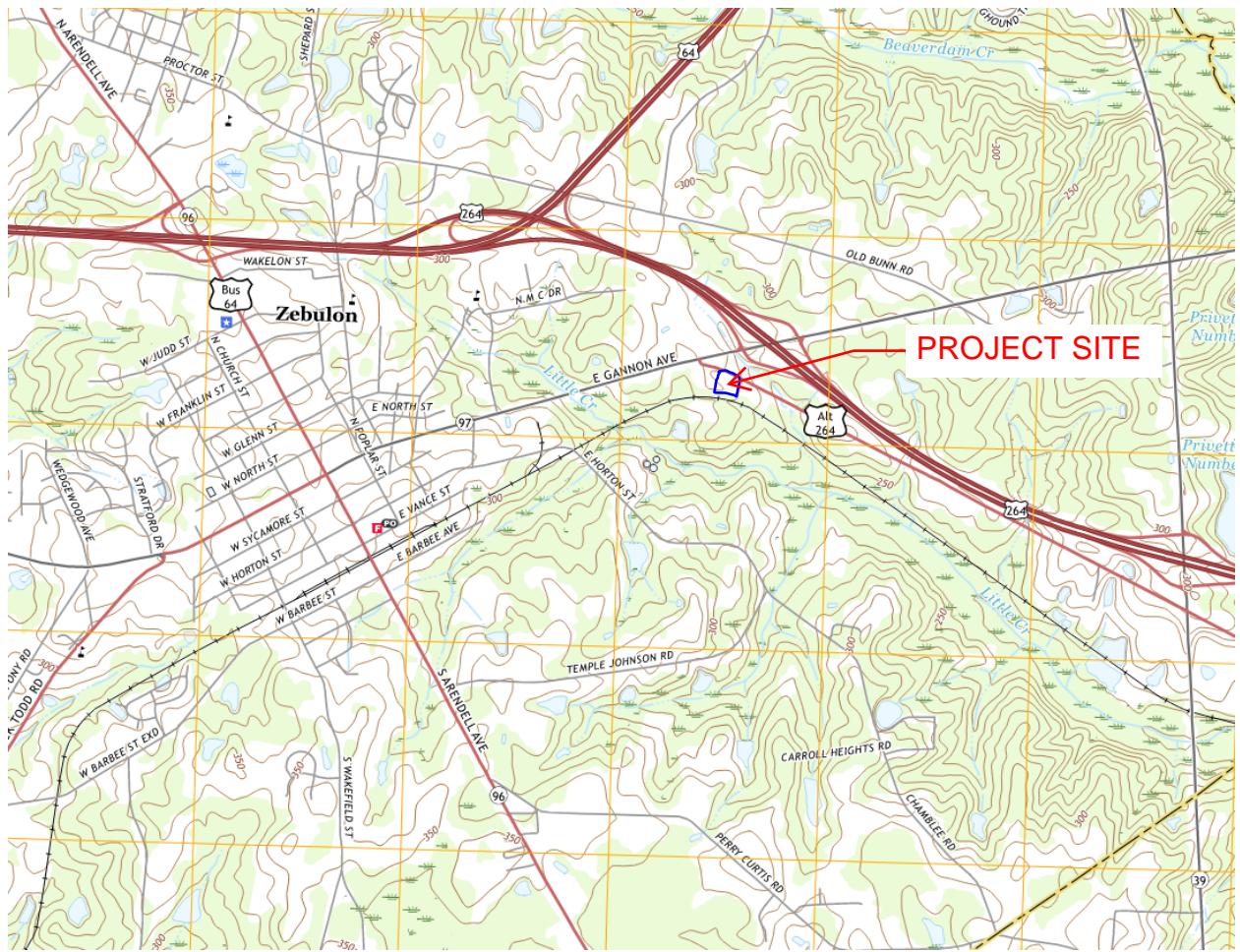
7,000

8,000

9,000

10,000





# National Flood Hazard Layer FIRMette



78°17'58"W 35°49'57"N



## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

### SPECIAL FLOOD HAZARD AREAS

	Without Base Flood Elevation (BFE) Zone A, V, A99
	With BFE or Depth Zone AE, AO, AH, VE, AR
	Regulatory Floodway

**0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile** Zone X

**Future Conditions 1% Annual Chance Flood Hazard** Zone X

**Area with Reduced Flood Risk due to Levee. See Notes.** Zone X

**Area with Flood Risk due to Levee** Zone D

### OTHER AREAS OF FLOOD HAZARD

**NO SCREEN** Area of Minimal Flood Hazard Zone X  
**Effective LOMRs**

**Area of Undetermined Flood Hazard** Zone D

### OTHER AREAS

**Channel, Culvert, or Storm Sewer**  
**Levee, Dike, or Floodwall**

### GENERAL STRUCTURES

**Cross Sections with 1% Annual Chance**  
**Water Surface Elevation**

**Coastal Transect**

**Base Flood Elevation Line (BFE)**

**Limit of Study**

**Jurisdiction Boundary**

**Coastal Transect Baseline**

**Profile Baseline**

**Hydrographic Feature**

### OTHER FEATURES

**Digital Data Available**

**No Digital Data Available**

**Unmapped**

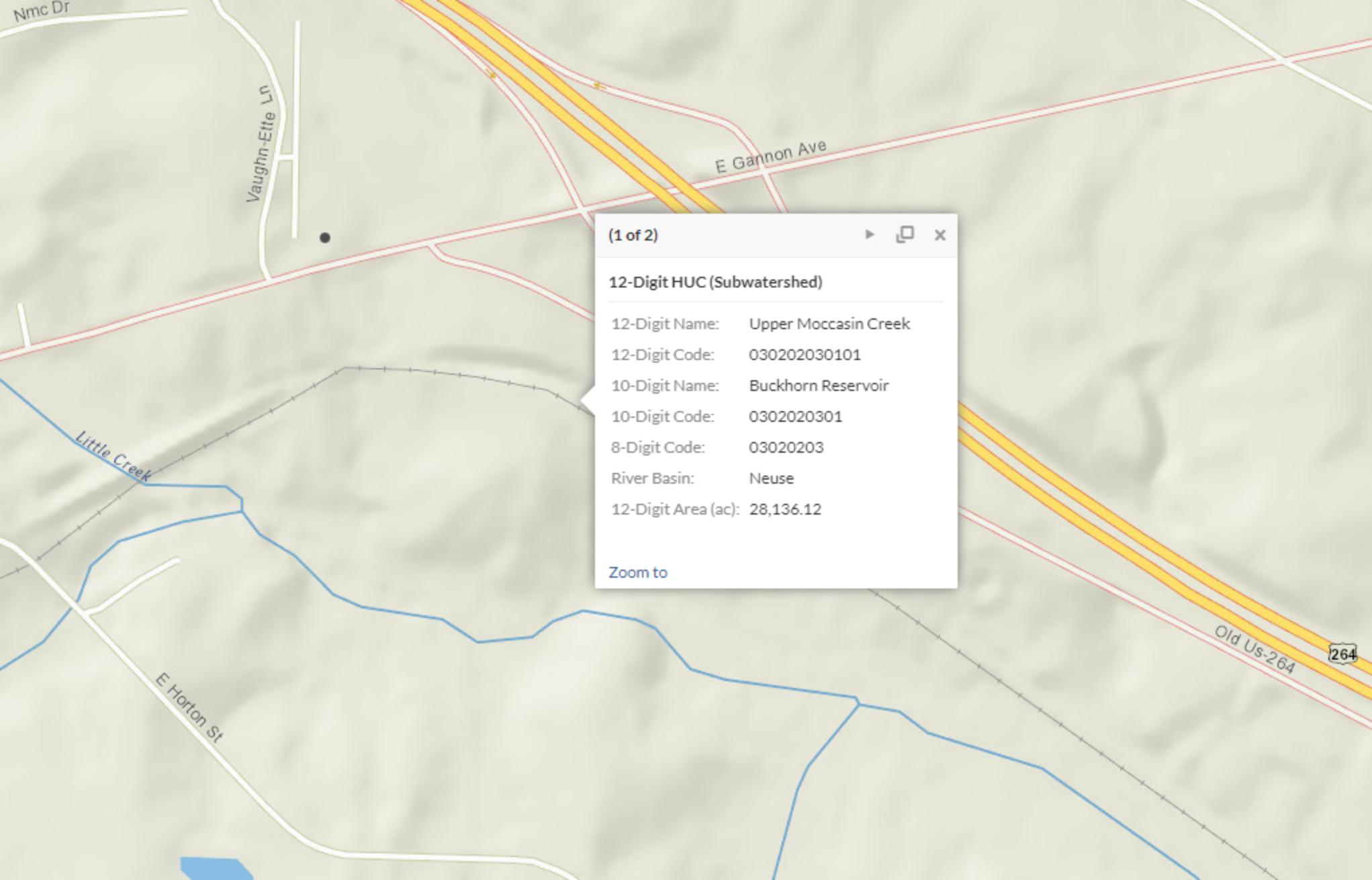


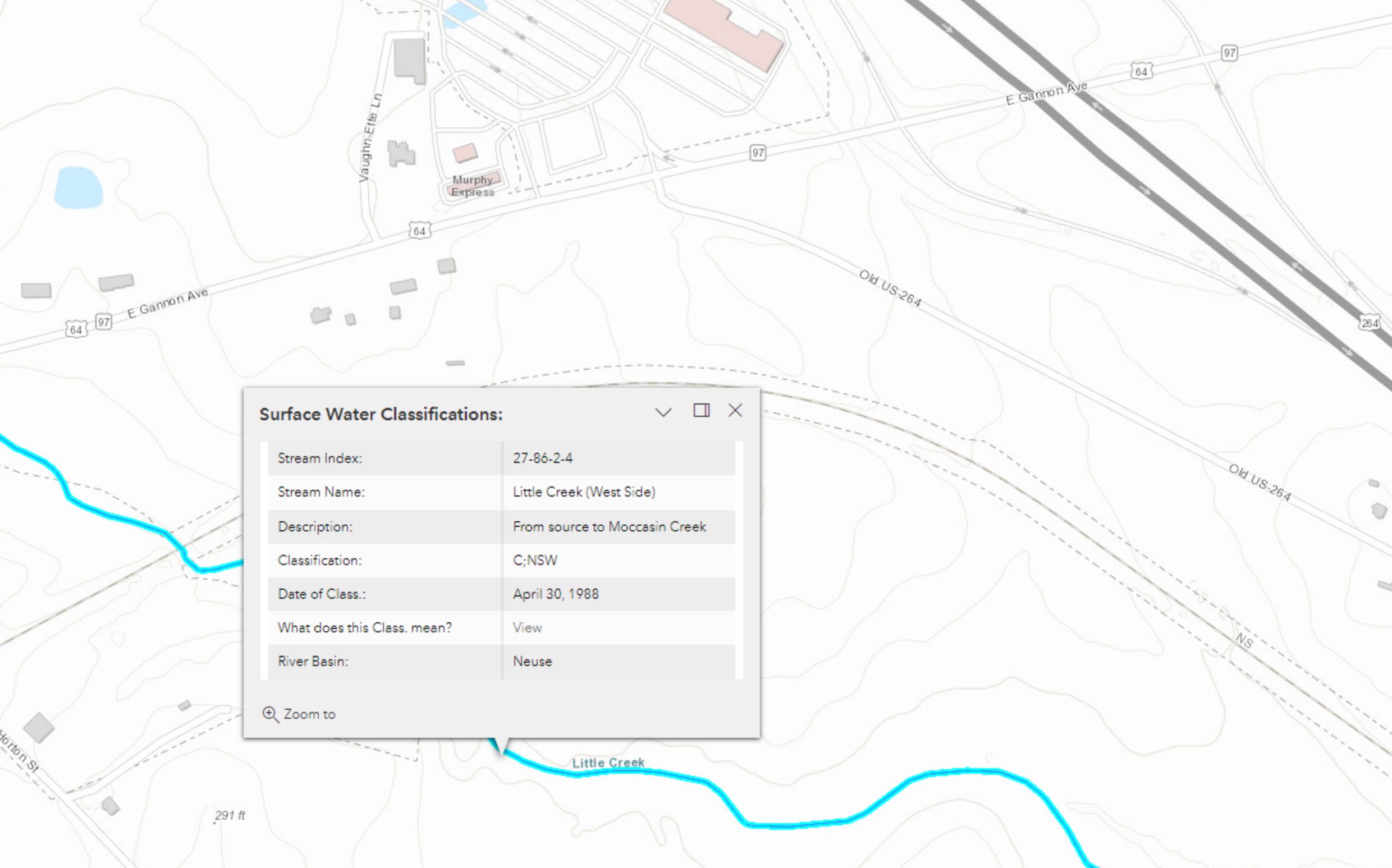
The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 1/5/2023 at 12:57 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.







**NOAA Atlas 14, Volume 2, Version 3**  
**Location name: Zebulon, North Carolina, USA\***  
**Latitude: 35.8183°, Longitude: -78.3283°**  
**Elevation: 326.74 ft\*\***

\* source: ESRI Maps

\*\* source: USGS



### POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

### PF tabular

<b>Duration</b>	<b>Average recurrence interval (years)</b>									
	<b>1</b>	<b>2</b>	<b>5</b>	<b>10</b>	<b>25</b>	<b>50</b>	<b>100</b>	<b>200</b>	<b>500</b>	<b>1000</b>
<b>5-min</b>	<b>0.406</b> (0.370-0.445)	<b>0.469</b> (0.429-0.513)	<b>0.532</b> (0.487-0.582)	<b>0.602</b> (0.549-0.658)	<b>0.672</b> (0.610-0.733)	<b>0.729</b> (0.660-0.797)	<b>0.781</b> (0.702-0.852)	<b>0.828</b> (0.740-0.905)	<b>0.881</b> (0.781-0.964)	<b>0.932</b> (0.819-1.02)
<b>10-min</b>	<b>0.648</b> (0.591-0.711)	<b>0.750</b> (0.686-0.821)	<b>0.852</b> (0.779-0.932)	<b>0.963</b> (0.879-1.05)	<b>1.07</b> (0.972-1.17)	<b>1.16</b> (1.05-1.27)	<b>1.24</b> (1.12-1.35)	<b>1.31</b> (1.17-1.44)	<b>1.39</b> (1.24-1.53)	<b>1.47</b> (1.29-1.61)
<b>15-min</b>	<b>0.810</b> (0.739-0.889)	<b>0.943</b> (0.863-1.03)	<b>1.08</b> (0.986-1.18)	<b>1.22</b> (1.11-1.33)	<b>1.36</b> (1.23-1.48)	<b>1.47</b> (1.33-1.61)	<b>1.57</b> (1.41-1.71)	<b>1.66</b> (1.48-1.81)	<b>1.75</b> (1.56-1.92)	<b>1.84</b> (1.62-2.02)
<b>30-min</b>	<b>1.11</b> (1.01-1.22)	<b>1.30</b> (1.19-1.43)	<b>1.53</b> (1.40-1.68)	<b>1.77</b> (1.61-1.93)	<b>2.01</b> (1.83-2.19)	<b>2.22</b> (2.00-2.42)	<b>2.40</b> (2.16-2.62)	<b>2.58</b> (2.30-2.82)	<b>2.79</b> (2.48-3.06)	<b>2.98</b> (2.62-3.27)
<b>60-min</b>	<b>1.38</b> (1.26-1.52)	<b>1.63</b> (1.50-1.79)	<b>1.96</b> (1.80-2.15)	<b>2.30</b> (2.10-2.51)	<b>2.68</b> (2.43-2.92)	<b>3.00</b> (2.72-3.28)	<b>3.31</b> (2.98-3.61)	<b>3.62</b> (3.23-3.95)	<b>4.01</b> (3.55-4.38)	<b>4.35</b> (3.83-4.78)
<b>2-hr</b>	<b>1.62</b> (1.47-1.79)	<b>1.92</b> (1.75-2.11)	<b>2.33</b> (2.12-2.57)	<b>2.77</b> (2.51-3.04)	<b>3.28</b> (2.95-3.60)	<b>3.75</b> (3.36-4.11)	<b>4.20</b> (3.74-4.60)	<b>4.67</b> (4.13-5.12)	<b>5.30</b> (4.64-5.80)	<b>5.87</b> (5.10-6.44)
<b>3-hr</b>	<b>1.71</b> (1.55-1.91)	<b>2.03</b> (1.85-2.25)	<b>2.48</b> (2.26-2.75)	<b>2.97</b> (2.69-3.27)	<b>3.55</b> (3.20-3.91)	<b>4.09</b> (3.66-4.50)	<b>4.63</b> (4.11-5.09)	<b>5.21</b> (4.58-5.72)	<b>5.98</b> (5.21-6.58)	<b>6.72</b> (5.78-7.40)
<b>6-hr</b>	<b>2.05</b> (1.87-2.27)	<b>2.44</b> (2.23-2.69)	<b>2.98</b> (2.71-3.28)	<b>3.56</b> (3.24-3.92)	<b>4.28</b> (3.86-4.69)	<b>4.95</b> (4.44-5.42)	<b>5.63</b> (5.00-6.16)	<b>6.35</b> (5.59-6.94)	<b>7.35</b> (6.38-8.02)	<b>8.29</b> (7.10-9.08)
<b>12-hr</b>	<b>2.42</b> (2.21-2.67)	<b>2.87</b> (2.63-3.15)	<b>3.52</b> (3.22-3.87)	<b>4.24</b> (3.85-4.65)	<b>5.13</b> (4.63-5.61)	<b>5.97</b> (5.35-6.51)	<b>6.83</b> (6.06-7.44)	<b>7.77</b> (6.81-8.45)	<b>9.07</b> (7.83-9.87)	<b>10.3</b> (8.77-11.2)
<b>24-hr</b>	<b>2.86</b> (2.65-3.09)	<b>3.46</b> (3.21-3.75)	<b>4.39</b> (4.07-4.75)	<b>5.15</b> (4.76-5.57)	<b>6.21</b> (5.71-6.71)	<b>7.08</b> (6.49-7.66)	<b>8.01</b> (7.30-8.66)	<b>9.00</b> (8.15-9.74)	<b>10.4</b> (9.34-11.3)	<b>11.6</b> (10.3-12.6)
<b>2-day</b>	<b>3.31</b> (3.07-3.57)	<b>3.99</b> (3.71-4.31)	<b>5.02</b> (4.66-5.43)	<b>5.86</b> (5.43-6.33)	<b>7.03</b> (6.48-7.59)	<b>7.99</b> (7.33-8.62)	<b>9.00</b> (8.21-9.73)	<b>10.1</b> (9.14-10.9)	<b>11.6</b> (10.4-12.6)	<b>12.9</b> (11.4-14.0)
<b>3-day</b>	<b>3.51</b> (3.27-3.78)	<b>4.23</b> (3.94-4.55)	<b>5.30</b> (4.93-5.70)	<b>6.15</b> (5.71-6.62)	<b>7.36</b> (6.80-7.91)	<b>8.34</b> (7.67-8.97)	<b>9.37</b> (8.57-10.1)	<b>10.5</b> (9.51-11.3)	<b>12.0</b> (10.8-13.0)	<b>13.3</b> (11.9-14.4)
<b>4-day</b>	<b>3.72</b> (3.47-3.99)	<b>4.47</b> (4.17-4.79)	<b>5.57</b> (5.19-5.97)	<b>6.45</b> (6.00-6.91)	<b>7.68</b> (7.11-8.23)	<b>8.69</b> (8.01-9.32)	<b>9.74</b> (8.93-10.5)	<b>10.8</b> (9.89-11.7)	<b>12.4</b> (11.2-13.4)	<b>13.7</b> (12.3-14.8)
<b>7-day</b>	<b>4.32</b> (4.04-4.62)	<b>5.17</b> (4.83-5.53)	<b>6.36</b> (5.94-6.81)	<b>7.32</b> (6.82-7.83)	<b>8.65</b> (8.04-9.26)	<b>9.72</b> (8.99-10.4)	<b>10.8</b> (9.98-11.6)	<b>12.0</b> (11.0-12.9)	<b>13.6</b> (12.4-14.7)	<b>15.0</b> (13.5-16.2)
<b>10-day</b>	<b>4.93</b> (4.62-5.26)	<b>5.88</b> (5.51-6.27)	<b>7.13</b> (6.68-7.60)	<b>8.12</b> (7.59-8.65)	<b>9.48</b> (8.84-10.1)	<b>10.6</b> (9.82-11.3)	<b>11.7</b> (10.8-12.5)	<b>12.8</b> (11.8-13.7)	<b>14.4</b> (13.2-15.5)	<b>15.7</b> (14.3-16.9)
<b>20-day</b>	<b>6.61</b> (6.22-7.04)	<b>7.83</b> (7.37-8.34)	<b>9.34</b> (8.78-9.94)	<b>10.5</b> (9.89-11.2)	<b>12.2</b> (11.4-13.0)	<b>13.5</b> (12.6-14.4)	<b>14.8</b> (13.8-15.8)	<b>16.2</b> (15.0-17.3)	<b>18.0</b> (16.6-19.3)	<b>19.5</b> (17.8-20.9)
<b>30-day</b>	<b>8.21</b> (7.75-8.72)	<b>9.68</b> (9.14-10.3)	<b>11.4</b> (10.7-12.1)	<b>12.7</b> (11.9-13.5)	<b>14.4</b> (13.5-15.3)	<b>15.8</b> (14.8-16.8)	<b>17.2</b> (16.0-18.2)	<b>18.5</b> (17.2-19.7)	<b>20.4</b> (18.9-21.8)	<b>21.8</b> (20.1-23.3)
<b>45-day</b>	<b>10.4</b> (9.91-11.0)	<b>12.3</b> (11.6-13.0)	<b>14.2</b> (13.4-15.0)	<b>15.6</b> (14.8-16.5)	<b>17.6</b> (16.6-18.6)	<b>19.1</b> (18.0-20.1)	<b>20.5</b> (19.3-21.7)	<b>22.0</b> (20.6-23.3)	<b>23.9</b> (22.3-25.4)	<b>25.4</b> (23.6-27.0)
<b>60-day</b>	<b>12.5</b> (11.9-13.2)	<b>14.7</b> (13.9-15.4)	<b>16.8</b> (15.9-17.6)	<b>18.4</b> (17.4-19.4)	<b>20.5</b> (19.4-21.6)	<b>22.1</b> (20.8-23.3)	<b>23.6</b> (22.2-24.9)	<b>25.1</b> (23.6-26.6)	<b>27.1</b> (25.4-28.8)	<b>28.6</b> (26.7-30.4)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

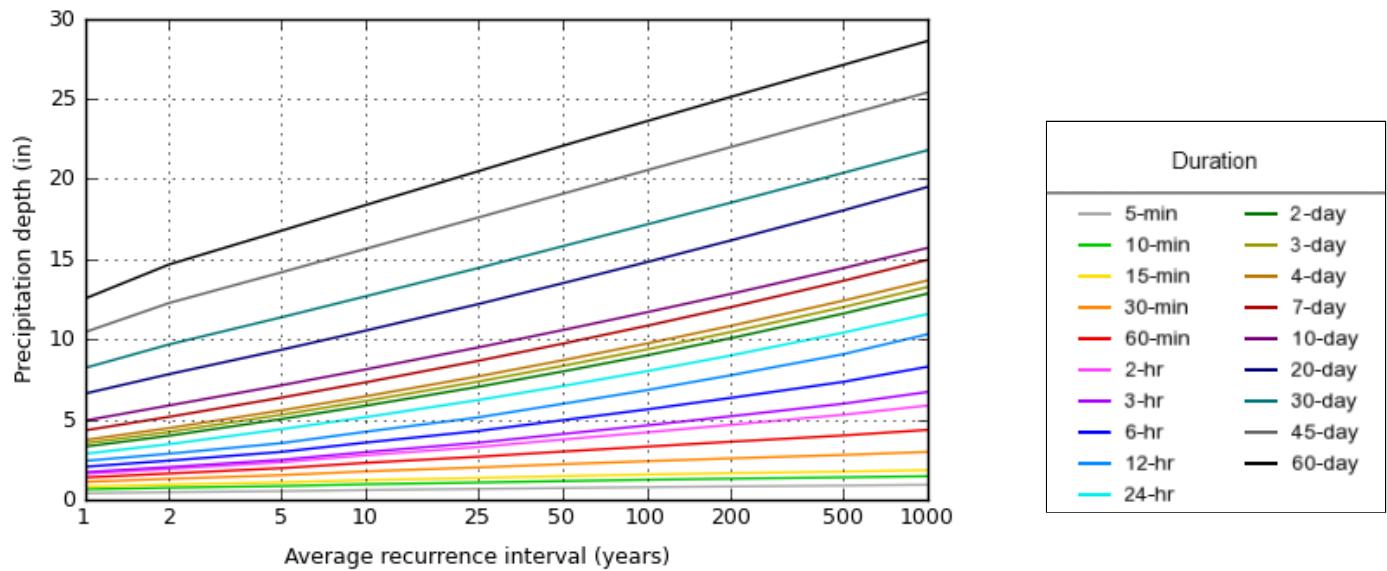
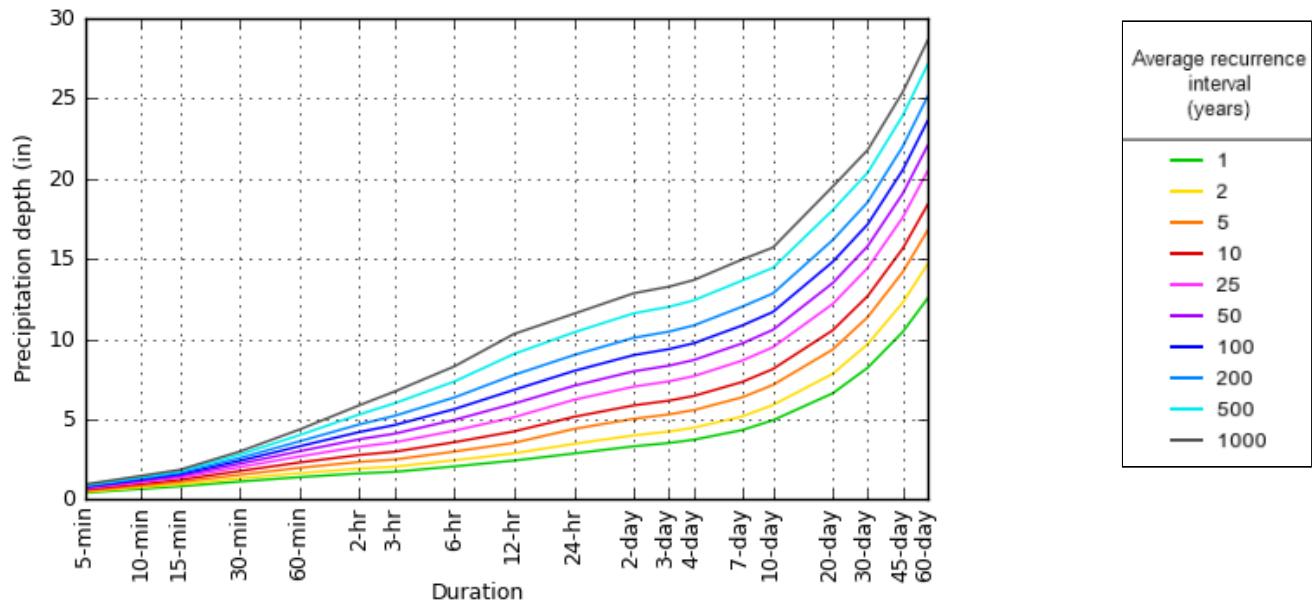
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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### PF graphical

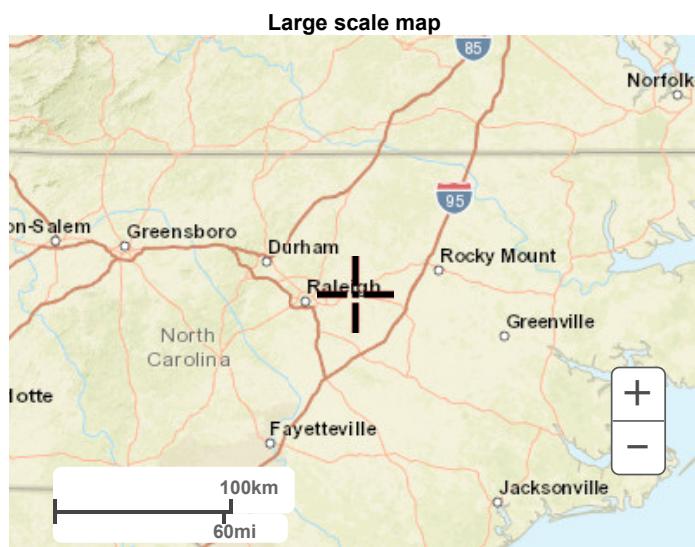
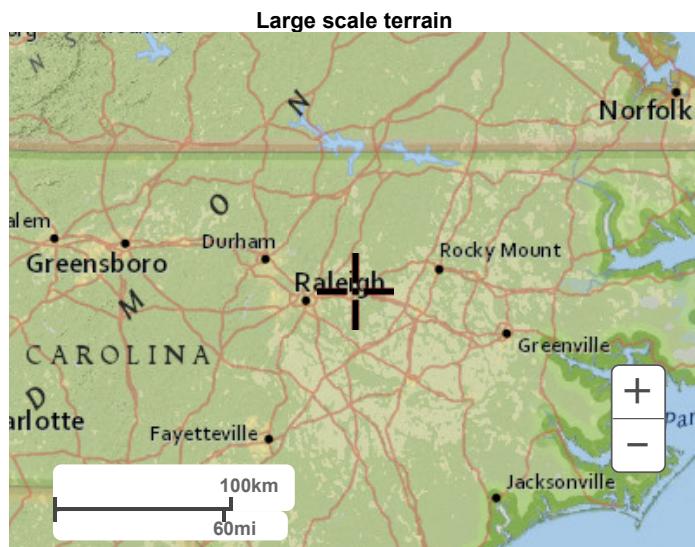
PDS-based depth-duration-frequency (DDF) curves  
Latitude: 35.8183°, Longitude: -78.3283°



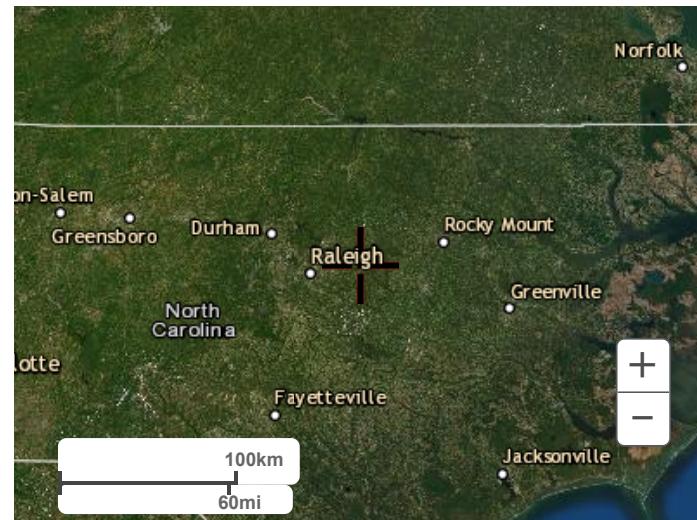
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**NOAA Atlas 14, Volume 2, Version 3**  
**Location name: Zebulon, North Carolina, USA\***  
**Latitude: 35.8183°, Longitude: -78.3283°**  
**Elevation: 326.74 ft\*\***

\* source: ESRI Maps

\*\* source: USGS



### POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

#### PF tabular

Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	<b>4.87</b> (4.44-5.34)	<b>5.63</b> (5.15-6.16)	<b>6.38</b> (5.84-6.98)	<b>7.22</b> (6.59-7.90)	<b>8.06</b> (7.32-8.80)	<b>8.75</b> (7.92-9.56)	<b>9.37</b> (8.42-10.2)	<b>9.94</b> (8.88-10.9)	<b>10.6</b> (9.37-11.6)	<b>11.2</b> (9.83-12.3)
10-min	<b>3.89</b> (3.55-4.27)	<b>4.50</b> (4.12-4.93)	<b>5.11</b> (4.67-5.59)	<b>5.78</b> (5.27-6.32)	<b>6.42</b> (5.83-7.01)	<b>6.97</b> (6.31-7.61)	<b>7.45</b> (6.70-8.12)	<b>7.88</b> (7.04-8.61)	<b>8.36</b> (7.42-9.16)	<b>8.80</b> (7.74-9.65)
15-min	<b>3.24</b> (2.96-3.56)	<b>3.77</b> (3.45-4.13)	<b>4.31</b> (3.94-4.72)	<b>4.87</b> (4.44-5.33)	<b>5.43</b> (4.93-5.92)	<b>5.88</b> (5.32-6.43)	<b>6.27</b> (5.64-6.85)	<b>6.62</b> (5.92-7.24)	<b>7.02</b> (6.22-7.68)	<b>7.37</b> (6.48-8.08)
30-min	<b>2.22</b> (2.03-2.44)	<b>2.60</b> (2.38-2.85)	<b>3.06</b> (2.80-3.35)	<b>3.53</b> (3.22-3.86)	<b>4.02</b> (3.65-4.39)	<b>4.43</b> (4.01-4.84)	<b>4.80</b> (4.32-5.24)	<b>5.16</b> (4.61-5.64)	<b>5.58</b> (4.95-6.11)	<b>5.96</b> (5.24-6.54)
60-min	<b>1.38</b> (1.26-1.52)	<b>1.63</b> (1.50-1.79)	<b>1.96</b> (1.80-2.15)	<b>2.30</b> (2.10-2.51)	<b>2.68</b> (2.43-2.92)	<b>3.00</b> (2.72-3.28)	<b>3.31</b> (2.98-3.61)	<b>3.62</b> (3.23-3.95)	<b>4.01</b> (3.55-4.38)	<b>4.35</b> (3.83-4.78)
2-hr	<b>0.809</b> (0.733-0.896)	<b>0.958</b> (0.873-1.05)	<b>1.17</b> (1.06-1.28)	<b>1.39</b> (1.25-1.52)	<b>1.64</b> (1.48-1.80)	<b>1.87</b> (1.68-2.05)	<b>2.10</b> (1.87-2.30)	<b>2.34</b> (2.07-2.56)	<b>2.65</b> (2.32-2.90)	<b>2.93</b> (2.55-3.22)
3-hr	<b>0.571</b> (0.517-0.634)	<b>0.677</b> (0.617-0.749)	<b>0.827</b> (0.751-0.914)	<b>0.988</b> (0.895-1.09)	<b>1.18</b> (1.06-1.30)	<b>1.36</b> (1.22-1.50)	<b>1.54</b> (1.37-1.70)	<b>1.73</b> (1.53-1.91)	<b>1.99</b> (1.74-2.19)	<b>2.24</b> (1.93-2.47)
6-hr	<b>0.343</b> (0.312-0.380)	<b>0.407</b> (0.372-0.449)	<b>0.497</b> (0.453-0.548)	<b>0.595</b> (0.540-0.654)	<b>0.715</b> (0.645-0.784)	<b>0.827</b> (0.741-0.906)	<b>0.940</b> (0.835-1.03)	<b>1.06</b> (0.933-1.16)	<b>1.23</b> (1.07-1.34)	<b>1.38</b> (1.19-1.52)
12-hr	<b>0.201</b> (0.183-0.221)	<b>0.238</b> (0.218-0.262)	<b>0.292</b> (0.267-0.321)	<b>0.352</b> (0.320-0.386)	<b>0.425</b> (0.384-0.466)	<b>0.496</b> (0.444-0.540)	<b>0.567</b> (0.503-0.618)	<b>0.644</b> (0.565-0.702)	<b>0.753</b> (0.650-0.819)	<b>0.856</b> (0.728-0.933)
24-hr	<b>0.119</b> (0.111-0.129)	<b>0.144</b> (0.134-0.156)	<b>0.183</b> (0.170-0.198)	<b>0.214</b> (0.198-0.232)	<b>0.259</b> (0.238-0.280)	<b>0.295</b> (0.270-0.319)	<b>0.334</b> (0.304-0.361)	<b>0.375</b> (0.339-0.406)	<b>0.434</b> (0.389-0.471)	<b>0.482</b> (0.429-0.525)
2-day	<b>0.069</b> (0.064-0.074)	<b>0.083</b> (0.077-0.090)	<b>0.105</b> (0.097-0.113)	<b>0.122</b> (0.113-0.132)	<b>0.146</b> (0.135-0.158)	<b>0.166</b> (0.153-0.180)	<b>0.187</b> (0.171-0.203)	<b>0.210</b> (0.190-0.227)	<b>0.242</b> (0.217-0.263)	<b>0.268</b> (0.238-0.292)
3-day	<b>0.049</b> (0.045-0.052)	<b>0.059</b> (0.055-0.063)	<b>0.074</b> (0.068-0.079)	<b>0.085</b> (0.079-0.092)	<b>0.102</b> (0.094-0.110)	<b>0.116</b> (0.107-0.125)	<b>0.130</b> (0.119-0.140)	<b>0.145</b> (0.132-0.157)	<b>0.167</b> (0.150-0.181)	<b>0.184</b> (0.165-0.200)
4-day	<b>0.039</b> (0.036-0.042)	<b>0.047</b> (0.043-0.050)	<b>0.058</b> (0.054-0.062)	<b>0.067</b> (0.062-0.072)	<b>0.080</b> (0.074-0.086)	<b>0.090</b> (0.083-0.097)	<b>0.101</b> (0.093-0.109)	<b>0.113</b> (0.103-0.122)	<b>0.129</b> (0.117-0.139)	<b>0.142</b> (0.128-0.154)
7-day	<b>0.026</b> (0.024-0.028)	<b>0.031</b> (0.029-0.033)	<b>0.038</b> (0.035-0.041)	<b>0.044</b> (0.041-0.047)	<b>0.051</b> (0.048-0.055)	<b>0.058</b> (0.054-0.062)	<b>0.065</b> (0.059-0.069)	<b>0.071</b> (0.065-0.077)	<b>0.081</b> (0.074-0.088)	<b>0.089</b> (0.080-0.096)
10-day	<b>0.021</b> (0.019-0.022)	<b>0.024</b> (0.023-0.026)	<b>0.030</b> (0.028-0.032)	<b>0.034</b> (0.032-0.036)	<b>0.040</b> (0.037-0.042)	<b>0.044</b> (0.041-0.047)	<b>0.049</b> (0.045-0.052)	<b>0.054</b> (0.049-0.057)	<b>0.060</b> (0.055-0.065)	<b>0.065</b> (0.060-0.070)
20-day	<b>0.014</b> (0.013-0.015)	<b>0.016</b> (0.015-0.017)	<b>0.019</b> (0.018-0.021)	<b>0.022</b> (0.021-0.023)	<b>0.025</b> (0.024-0.027)	<b>0.028</b> (0.026-0.030)	<b>0.031</b> (0.029-0.033)	<b>0.034</b> (0.031-0.036)	<b>0.038</b> (0.035-0.040)	<b>0.041</b> (0.037-0.044)
30-day	<b>0.011</b> (0.011-0.012)	<b>0.013</b> (0.013-0.014)	<b>0.016</b> (0.015-0.017)	<b>0.018</b> (0.017-0.019)	<b>0.020</b> (0.019-0.021)	<b>0.022</b> (0.021-0.023)	<b>0.024</b> (0.022-0.025)	<b>0.026</b> (0.024-0.027)	<b>0.028</b> (0.026-0.030)	<b>0.030</b> (0.028-0.032)
45-day	<b>0.010</b> (0.009-0.010)	<b>0.011</b> (0.011-0.012)	<b>0.013</b> (0.012-0.014)	<b>0.014</b> (0.014-0.015)	<b>0.016</b> (0.015-0.017)	<b>0.018</b> (0.017-0.019)	<b>0.019</b> (0.018-0.020)	<b>0.020</b> (0.019-0.022)	<b>0.022</b> (0.021-0.024)	<b>0.024</b> (0.022-0.025)
60-day	<b>0.009</b> (0.008-0.009)	<b>0.010</b> (0.010-0.011)	<b>0.012</b> (0.011-0.012)	<b>0.013</b> (0.012-0.013)	<b>0.014</b> (0.013-0.015)	<b>0.015</b> (0.014-0.016)	<b>0.016</b> (0.015-0.017)	<b>0.017</b> (0.016-0.018)	<b>0.019</b> (0.018-0.020)	<b>0.020</b> (0.019-0.021)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

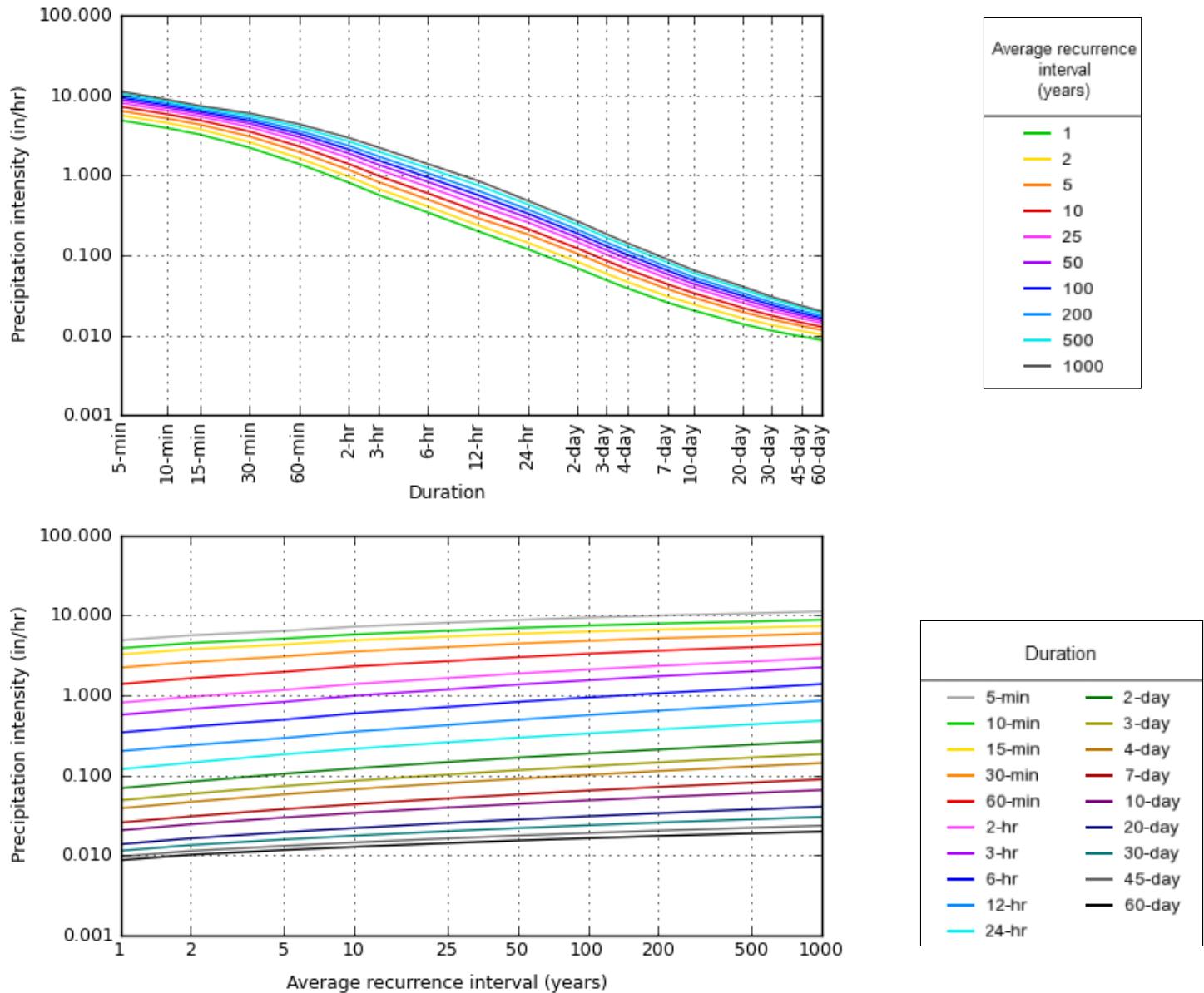
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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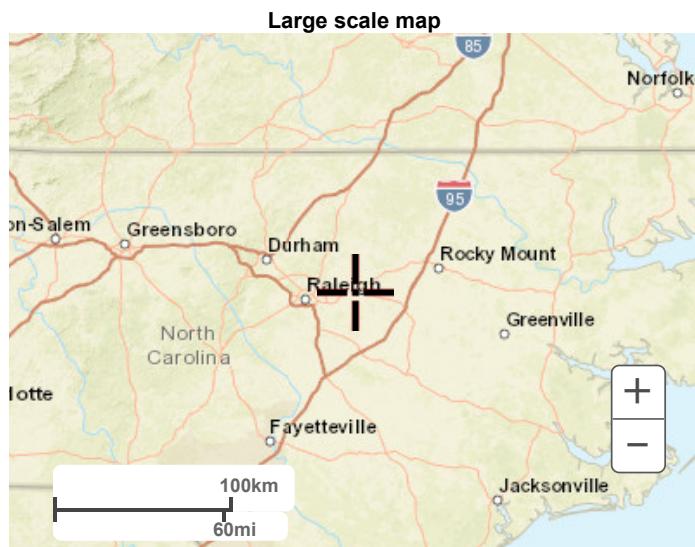
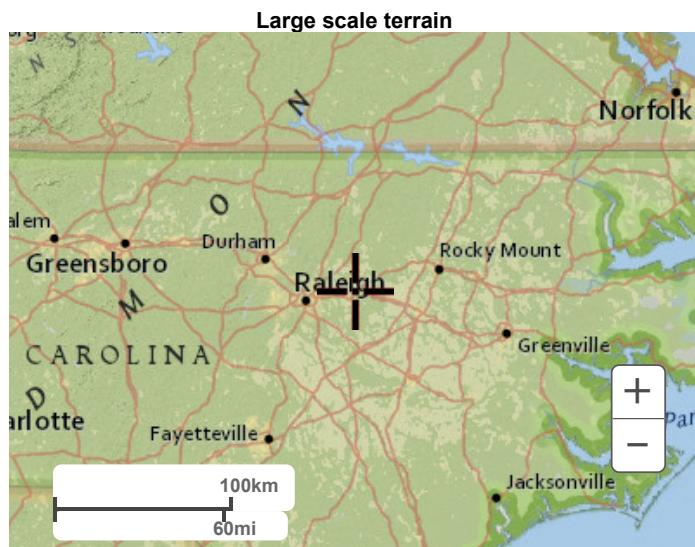
#### PF graphical

PDS-based intensity-duration-frequency (IDF) curves  
Latitude: 35.8183°, Longitude: -78.3283°

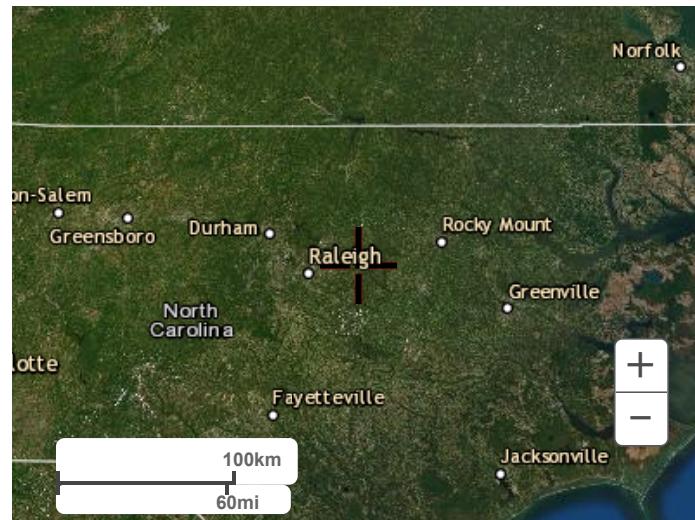


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WATER QUALITY/QUANTITY



## SITE DATA

Project Information		
Project Name:	Tractor Supply - Zebulon	
Applicant:		
Applicant Contact Name:	Sea Mountain Ventures II, LLC	
Applicant Contact Number:	Adam Sellner	
Contact Email:	704-954-7224	
Municipal Jurisdiction (Select from dropdown menu):	asellner@primaxproperties.com	
Last Updated:	Wednesday, February 15, 2023	
Site Data:		
Total Site Area (Ac):	8.15 ac	
Existing Lake/Pond Area (Ac):		
Proposed Disturbed Area (Ac):	5.69 ac	
Impervious Surface Area (acre):	4.62	
Type of Development (Select from Dropdown menu):	Non-Residential	
Percent Built Upon Area (BUA):		
Project Density:		
Is the proposed project a site expansion?	No	
Number of Drainage Areas on Site:	1	
NOAA	1-Year, 24-Hour Storm (inches) (See NOAA Website):	2.86
	2-Year, 24-Hour Storm (inches) (See NOAA Website):	3.46
	10-Year, 24-Hour Storm (inches) (See NOAA Website):	5.15
Lot Data (if applicable):		
Total Acreage in Lots:		
Number of Lots:		
Average Lot Size (SF):		
Total Impervious Surface Area on Lots (SF):		
Average Impervious Surface Area Per Lot (SF):		
Stormwater Narrative (limit to 1,200 characters - attach additional pages with submittal if necessary):		
<p>There are proposed storm water management facilities (wet pond and level spreader-filter strip) on site. The design includes the Tractor Supply site (164,059 sf-3.766 ac) and the 2.52 ac parcel to the west and assumes 80% impervious (90,769 sf-2.08 ac). The SCM outlined in this report has been designed for post-development peak attenuation and water quality. The SCM is designed to capture a drainage area of 5.57 ac with an impervious area of 4.62 ac. A level spreader-filter strip will be used as a secondary SCM receiving the 1.0" storm from the stormwater wetland pond, and it will be adjacent to a riparian buffer. The level spreader is designed to treat a 0.75" storm event. The outlet control structure has been designed so that only the 1" stormwater runoff is discharging to the level spreader-filter strip. The site grading and storm drainage systems are designed to convey stormwater runoff from the impervious areas of the site to the wet pond and level spreader-filter strip. The site is not located within a coastal county, therefore the design storm for water quality is a 1.0" storm event. The SCMs are designed per the Town of Zebulon stormwater UDO.</p>		



Project Name: Tractor Supply - Zebulon

**DRAINAGE AREA 1**  
**STORMWATER PRE-POST CALCULATIONS**

<b>LAND USE &amp; SITE DATA</b>		<b>PRE-DEVELOPMENT</b>				<b>POST-DEVELOPMENT</b>			
Drainage Area (Acres)=		3.71				5.57			
Site Acreage within Drainage=		3.71				5.57			
One-year, 24-hour rainfall (in)=						2.86			
Two-year, 24-hour rainfall (in)=						3.46			
Ten-year, 24-hour storm (in)=						5.15			
Total Lake/Pond Area (Acres)=		-				-			
Lake/Pond Area not in the Tc flow path (Acres)=									
Site Land Use (acres):		A	B	C	D	A	B	C	D
Pasture									
Woods, Poor Condition									
Woods, Fair Condition									
Woods, Good Condition					0.54				
Open Space, Poor Condition									
Open Space, Fair condition					3.17				
Open Space, Good Condition									0.95
Reforestation (in dedicated OS)									
Connected Impervious									4.62
Disconnected Impervious									
SITE FLOW		<b>PRE-DEVELOPMENT T<sub>c</sub></b>				<b>POST-DEVELOPMENT T<sub>c</sub></b>			
Sheet Flow									
Length (ft)=		100.00				100.00			
Slope (ft/ft)=		0.025				0.010			
Surface Cover:		Woods				Paved, Gravel, or Bare Soil			
n-value=		0.400				0.011			
T <sub>t</sub> (hrs)=		0.346				0.028			
Shallow Flow									
Length (ft)=		286.50				0.00			
Slope (ft/ft)=		0.041				0.000			
Surface Cover:		Unpaved				Paved			
Average Velocity (ft/sec)=		3.27							
T <sub>t</sub> (hrs)=		0.02							
Channel Flow 1									
Length (ft)=		0.00				0.00			
Slope (ft/ft)=		0.000				0.000			
Cross Sectional Flow Area (ft <sup>2</sup> )=		0.00				0.00			
Wetted Perimeter (ft)=		0.00				0.00			
Channel Lining:									
n-value=									
Hydraulic Radius (ft)=									
Average Velocity (ft/sec)=									
T <sub>t</sub> (hrs)=									



Project Name:

**DRAINAGE AREA 1**  
**STORMWATER PRE-POST CALCULATIONS**

Channel Flow 2		
Length (ft)=	0.00	0.00
Slope (ft/ft)=	0.000	0.000
Cross Sectional Flow Area ( $\text{ft}^2$ )=	0.00	0.00
Wetted Perimeter (ft)=	0.00	0.00
Channel Lining:		
n-value=		
Hydraulic Radius (ft)=		
Average Velocity (ft/sec)=		
$T_t$ (hrs)=		
Channel Flow 3		
Length (ft)=	0.00	0.00
Slope (ft/ft)=	0.000	0.000
Cross Sectional Flow Area ( $\text{ft}^2$ )=	0.00	0.00
Wetted Perimeter (ft)=	0.00	0.00
Channel Lining:		
n-value=		
Hydraulic Radius (ft)=		
Average Velocity (ft/sec)=		
$T_t$ (hrs)=		
$T_c$ (hrs)=	0.37	0.03
RESULTS	PRE-DEVELOPMENT	POST-DEVELOPMENT
Composite Curve Number=	83	95
Disconnected Impervious Adjustment		
Disconnected impervious area (acre)=		
$CN_{adjusted \ (1-year)}$ =	95	
High Density Only		
Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = ( $\text{ft}^3$ ) =	16,104	
1-year, 24-hour storm (Peak Flow)		
Runoff (inches) = $Q^{*}_{1-year}$ =	1.33	2.31
Volume of runoff ( $\text{ft}^3$ ) =	17,957	46,623
Volume change ( $\text{ft}^3$ ) =	28,666	
Peak Discharge (cfs) = $Q_{1-year}$ =	4.744	26.007
2-year, 24-hour storm (LID)		
Runoff (inches) = $Q^{*}_{2-year}$ =	1.82	2.89
Volume of runoff ( $\text{ft}^3$ ) =	24,557	58,483
Peak Discharge (cfs) = $Q_{2-year}$ =	6.487	32.623
10-year, 24-hour storm (DIA)		
Runoff (inches) = $Q^{*}_{10-year}$ =	3.31	4.56
Volume of runoff ( $\text{ft}^3$ ) =	44,552	61,414
Peak Discharge (cfs) = $Q_{10-year}$ =	11.769	51.433



**DA SITE SUMMARY**  
**STORMWATER PRE-POST CALCULATIONS**

<b>SITE SUMMARY</b>										
<b>DRAINAGE AREA SUMMARIES</b>										
DRAINAGE AREA:	DA1	DA2	DA3	DA4	DA5	DA6	DA7	DA8	DA9	DA10
<b>Pre-Development (1-year, 24-hour storm)</b>										
Runoff (in) = $Q_{\text{pre,1-year}} =$	1.33									
Peak Flow (cfs)= $Q_{1,\text{year}} =$	4.744									
<b>Post-Development (1-year, 24-hour storm)</b>										
Proposed Impervious Surface (acre) =	4.62									
Runoff (in)= $Q_{1,\text{year}} =$	2.31									
Peak Flow (cfs)= $Q_{1,\text{year}} =$	26.007									
Increase in volume per DA ( $\text{ft}^3$ )_1-yr storm=	28,666									
Minimum Volume to be Managed for DA HIGH DENSITY REQUIREMENT = ( $\text{ft}^3$ ) =	16,104									
<b>TARGET CURVE NUMBER (TCN)</b>										
<b>Site Data</b>										
<b>SITE \SOIL COMPOSITION</b>										
HYDROLOGIC SOIL GROUP					Site Area	%	Target CN			
A					0.00	0%	N/A			
B					0.00	0%	N/A			
C					0.00	0%	N/A			
D					5.57	100%	N/A			
Total Site Area (acres) =					5.57					
Percent BUA (Includes Existing Lakes/Pond Areas) =					83%					
Project Density =					High					
Target Curve Number (TCN) =					N/A					
$CN_{\text{adjusted (1-year)}} =$										
Minimum Volume to be Managed (Total Site) Per TCN Requirement= $\text{ft}^3$ =										
<b>Site Nitrogen Loading Data</b>										
HSG			TN export coefficient (lbs/ac/yr)		Site Acreage		N Export			
Pasture			1.2		0.00		0.00			
Woods, Poor Condition			1.6		0.00		0.00			
Woods, Fair Condition			1.2		0.00		0.00			
Woods, Good Condition			0.8		0.00		0.00			
Open Space, Poor Condition			1.0		0.00		0.00			
Open Space, Fair Condition			0.8		0.00		0.00			
Open Space, Good Condition			0.6		0.95		0.57			
Reforestation (in dedicated OS)			0.6		0.00		0.00			
Impervious			21.2		4.62		97.94			
SITE NITROGEN LOADING RATE (lbs/ac/yr)=					17.69					
Nitrogen Load (lbs/yr)=					98.51					
TOTAL SITE NITROGEN TO MITIGATE (lbs/yr)_Wendell Only=					78.46					
<b>Site Nitrogen Loading Data For Expansions Only</b>										
Existing					New					
Impervious(acres)=					NA		NA			
"Expansion Area" (acres=)										
Nitrogen Load (lbs/yr)=					NA		NA			
SITE NITROGEN LOADING RATE (lbs/ac/yr)=					NA		NA			
Total Site loading rate (lbs/ac/yr)										
TOTAL SITE NITROGEN TO MITIGATE (lbs/yr)=					NA					



Project Name: Tractor Supply - Zebulon

**DRAINAGE AREA 1  
BMP CALCULATIONS**

**DRAINAGE AREA 1 - BMP DEVICES AND ADJUSTMENTS**

DA1 Site Acreage=	5.57							
DA1 Off-Site Acreage=								
Total Required Storage Volume for Site TCN Requirement (ft <sup>3</sup> )=								
Total Required Storage Volume for DA1 1" Rainfall for High Density (ft <sup>3</sup> )=	16,104							
Will site use underground detention/cistern?	No	Enter % of the year water will be reused=	0%	Note: Supporting information/details should be submitted to demonstrate water usage.				

**ENTER ACREAGE FOR ALL SUB-DRAINAGE AREAS IN DA**

HSG	Sub-DA1(a) (Ac)		Sub-DA1(b) (Ac)		Sub-DA1(c) (Ac)		Sub-DA1(d) (Ac)		Sub-DA1(e) (Ac)	
	Site	Off-site								
Pasture										
Woods, Poor Condition										
Woods, Fair Condition										
Woods, Good Condition										
Open Space, Poor Condition										
Open Space, Fair Condition										
Open Space, Good Condition	0.95									
Reforestation (in dedicated OS)										
Impervious	4.62									

**Sub-DA1(a) BMP(s)**

Device Name (As Shown on Plan)	Device Type	Water Quality Volume for Sub-DA (ft <sup>3</sup> )	Provided Volume that will drawdown 2-5 days (ft <sup>3</sup> )	Nitrogen Removal Efficiency	Sub-DA Nitrogen (lbs)	Nitrogen Removed (lbs)	Drawdown Time (hours)
Wet Pond	Wet Detention Basin	16,104	17,189	25%	98.51	24.63	48.33
Level Spreader-Filter Strip	Level Spreader, Filter Strip			0%	73.89	0.00	
				0%	73.89	0.00	
				0%	73.89	0.00	
				0%	73.89	0.00	
<b>Total Nitrogen remaining leaving the subbasin (lbs):</b>		<b>73.89</b>					

**Sub-DA1(b) BMP(s)**

If Sub-DA1(b) is connected to upstream subbasin(s), enter the nitrogen leaving the most upstream subbasin(lbs):							
Device Name (As Shown on Plan)	Device Type	Water Quality Volume for Sub-DA (ft <sup>3</sup> )	Provided Volume that will drawdown 2-5 days (ft <sup>3</sup> )	Nitrogen Removal Efficiency	Sub-DA Nitrogen (lbs)	Nitrogen Removed (lbs)	Drawdown Time (hours)
		0	0	0%	0.00	0.00	
				0%	0.00	0.00	
				0%	0.00	0.00	
				0%	0.00	0.00	
				0%	0.00	0.00	
<b>Total Nitrogen remaining leaving the subbasin (lbs):</b>							

**Sub-DA1 (c) BMP(s)**

If Sub-DA1(c) is connected to upstream subbasin(s), enter the nitrogen leaving the most upstream subbasin(lbs):							
Device Name (As Shown on Plan)	Device Type	Water Quality Volume for Sub-DA (ft <sup>3</sup> )	Provided Volume that will drawdown 2-5 days (ft <sup>3</sup> )	Nitrogen Removal Efficiency	Sub-DA Nitrogen (lbs)	Nitrogen Removed (lbs)	Drawdown Time (hours)
		0	0	0%	0.00	0.00	
				0%	0.00	0.00	
				0%	0.00	0.00	
				0%	0.00	0.00	
				0%	0.00	0.00	
<b>Total Nitrogen remaining leaving the subbasin (lbs):</b>							



Project Name: Tractor Supply - Zebulon

**DRAINAGE AREA 1**  
**BMP CALCULATIONS**

**Sub-DA1(d) BMP(s)**

If Sub-DA1(d) is connected to upstream subbasin(s), enter the nitrogen leaving the most upstream subbasin(lbs):							
Device Name (As Shown on Plan)	Device Type	Water Quality Volume for Sub-DA (ft <sup>3</sup> )	Provided Volume that will drawdown 2-5 days (ft <sup>3</sup> )	Nitrogen Removal Efficiency	Sub-DA Nitrogen (lbs)	Nitrogen Removed (lbs)	Drawdown Time (hours)
		0	0	0%	0.00	0.00	
				0%	0.00	0.00	
				0%	0.00	0.00	
				0%	0.00	0.00	
				0%	0.00	0.00	
<b>Total Nitrogen remaining leaving the subbasin (lbs):</b>							

**Sub-DA1(e) BMP(s)**

If Sub-DA1(e) is connected to upstream subbasin(s), enter the nitrogen leaving the most upstream subbasin(lbs):							
Device Name (As Shown on Plan)	Device Type	Water Quality Volume for Sub-DA (ft <sup>3</sup> )	Provided Volume that will drawdown 2-5 days (ft <sup>3</sup> )	Nitrogen Removal Efficiency	Sub-DA Nitrogen (lbs)	Nitrogen Removed (lbs)	Drawdown Time (hours)
		0	0	0%	0.00	0.00	
				0%	0.00	0.00	
				0%	0.00	0.00	
				0%	0.00	0.00	
				0%	0.00	0.00	
<b>Total Nitrogen remaining leaving the subbasin (lbs):</b>							

**DA1 BMP SUMMARY**

Total Volume Treated (ft <sup>3</sup> )=	17,189
Nitrogen Mitigated(lbs)=	24.63

**1-year, 24-hour storm**

Post BMP Volume of Runoff (ft <sup>3</sup> ) <sub>(1-year)</sub> =	29,434
Post BMP Runoff (inches) = Q* <sub>(1-year)</sub> =	1.46
Post BMP CN <sub>(1-year)</sub> =	84
Post BMP Peak Discharge (cfs)= Q <sub>(1-year)</sub> =	2.294

**2-year, 24-hour storm (LID)**

Post BMP Volume of Runoff (ft <sup>3</sup> ) <sub>(2-year)</sub> =	41,294
Post BMP Runoff (inches) = Q* <sub>(2-year)</sub> =	2.04
Post BMP CN <sub>(2-year)</sub> =	85
Post BMP Peak Discharge (cfs)= Q <sub>(2-year)</sub> =	14.130

**10-year, 24-hour storm (DIA)**

Post BMP Volume of Runoff (ft <sup>3</sup> ) <sub>(10-year)</sub> =	44,225
Post BMP Runoff (inches) = Q* <sub>(10-year)</sub> =	2.19
Post BMP CN <sub>(10-year)</sub> =	87
Post BMP Peak Discharge (cfs)= Q <sub>(10-year)</sub> =	32.630



Project Name: **Tractor Supply - Zebulon**

**DA SITE SUMMARY**  
**BMP CALCULATIONS**

BMP SUMMARY										
DRAINAGE AREA SUMMARIES										
DRAINAGE AREA:	DA1	DA2	DA3	DA4	DA5	DA6	DA7	DA8	DA9	DA10
Pre-Development (1-year, 24-hour storm)										
Runoff (in)=Q* <sub>1-year</sub> =	1.33									
Peak Flow (cfs)=Q <sub>1-year</sub> =	4.744									
Post-Development (1-year, 24-hour storm)										
Target Curve Number (TCN) =	NA									
Post BMP Runoff (inches) = Q* <sub>(1-year)</sub> =	1.46									
Post BMP Peak Discharge (cfs)= Q <sub>(1-year)</sub> =	2.294									
Post BMP CN <sub>(1-year)</sub> =										
Post-BMP Nitrogen Loading										
TOTAL SITE NITROGEN MITIGATED (lbs)=	24.63									
SITE NITROGEN LOADING RATE (lbs/ac/yr)=	13.26									
TOTAL SITE NITROGEN LEFT TO MITIGATE_Wendell Only (lbs)=	53.83									



Project Name: Tractor Supply - Zebulon

## DOWNSTREAM IMPACT ANALYSIS SITE SUMMARY

### DRAINAGE AREA SUMMARIES

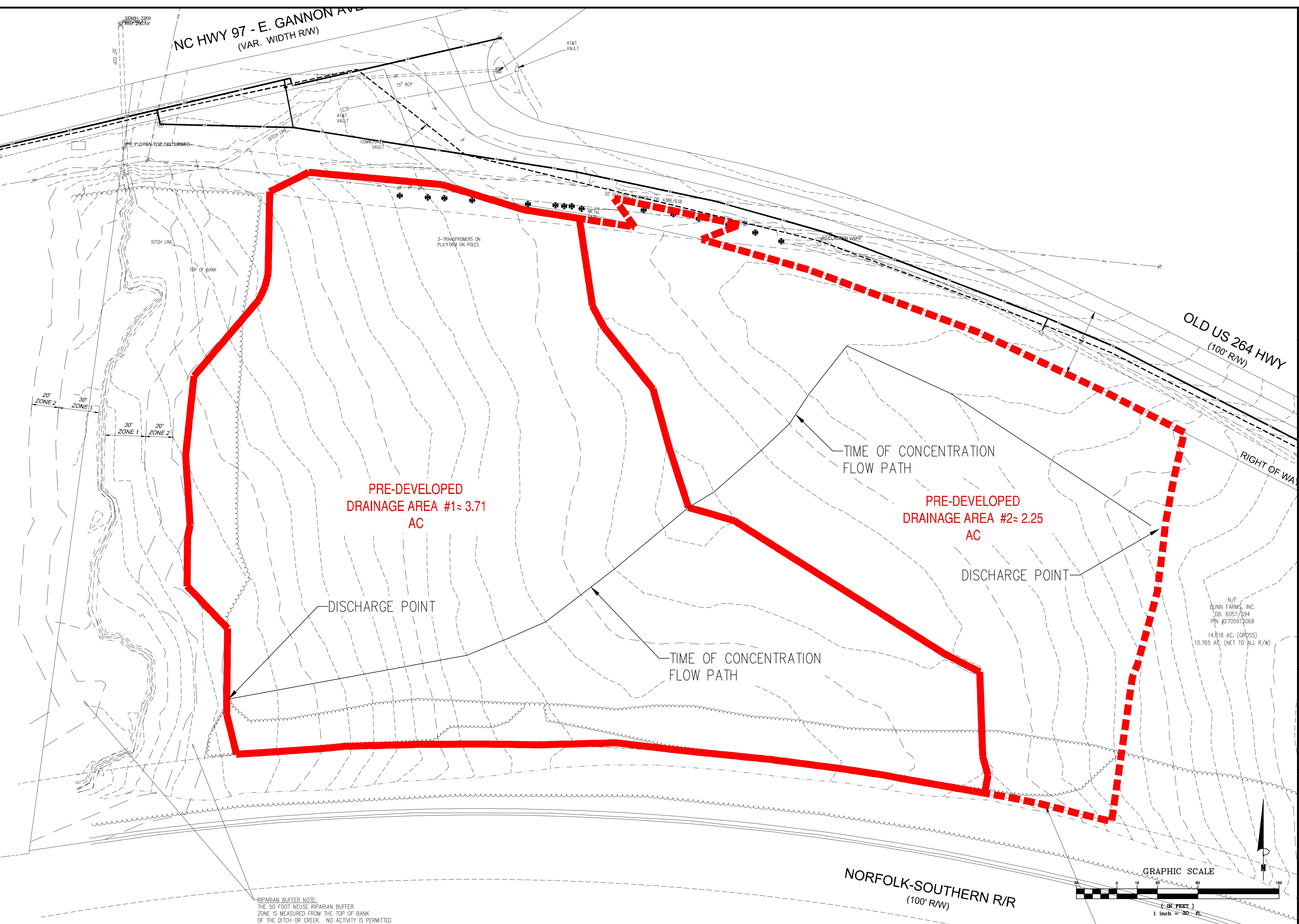
DRAINAGE AREA:	DA1	DA2	DA3	DA4	DA5	DA6	DA7	DA8	DA9	DA10
<b>Pre-Development</b>										
Peak Discharge (cfs)=Q <sub>10-year</sub> =	11.77									
Volume of Runoff (ft <sup>3</sup> ) <sub>(10-year)</sub> =	44,552									
<b>Post-Development</b>										
<b>10-year, 24-hour storm (DIA)</b>										
Post BMP Peak Discharge (cfs)= Q <sub>(10-year)</sub> =	32.63									
Post BMP Volume of Runoff (ft <sup>3</sup> ) <sub>(10-year)</sub> =	44,225									



TSC  
TRACTOR SUPPLY COMPANY

PRE-DEVELOPED DRAINAGE AREA

Tractor Supply  
Old US Highway 264  
Zebulon, NC Wake County



PLAN STATUS	DESCRIPTION
1/10/23	1ST CD SUBMISSION
2/10/23	2ND CD SUBMISSION

DATE	DESCRIPTION
MEL DESIGN	MEL XXX DRAWN XXX CHKD XXX
SCALE	H: 1" = XXX V: 1" = XXX

JOB No. 220127-01-001

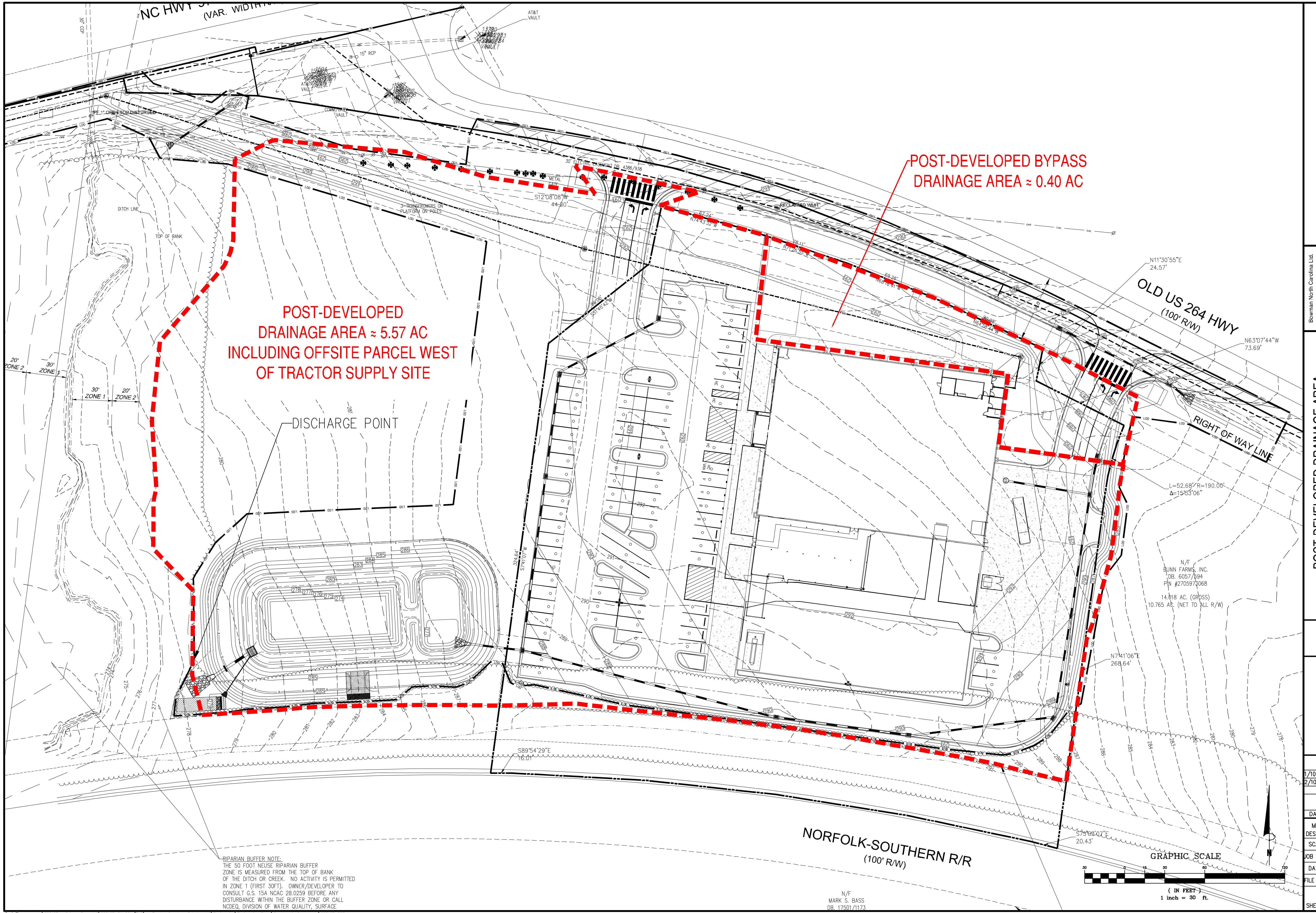
DATE January 10, 2023

FILE No. 220127-D-CP-001

SHEET #####



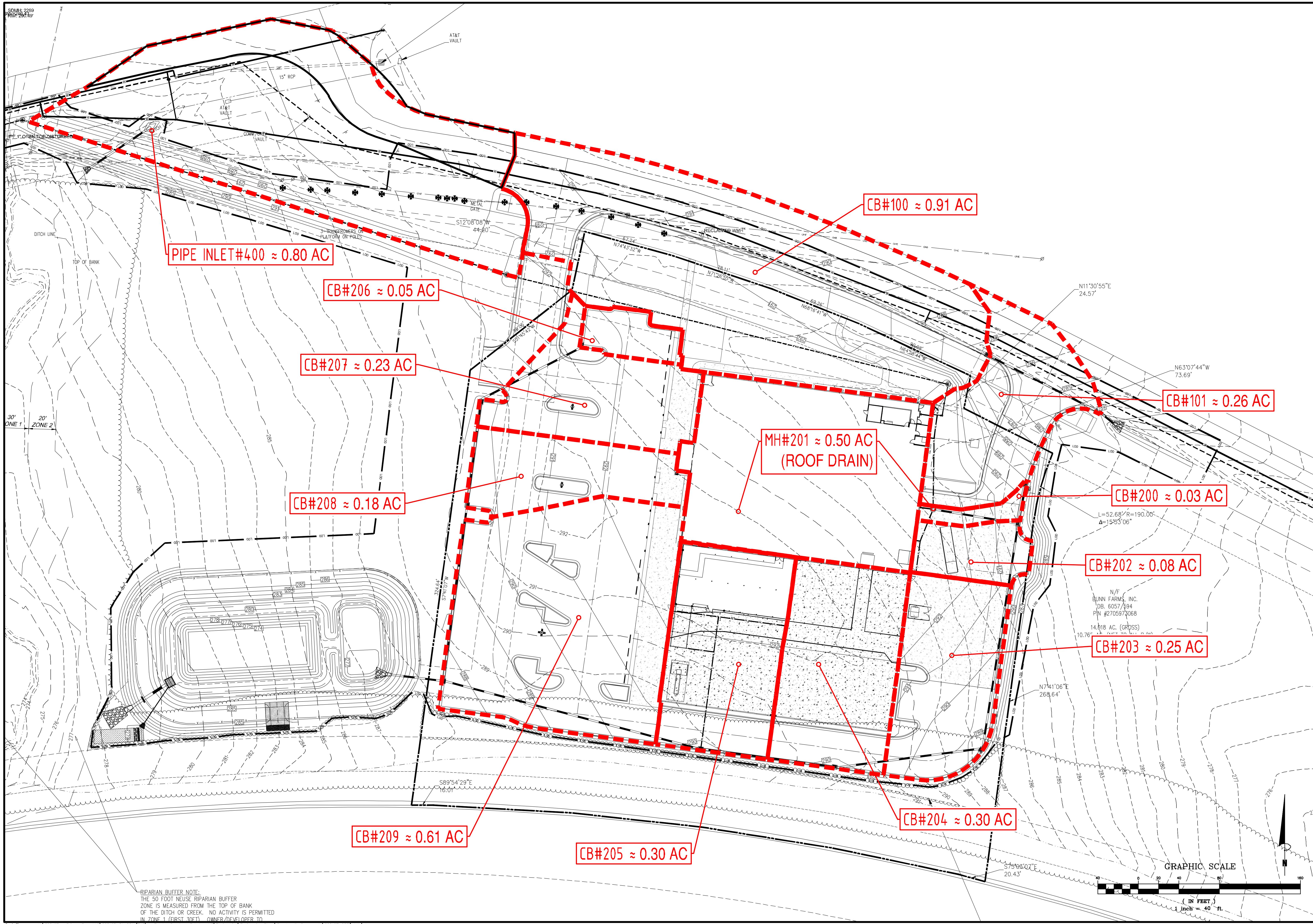
Tractor Supply  
Old US Highway 264  
Zebulon, NC Wake County





Tractor Supply  
Old US Highway 264  
Zebulon, NC Wake County

POST-DEVELOPED DRAINAGE AREA TO INLETS



RIPARIAN BUFFER NOTE:  
THE 50 FOOT NEUSE RIPARIAN BUFFER  
ZONE IS MEASURED FROM THE TOP OF BANK  
OF THE DITCH OR CREEK. NO ACTIVITY IS PERMITTED  
IN ZONE 1 (FIRST 30FT). OWNER/DEVELOPER TO

Bowman North Carolina, Ltd.  
Tractor Supply, Zebulon, NC

## Curve Number Calculation (CN)

### Pre-Developed Conditions #1

Drainage Area (acres): 3.71

Existing Soil Groups:

<u>Soil Group</u>	<u>Map Symbol</u>	<u>Soil Description</u>	<u>Acres</u>	<u>Percent of DA</u>
D	VaB, VaC, & HeB	Vance and Helena Sandy Loam	3.71	100%

Existing Land Uses:

<u>Land Use Description</u>	<u>Existing Soil Group</u>	<u>Acres</u>	<u>Curve #</u>	<u>Weighted CN</u>
Wooded - Good Stand	D	0.54	77	11.2
Open Space - Fair	D	3.17	84	71.8

Cumulative Curve # = 83.0

Bowman North Carolina, Ltd.  
Tractor Supply, Zebulon, NC

## Curve Number Calculation (CN)

**Pre-Developed Conditions #2**

Drainage Area (acres): 2.25

Existing Soil Groups:

<u>Soil Group</u>	<u>Map Symbol</u>	<u>Soil Description</u>	<u>Acres</u>	<u>Percent of DA</u>
D	VaB, VaC, & HeB	Vance and Helena Sandy Loam	2.25	100%

Existing Land Uses:

<u>Land Use Description</u>	<u>Existing Soil Group</u>	<u>Acres</u>	<u>Curve #</u>	<u>Weighted CN</u>
Wooded - Good Stand	D	0.11	77	3.8
Open Space - Fair	D	2.14	84	79.9

Cumulative Curve # = 83.7

Bowman North Carolina, Ltd.  
Tractor Supply, Zebulon, NC

## Curve Number Calculation (CN)

**Post-Developed Conditions**

Drainage Area (acres): 5.57

Existing Soil Groups:

<u>Soil Group</u>	<u>Map Symbol</u>	<u>Soil Description</u>	<u>Acres</u>	<u>Percent of DA</u>
D	VaB, VaC, & HeB	Vance and Helena Sandy Loam	5.57	100%

Proposed Land Uses:

<u>Land Use Description</u>	<u>Existing Soil Group</u>	<u>Acres</u>	<u>Curve #</u>	<u>Weighted CN</u>
Impervious	D	4.62	98	81.3
Open Space - Good Condition	D	0.95	80	13.6
Cumulative Curve # =				94.9

Bowman North Carolina, Ltd.  
Tractor Supply, Zebulon, NC

## Curve Number Calculation (CN)

**Post-Developed Conditions ByPass**

Drainage Area (acres): 0.40

Existing Soil Groups:

<u>Soil Group</u>	<u>Map Symbol</u>	<u>Soil Description</u>	<u>Acres</u>	<u>Percent of DA</u>
D	VaB, VaC, & HeB	Vance and Helena Sandy Loam	0.40	100%

Proposed Land Uses:

<u>Land Use Description</u>	<u>Existing Soil Group</u>	<u>Acres</u>	<u>Curve #</u>	<u>Weighted CN</u>
Open Space - Good Condition	D	0.31	80	63.2
Impervious	D	0.08	98	20.5
Cumulative Curve # =				83.8

## Proposed Wet Pond

### Project Information

Project Name: Tractor Supply (Zebulon)  
Project #: 220127-01-001  
Designed by: CEP Date: 2/8/2023  
Revised by: \_\_\_\_\_ Date: \_\_\_\_\_  
Checked by: \_\_\_\_\_ Date: \_\_\_\_\_

### Site Information

Sub Area Location: Drainage To Proposed Wet Pond  
Drainage Area (DA) = 5.57 Acres 242,500 sf  
Impervious Area (IA) = 4.62 Acres 201,297 sf  
Percent Impervious (I) = % 83.01 %

### Required Surface Area

Permanent Pool Depth: 4.43 ft Non-Coastal County  
SA/DA = 2.33  
Min Req'd Surface Area = 5,661 sf (at Permanent Pool) (Main Pond)

### Required WQv Storage Volume

Design Storm = 1 inch Non-Coastal County  
Determine Rv Value = 0.05 + .009 (I) = 0.797 in/in  
Storage Volume Required = 16,108 cf (above Permanent Pool)

### Elevations

Top of Pond Elevation = 285.00 ft  
Temporary Pool Elevation = 281.70 ft  
Permanent Pool Elevation = 280.00 ft  
  
Shelf Beginning Elevation = 280.50 ft  
Forebay Weir = 279.00 ft  
Shelf Ending Elevation = 279.50 ft  
Bottom Elevation = 274.00 ft

### Permanent Pool Area

Area @ Top of Permanent Pool = 6,335 sf

Volume of Temporary Storage = 17,189 cf

Is Permanent Pool Surface Area Sufficient (yes/no)? Yes ( 6335 > 5661 ) sf

Volume of Storage for Design Storm = 17,189 Yes ( 17189 > 16108 ) cf

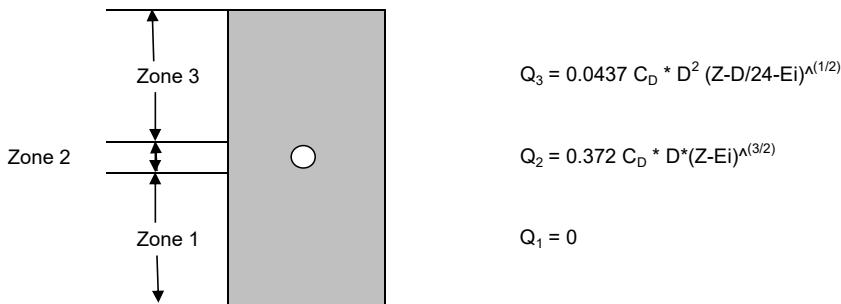
**STORMWATER POND**  
**INCREMENTAL DRAWDOWN METHOD-Water Quality Volume**

**Project Information**

Project Name: Tractor Supply (Zebulon)  
 Project #: 220127-01-001  
 Designed by: CEP Date: 1/10/2023  
 Checked by: \_\_\_\_\_ Date: \_\_\_\_\_

**Water Quality Orifice**

\* Incremental Determination of Water Quality Volume Drawdown Time



Orifice Diameter (D) = **2** in  
 Cd = 0.6  
 Ei = 280 Orifice Inv.  
 Zone 1 Range = 0.00 to 280  
 Zone 2 Range = 280 to 280.1  
 Zone 3 Range = 280.1 to 281

Incremental Drawdown Method						
Contour	Contour Area	Incremental Volume	Stage, Z	Zone	Q	Drawdown Time
	sq ft	cu ft	ft		cfs	min
280.00	<b>8,385</b>	0	0.00	2.00	0.000	--
280.50	9635	4,505	0.50	3.00	0.068	1,109
281.00	10395	5,008	0.50	3.00	0.100	831
281.70	11535	7,676	0.70	3.00	0.133	959
<b>Total</b>	--	<b>17,189</b>	--	--	--	<b>2,900</b>

Drawdown Time = Incremental Volume / Q / 60sec/min

**Summary**

Total Volume = **17,189** cf  
 Total Time = **2,900** min  
 Total Time = **2.01** days Between 2 & 5

Project:

Pond #1

Date: 1/10/2023

<b>Main-Pond Contours-Volumes</b>				
Elevation	Main-Pond	Incremental Vol.	Accumulated Vol.	Description
280	6,335	2,933	24,118	A2 (Perm_Pool)
279.5	5,395	2,623	21,185	A1 (Bottom_Shelf)
279	5,095	4,803	18,563	
278	4,510	4,230	13,760	
277	3,950	3,685	9,530	
276	3,420	3,168	5,845	
275	2,915	2,678	2,678	
274	2,440	0	0	A3 (Bottom_Pond)

<b>Forebay Contours-Volumes</b>						
Elevation	FB1	FB2	FB3	Total-Areas	Incremental Vol.	Accumulated Vol.
280	1,965			1,965	941	4,143
279.5	1,800			1,800	859	3,201
279	1,635			1,635	1,485	2,343
278	1,335			1,335	858	858
277	380			380	0	0

Forebay Volume 17.2% \*Between 15% &amp; 20%

Average Depth (Option 1) 3.93 \*At least 3' average depth

Average Depth Calculation (Option 2)

Vpp	24,118
perimeter of shelf	323
width of shelf	3
A1 (Bottom_Shelf):	5,395

Average Depth = 4.43

## Proposed Wet Pond #1

### Project Information

Project Name: Tractor Supply (Zebulon)  
Project #: 220127-01-001  
Designed by: CEP Date: 2/8/2023  
Revised by: \_\_\_\_\_ Date: \_\_\_\_\_  
Checked by: \_\_\_\_\_ Date: \_\_\_\_\_

### Site Information

Sub Area Location: Drainage to Proposed Pond  
Drainage Area (DA) = 5.57 Acres  
Impervious Area (IA) = 4.62 Acres  
Percent Impervious (I) = 83.01 % (Drainage Area)

### Orifice Sizing

Orifice Size = 2.00 in (Diameter)  
Drawdown Time = 2.01 days (Incremental Draw Down Method)

less than 5 days (yes/no) ? yes  
greater than 2 day (yes/no) ? yes

### Anti-Flotation Device

6' x 5' Outlet Structure

Area: 30.0 sf  
Volume: 330.0 cf  
Weight: 20592 lbs  
(Water Displaced - Top of Pond to Bottom of Pond)

Factor of Safety 1.20  
WT Req'd of Anti-Flotation Device: 24,710 lbs  
Volume of Concrete Req'd: 164.7 cf  
(Unit WT of Concrete = 150pcf)

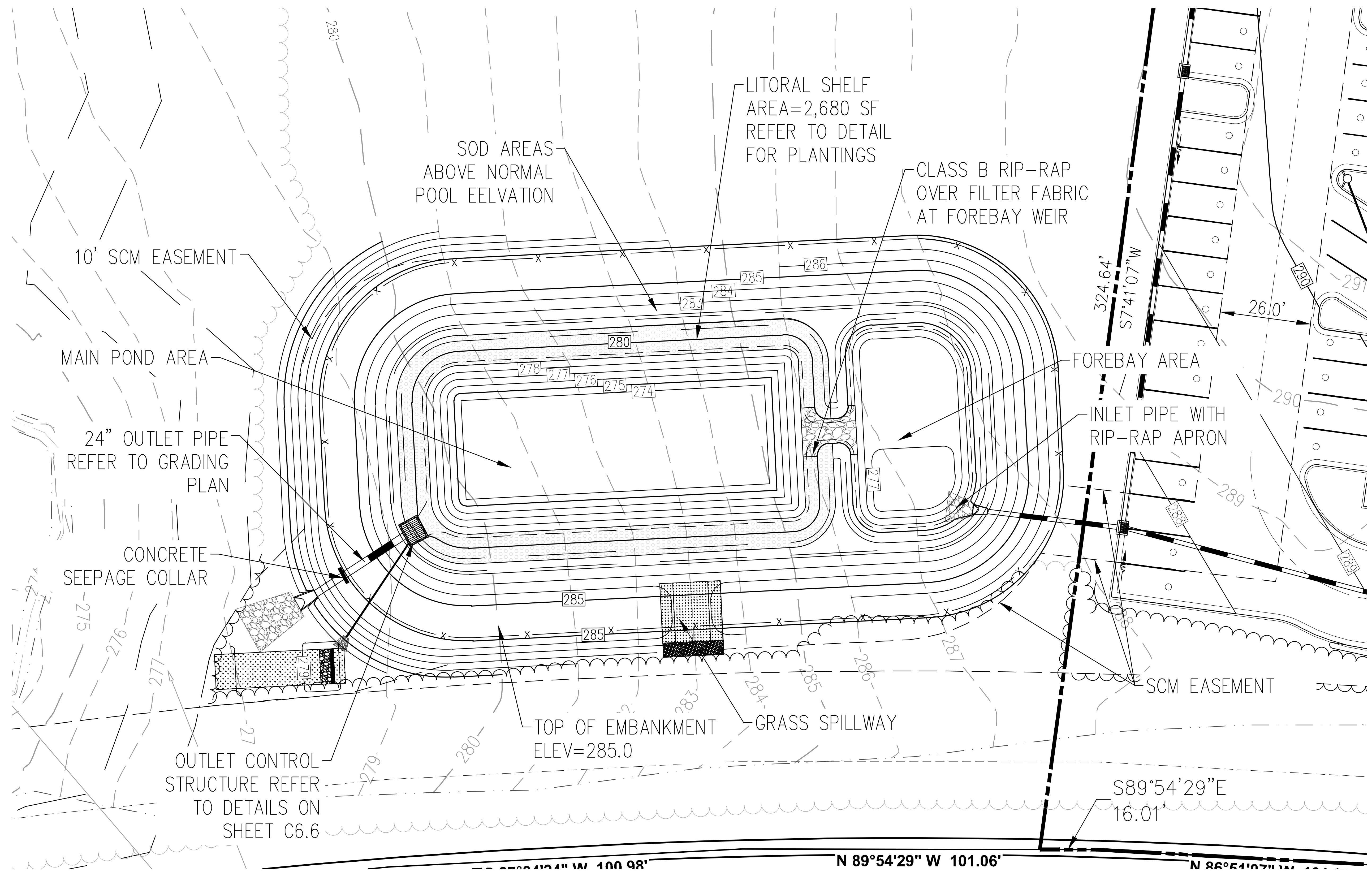
Volume Provided: 213.0 cf  
(6'x5' riser x 5.0' =150.0cf, 7'x6' footing x 1.5' =63.0cf)

## IMPERVIOUS SUMMARY TABLE

ON-SITE AREA = 164,059 SF (3.766 AC)

TOTAL DRAINAGE AREA = 242,500 SF (5.567 AC)

BUILDINGS	21,147 SF	0.49 ACRE(S)	12.91 % OF AREA
PAVEMENT	81,500 SF	1.87 ACRE(S)	49.68 % OF AREA
SIDEWALK	7,100 SF	0.16 ACRE(S)	4.33 % OF AREA
ON-SITE IMPERVIOUS AREA	109,774 SF	2.52 ACRE(S)	66.91 % OF AREA
OFF-SITE IMPERVIOUS AREA	10,051 SF	0.23 ACRE(S)	6.13 % OF AREA
GREEN/OPEN SPACE	54,285 SF	1.25 ACRE(S)	33.09 % OF AREA
EXISTING IMPERVIOUS AREA	0 SF	0 ACRE(S)	0.0 % OF AREA
INCREASE IN IMPERVIOUS AREA	119,825 SF	2.75 ACRE(S)	73.04 % OF AREA



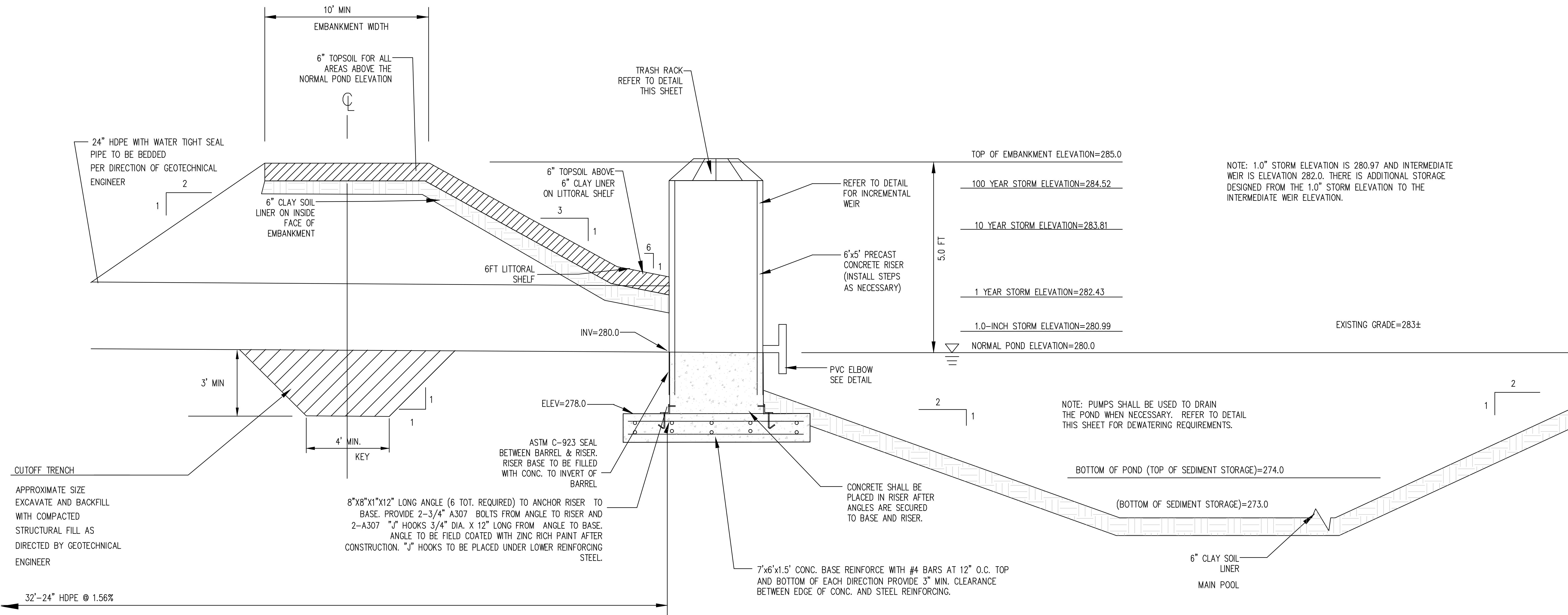
### GRAPHIC SCALE



( IN FEET )

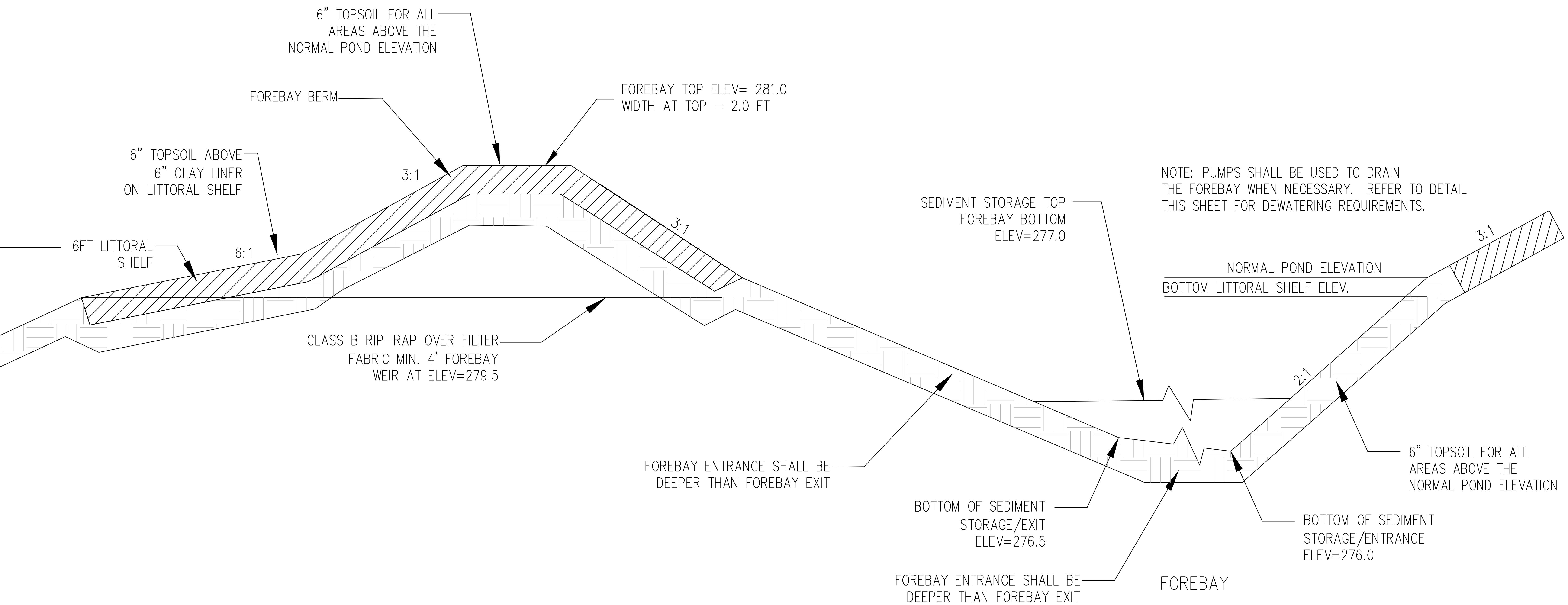
1 inch = 40 ft.

### PLAN VIEW



**PROFILE OF WET POND DETENTION SYSTEM**

SCALE: N.T.S.



STAGE/STORAGE TABLE				
STAGE (FT)	ELEVATION (FT)	CONTOUR AREA (SF)	INCREMENTAL STORAGE (CF)	TOTAL STORAGE (CF)
0.0	280.0	8385	0	0
0.5	280.5	9635	4505	4505
1.0	281.0	10395	5008	9513
1.7	281.7	11535	7676	17188 (WQV)
2.0	282.0	11940	3521	20709
3.0	283.0	13325	12633	33342
4.0	284.0	14765	14045	47387
5.0	285.0	16265	15515	62902

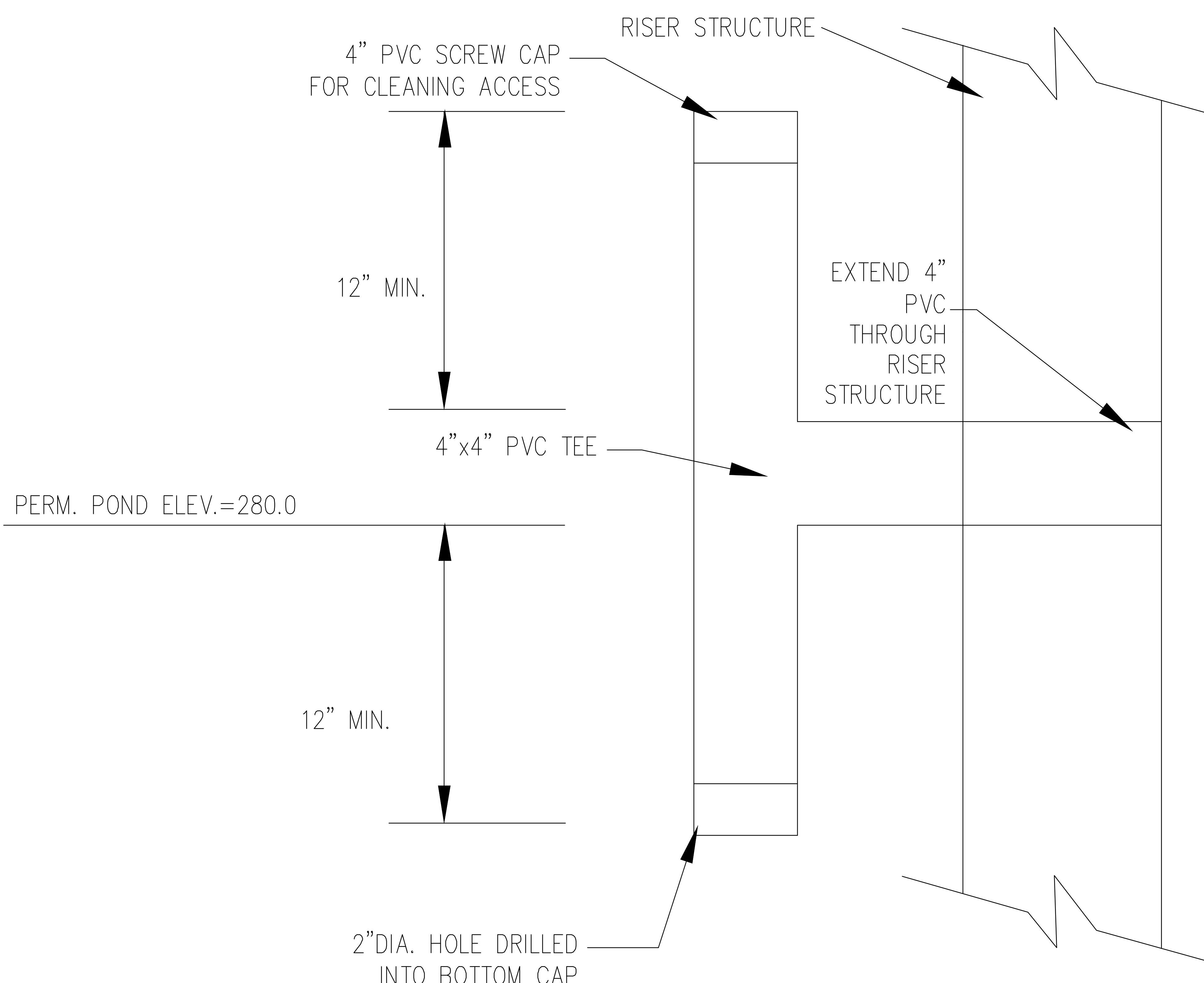
## STORMWATER MANAGEMENT DESIGN WET DETENTION POND:

RIVER BASIN: NEUSE  
RECEIVING STREAM: LITTLE CREEK (WEST SIDE)  
STREAM INDEX: 27-86-2-4  
STREAM CLASS: C; NSW  
HUC: 03020203  
PROJECT COORDINATES: 35.828782°N, -78.293752°W

### POND DESIGN SUMMARY

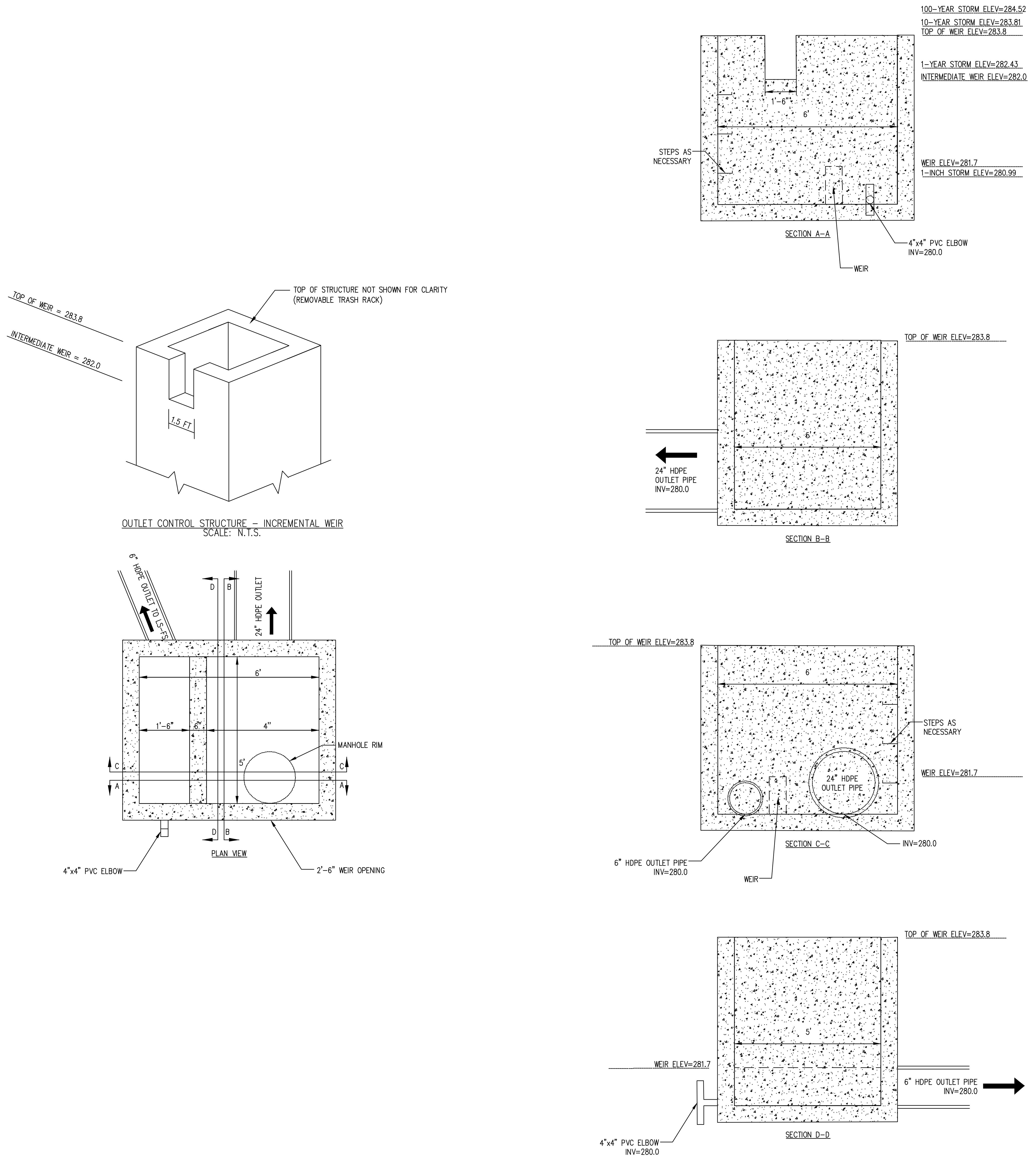
DRAINAGE AREA TO POND:	5.57 ACRES
SITE IMPERVIOUS AREA TO POND:	2.53 ACRES
OFF-SITE DESIGN IMPERVIOUS AREA TO POND:	2.08 ACRES
TOTAL DESIGN IMPERVIOUS AREA TO POND:	4.62 ACRES

	PRE-DEVELOPED TO POND	POST-DEVELOPED TO POND	POST-DEVELOPED THROUGH POND	POST-DEVELOPED BYPASS	POST-DEVELOPED TOTAL
DRAINAGE AREA:	3.71 AC	5.57 AC		0.40 AC	
CURVE NUMBER:	83.0	94.9		83.8	
TIME OF CONCENTRATION:	14.0 MIN	5 MIN		10 MIN	
1.0" STORM EVENT:		2.599 CFS	0.098 CFS		
1-YEAR STORM EVENT:	6.225 CFS	19.97 CFS	1.561 CFS	0.800 CFS	2.361 CFS
10-YEAR STORM EVENT:	15.39 CFS	37.96 CFS	12.59 CFS	1.936 CFS	14.53 CFS
100-YEAR STORM EVENT:	27.21 CFS	60.08 CFS	43.50 CFS	3.389 CFS	46.89 CFS



## PVC DRAIN OUTLET

SCALE: N.T.S.



## Level Spreader Design

### **Site Information**

Sub Area Location:	Drainage To Proposed LSFS		
Drainage Area (DA) =	5.57	Acres	242,500 sf
Impervious Area (IA) =	4.62	Acres	201,297 sf
Percent Impervious (I) =	%	83.01	%

### **Required Water Quality Volume**

Design Storm =	1	inch
Determine Rv Value =	0.05 + .009 (I) =	0.80 in/in
Water Quality Volume =	0.370 ac-ft	
Water Quality Volume =	16,108 cf	
Water Quality Volume =	0.797 inches of runoff	

### **Level Spreader Design Storm**

$$I = 0.75 \text{ in/hr}$$

$$\begin{aligned} Q_{1.0\text{" storm}} &= 0.098 \text{ cfs} && \text{through pond} \\ Q_{0.75\text{" storm}} &= 0.098 \text{ cfs} \end{aligned}$$

### **Level Spreader Length**

$$\text{Level Spreader Length} = 10 \text{ ft/cfs} \times Q_{1.0\text{in-storm}}$$

$$\begin{aligned} L_{\text{required}} &= 1.0 \text{ ft} \\ L_{\text{min}} &= 10.0 \text{ ft} \\ L_{\text{provided}} &= 10.0 \text{ ft} \end{aligned}$$

#### VEGETATIVE FILTER STRIP – SOIL MIXTURE

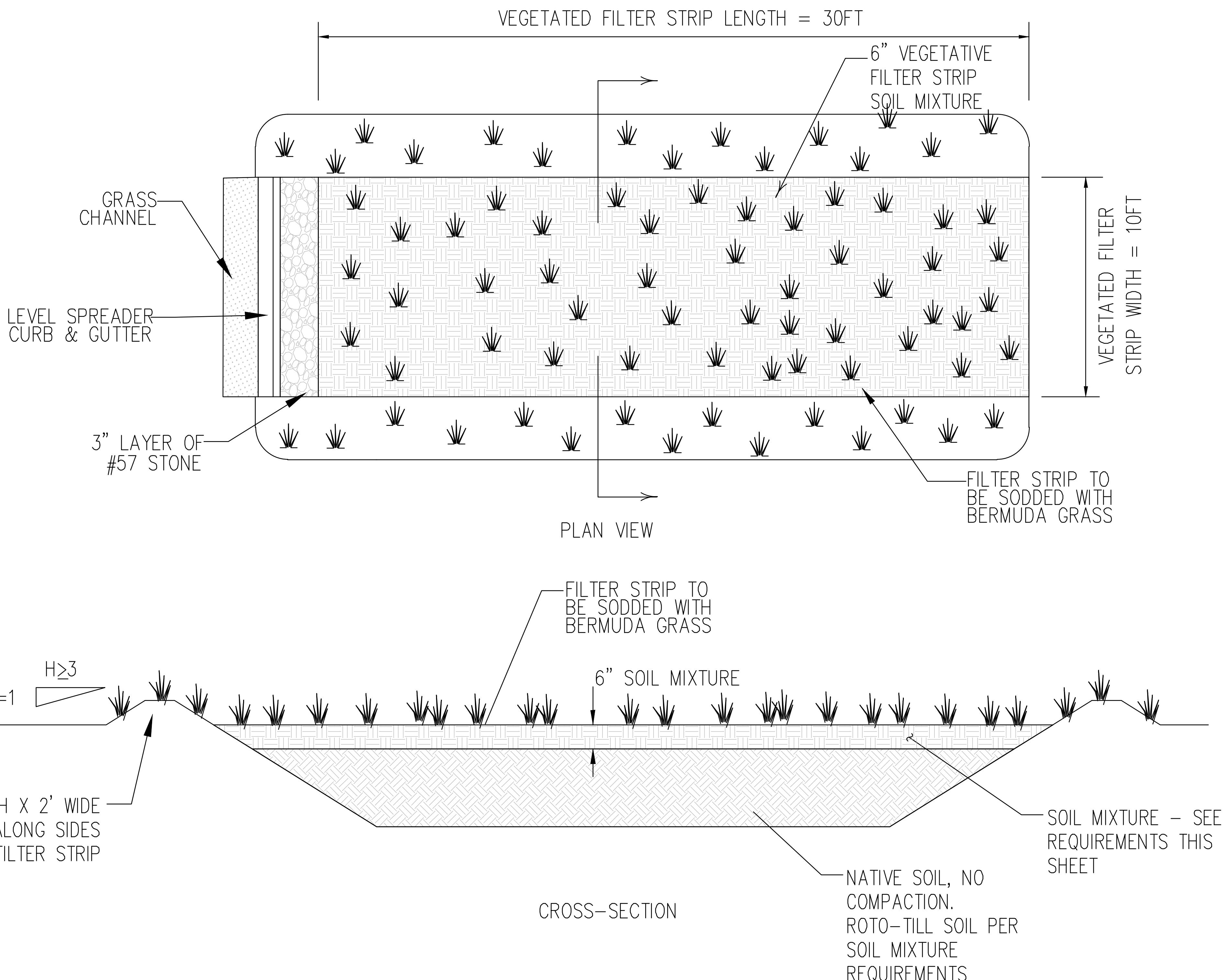
##### SOIL MIXTURE

ITEM	PERCENT BY WEIGHT	MATERIAL
SAND	85–88%	CONSTRUCTION SAND
FINES	8%–12%	SILT
ORGANIC MATTER	3%–5%	COMPOST/PEAT MOSS

**SOIL MIXTURE:** SHALL BE PLACED AND GRADED USING LOW GROUND-CONTACT PRESSURE EQUIPMENT OR BY EXCAVATORS AND/OR BACKHOES OPERATING ON THE GROUND ADJACENT TO THE VEGETATIVE FILTER STRIP FACILITY. NO HEAVY EQUIPMENT SHALL BE USED WITHIN THE PERIMETER OF THE VEGETATIVE FILTER STRIP FACILITY BEFORE, DURING, OR AFTER THE PLACEMENT OF THE SOIL MIXTURE. THE SOIL MIXTURE SHALL BE PLACED IN HORIZONTAL LAYERS NOT TO EXCEED 4 INCHES FOR THE ENTIRE AREA OF THE VEGETATIVE FILTER STRIP FACILITY. IF THE SOIL MIXTURE BECOMES CONTAMINATED DURING THE CONSTRUCTION OF THE VEGETATIVE FILTER STRIP FACILITY, THE CONTAMINATED MATERIAL SHALL BE REMOVED AND REPLACED WITH UNCONTAMINATED MATERIAL AT NO ADDITIONAL COST. FINAL GRADING OF THE VEGETATIVE FILTER STRIP SHALL BE PERFORMED AFTER A 24-HOUR SETTLING PERIOD. FINAL ELEVATIONS SHALL BE WITHIN 2 INCHES OF ELEVATIONS SHOWN ON THE CONTRACT PLANS.

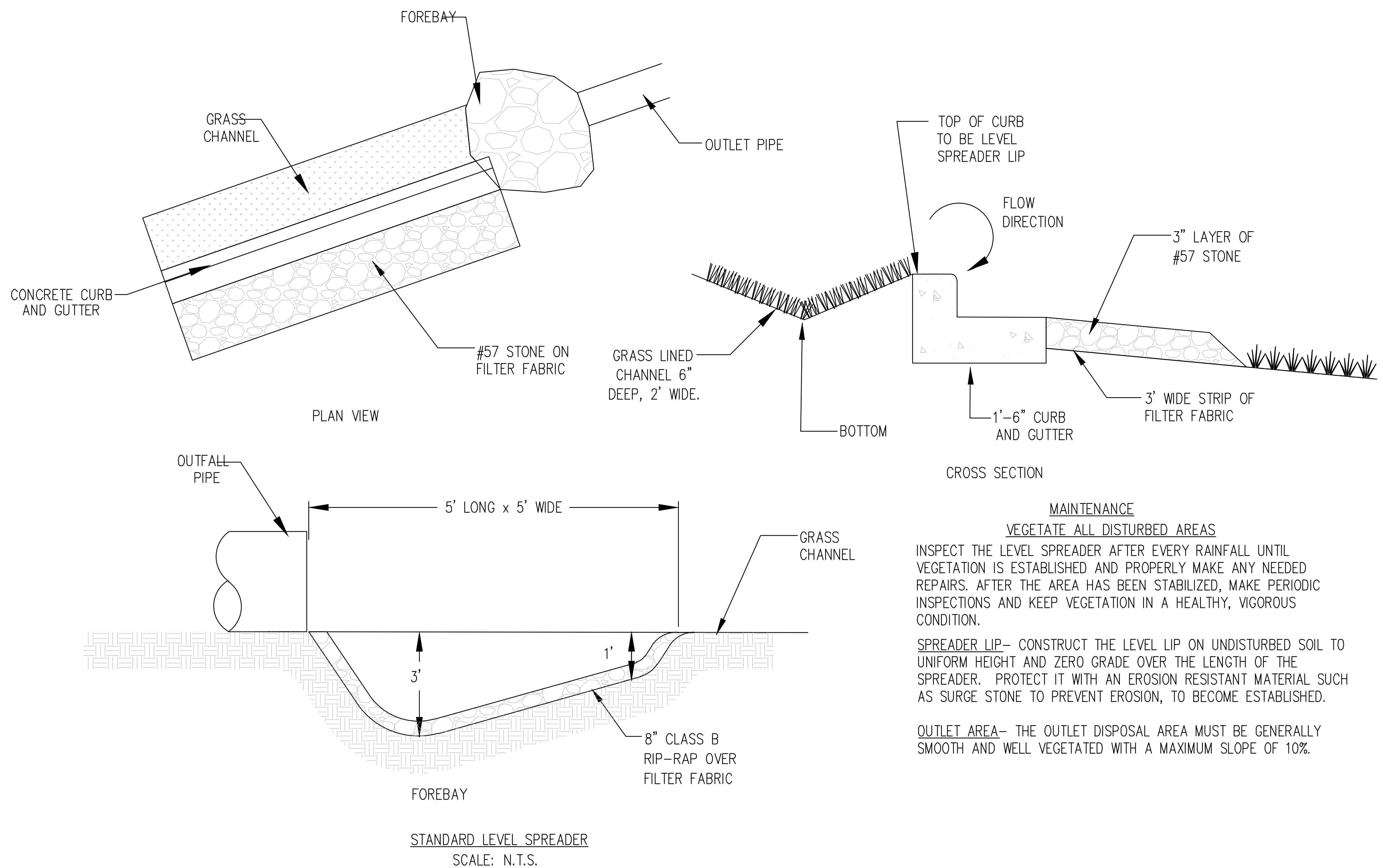
THE SOIL MIXTURE SHALL BE A UNIFORM MIX, FREE OF STONES, STUMPS, ROOTS OR OTHER SIMILAR OBJECTS LARGER THAN TWO INCHES EXCLUDING MULCH. NO OTHER MATERIALS OR SUBSTANCES SHALL BE MIXED OR DUMPED WITHIN THE VEGETATIVE FILTER STRIP AREA THAT MAY BE HARMFUL TO PLANT GROWTH, OR PROVE A HINDRANCE TO THE PLANTING OR MAINTENANCE OPERATIONS.

PRIOR TO PLACING THE SOIL MIXTURE, THE BOTTOM OF THE EXCAVATION SHALL BE ROTO-TILLED TO A MINIMUM DEPTH OF 6 INCHES TO ALLEVIATE ANY COMPACTION OF THE FACILITY BOTTOM. ANY SUBSTITUTE METHOD FOR ROTO-TILLING MUST BE APPROVED BY THE ENGINEER PRIOR TO USE. ANY PONDED WATER SHALL BE REMOVED FROM THE BOTTOM OF THE FACILITY AND THE SOIL SHALL BE FRIABLE BEFORE ROTO-TILLING.



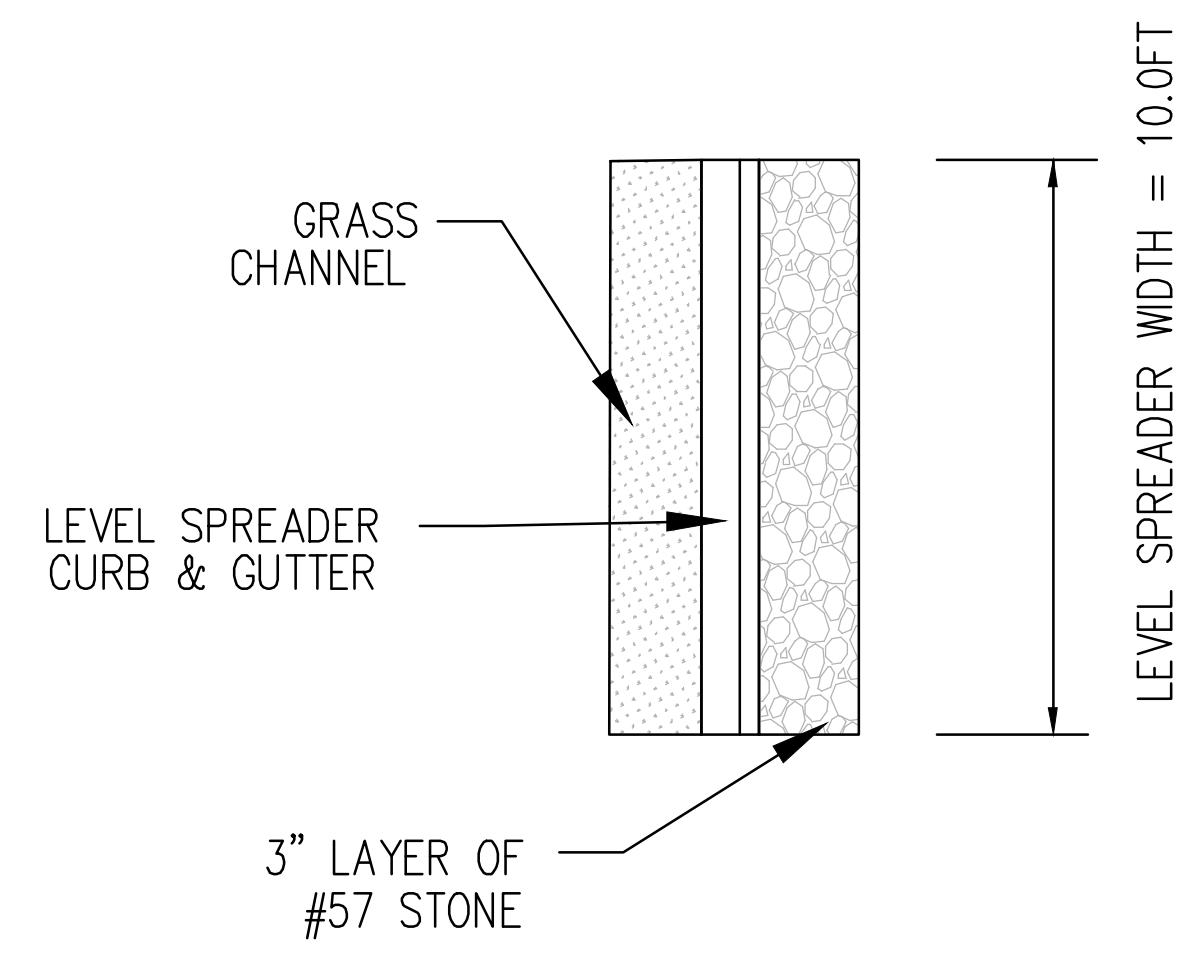
## VEGETATIVE FILTER STRIP

SCALE: N.T.S.



#### CONSTRUCTION SPECIFICATIONS

1. THE MATTING SHOULD BE A MINIMUM OF 4 FEET WIDE EXTENDING 6 INCHES OVER THE LIP AND BURIED 6 INCHES DEEP IN A VERTICAL TRENCH ON THE LOWER EDGE. THE UPPER EDGE SHOULD BUTT AGAINST SMOOTHLY CUT SOD AND BE SECURELY HELD IN PLACE WITH CLOSELY SPACED HEAVY DUTY WIRE STAPLES AT LEAST 12 INCHES LONG.
2. ENSURE THAT THE SPREADER IS LEVEL, FOR UNIFORM SPREADING OF STORM RUNOFF.
3. CONSTRUCT THE LEVEL SPREADER ON UNDISTURBED SOIL.  
(NOT ON FILL)
4. CONSTRUCT A 20 FOOT TRANSITION SECTION FROM THE DIVERSION CHANNEL TO BLEND SMOOTHLY WITH THE WIDTH AND DEPTH OF THE LEVEL SPREADER.
5. DISPERSE RUNOFF FROM THE SPREADER ACROSS A PROPERLY STABILIZED SLOPE, NOT TO EXCEED 10%, MAKE SURE THAT THE SLOPE IS SUFFICIENTLY SMOOTH TO KEEP THE FLOW FROM CONCENTRATING.
6. IMMEDIATELY AFTER IT'S CONSTRUCTION, APPROPRIATELY SEED AND MULCH THE ENTIRE DISTURBED AREA OF THE LEVEL SPREADER.

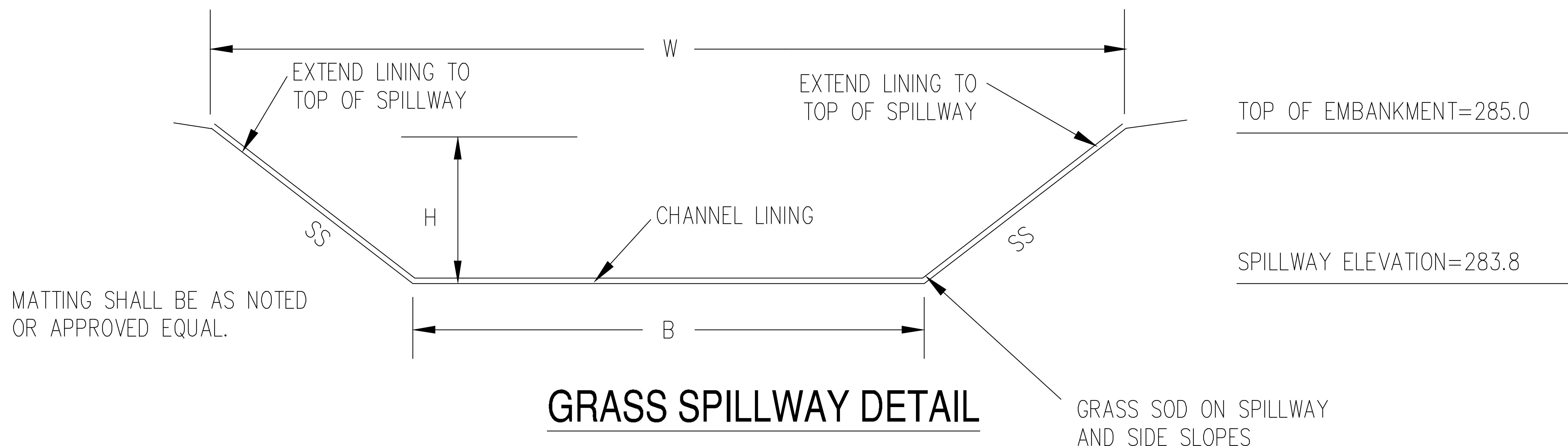


## LEVEL SPREADER

SCALE: N.T.S.

**GRASS NOTE:**  
GRASS SHALL BE EITHER HYBRID BERMUDA GRASS OR CENTIPEDE

SPILLWAY	FLOW Q(100)	LONG SLOPE(%)	H	B	W	SS	CHANNEL LINING	TOP OF EMBANKMENT ELEVATION	SPILLWAY ELEVATION
GRASS SPILLWAY	43.50 CFS	50.0%	1.2'	10.0'	17.2'	3:1	STRAW WITH NET NAG SHOREMAX W/ P550	285.0	283.8





North American Green  
 5401 St. Wendel-Cynthiana Rd.  
 Poseyville, Indiana 47633  
 Tel. 800.772.2040  
 >Fax 812.867.0247  
[www.nagreen.com](http://www.nagreen.com)  
 ECMDS v7.0

## SPILLWAY ANALYSIS

> > Grass Spillway

Name	Grass Spillway
Discharge	43.5
Peak Flow Period	1
Channel Slope	0.5
Channel Bottom Width	10
Low Flow Liner	
Retardence Class	C 6-12 in
Vegetation Type	Mix (Sod and Bunch)
Vegetation Density	Very Good 80-95%
Soil Type	Sandy Loam (GM)

Shoremax - Class C - Mix (Sod & Bunch) - Very Good 80-95%

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor	Remarks	Staple Pattern
Shoremax w/ P550 Unvegetated	Straight	43.5 cfs	16.92 ft/s	0.25 ft	0.024	8.5 lbs/ft <sup>2</sup>	7.83 lbs/ft <sup>2</sup>	1.09	STABLE	G
Underlying Substrate	Straight	43.5 cfs	16.92 ft/s	0.25 ft	0.024	8.05 lbs/ft <sup>2</sup>	7.49 lbs/ft <sup>2</sup>	1.07	STABLE	G
Shoremax w/ P550 Reinforced Vegetation	Straight	43.5 cfs	18.09 ft/s	0.23 ft	0.021	14 lbs/ft <sup>2</sup>	7.31 lbs/ft <sup>2</sup>	1.91	STABLE	G
Underlying Substrate	Straight	43.5 cfs	18.09 ft/s	0.23 ft	0.021	8.5 lbs/ft <sup>2</sup>	7.02 lbs/ft <sup>2</sup>	1.21	STABLE	G

# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Tuesday, 02 / 7 / 2023

## Hyd. No. 3

Post Through Pond

Hydrograph type	= Reservoir	Peak discharge	= 43.50 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.00 hrs
Time interval	= 2 min	Hyd. volume	= 139,470 cuft
Inflow hyd. No.	= 2 - Post Developed to Reservoir name	Reservoir name	= Wet Pond
Max. Elevation	= 284.52 ft	Max. Storage	= 55,383 cuft

Storage Indication method used.

## Hydrograph Discharge Table

( Printed values &gt;= 1.00% of Qp.)

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
11.00	2.770	282.16	0.494	0.144	----	----	0.340	----	----	----	----	0.484
11.03	2.833	282.18	0.554	0.145	----	----	0.402	----	----	----	----	0.547
11.07	2.919	282.21	0.623	0.145	----	----	0.471	----	----	----	----	0.615
11.10	3.030	282.23	0.713	0.145	----	----	0.553	----	----	----	----	0.698
11.13	3.156	282.25	0.804	0.145	----	----	0.637	----	----	----	----	0.781
11.17	3.287	282.27	0.897	0.145	----	----	0.722	----	----	----	----	0.867
11.20	3.418	282.30	0.992	0.145	----	----	0.809	----	----	----	----	0.953
11.23	3.550	282.32	1.087	0.145	----	----	0.911	----	----	----	----	1.056
11.27	3.683	282.34	1.183	0.145	----	----	1.016	----	----	----	----	1.161
11.30	3.815	282.37	1.281	0.145	----	----	1.123	----	----	----	----	1.268
11.33	3.947	282.39	1.379	0.146	----	----	1.231	----	----	----	----	1.376
11.37	4.080	282.42	1.495	0.146	----	----	1.349	----	----	----	----	1.495
11.40	4.214	282.44	1.619	0.146	----	----	1.473	----	----	----	----	1.618
11.43	4.347	282.47	1.743	0.146	----	----	1.597	----	----	----	----	1.743
11.47	4.480	282.49	1.867	0.146	----	----	1.721	----	----	----	----	1.867
11.50	4.614	282.52	2.003	0.146	----	----	1.854	----	----	----	----	2.001
11.53	5.057	282.54	2.152	0.146	----	----	2.000	----	----	----	----	2.147
11.57	6.423	282.58	2.342	0.147	----	----	2.185	----	----	----	----	2.332
11.60	8.817	282.62	2.644	0.147	----	----	2.468	----	----	----	----	2.615
11.63	11.84	282.70	3.121	0.147	----	----	2.898	----	----	----	----	3.046

Continues on next page...

Post Through Pond

**Peak Flow Period**  
**12.23hr-11.87hr = 0.36 hr**  
**~Use 1.0 hr**

**Hydrograph Discharge Table**

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs	
11.67	15.08	282.79	3.718	0.148	----	----	3.519	----	----	----	----	3.667	
11.70	18.34	282.91	4.524	0.149	----	----	4.349	----	----	----	----	4.498	
11.73	21.62	283.05	5.522	0.150	----	----	5.365	----	----	----	----	5.515	
11.77	25.03	283.20	6.681	0.151	----	----	6.530	----	----	----	----	6.681	
11.80	29.64	283.37	8.166	0.152	----	----	7.976	----	----	----	----	8.128	
11.83	36.39	283.57	10.03	0.153	----	----	9.834	----	----	----	----	9.987	
<b>11.87</b>	<b>44.71</b>	<b>283.82</b>	12.73	0.149	----	----	12.24	0.325	0.159	----	----	12.87	
11.90	53.86	284.07	20.78	0.113	----	----	12.98	7.681	3.747	----	----	24.53	
11.93	60.14 <<	284.28	25.93	0.061	----	----	9.488	16.38	8.793	----	----	34.72	
11.97	57.43	284.45	27.33	0.045	----	----	8.122	19.16	13.56	----	----	40.89	
<b>&lt;&lt;</b>	<b>12.00</b>	<b>44.64</b>	<b>284.52 &lt;&lt;</b>	27.76	0.040	----	----	7.737	19.98	15.75	----	----	43.50
12.03	27.85	284.47	27.46	0.043	----	----	8.006	19.40	14.18	----	----	41.63	
12.07	15.24	284.33	26.44	0.055	----	----	8.965	17.42	10.09	----	----	36.52	
12.10	9.427	284.17	23.71	0.087	----	----	11.53	12.09	5.900	----	----	29.61	
12.13	7.736	284.04	19.51	0.121	----	----	13.21	6.178	3.014	----	----	22.52	
12.17	7.401	283.93	15.98	0.135	----	----	13.12	2.722	1.328	----	----	17.30	
12.20	7.083	283.86	13.79	0.144	----	----	12.61	1.022	0.499	----	----	14.27	
<b>12.23</b>	<b>6.766</b>	<b>283.81</b>	12.38	0.150	----	----	12.11	0.097	0.047	----	----	12.41	
12.27	6.449	283.76	11.85	0.152	----	----	11.65	----	----	----	----	11.81	
12.30	6.131	283.71	11.42	0.153	----	----	11.21	----	----	----	----	11.36	
12.33	5.814	283.67	10.99	0.153	----	----	10.78	----	----	----	----	10.93	
12.37	5.497	283.63	10.55	0.153	----	----	10.36	----	----	----	----	10.51	
12.40	5.180	283.58	10.14	0.153	----	----	9.956	----	----	----	----	10.11	
12.43	4.862	283.54	9.764	0.153	----	----	9.566	----	----	----	----	9.719	
12.47	4.543	283.50	9.388	0.153	----	----	9.182	----	----	----	----	9.334	
12.50	4.225	283.46	9.004	0.153	----	----	8.814	----	----	----	----	8.967	
12.53	3.933	283.42	8.624	0.153	----	----	8.451	----	----	----	----	8.604	

Continues on next page...

Post Through Pond

**Hydrograph Discharge Table**

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
12.57	3.713	283.38	8.281	0.152	----	----	8.102	----	----	----	----	8.255
12.60	3.575	283.34	7.978	0.152	----	----	7.772	----	----	----	----	7.924
12.63	3.486	283.31	7.690	0.152	----	----	7.456	----	----	----	----	7.608
12.67	3.413	283.27	7.381	0.151	----	----	7.167	----	----	----	----	7.319
12.70	3.341	283.24	7.080	0.151	----	----	6.895	----	----	----	----	7.046
12.73	3.269	283.21	6.795	0.151	----	----	6.637	----	----	----	----	6.788
12.77	3.196	283.18	6.549	0.151	----	----	6.398	----	----	----	----	6.549
12.80	3.124	283.15	6.324	0.151	----	----	6.173	----	----	----	----	6.324
12.83	3.051	283.12	6.109	0.151	----	----	5.958	----	----	----	----	6.109
12.87	2.979	283.10	5.904	0.150	----	----	5.753	----	----	----	----	5.904
12.90	2.906	283.07	5.719	0.150	----	----	5.565	----	----	----	----	5.716
12.93	2.834	283.05	5.541	0.150	----	----	5.385	----	----	----	----	5.535
12.97	2.761	283.03	5.370	0.150	----	----	5.211	----	----	----	----	5.361
13.00	2.688	283.01	5.206	0.150	----	----	5.043	----	----	----	----	5.193
13.03	2.619	282.98	5.041	0.150	----	----	4.876	----	----	----	----	5.025
13.07	2.560	282.96	4.881	0.149	----	----	4.713	----	----	----	----	4.862
13.10	2.513	282.94	4.728	0.149	----	----	4.557	----	----	----	----	4.706
13.13	2.471	282.92	4.583	0.149	----	----	4.409	----	----	----	----	4.558
13.17	2.432	282.90	4.445	0.149	----	----	4.268	----	----	----	----	4.417
13.20	2.393	282.88	4.321	0.149	----	----	4.140	----	----	----	----	4.289
13.23	2.354	282.86	4.203	0.149	----	----	4.018	----	----	----	----	4.167
13.27	2.315	282.85	4.089	0.148	----	----	3.902	----	----	----	----	4.050
13.30	2.276	282.83	3.981	0.148	----	----	3.790	----	----	----	----	3.939
13.33	2.237	282.82	3.877	0.148	----	----	3.683	----	----	----	----	3.831
13.37	2.198	282.80	3.777	0.148	----	----	3.581	----	----	----	----	3.729
13.40	2.159	282.79	3.688	0.148	----	----	3.488	----	----	----	----	3.636
13.43	2.120	282.77	3.603	0.148	----	----	3.398	----	----	----	----	3.546
13.47	2.081	282.76	3.520	0.148	----	----	3.312	----	----	----	----	3.459

Continues on next page...

Post Through Pond

**Hydrograph Discharge Table**

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
13.50	2.042	282.75	3.440	0.148	----	----	3.228	----	----	----	----	3.376
13.53	2.004	282.73	3.363	0.147	----	----	3.147	----	----	----	----	3.295
13.57	1.969	282.72	3.288	0.147	----	----	3.069	----	----	----	----	3.216
13.60	1.938	282.71	3.216	0.147	----	----	2.994	----	----	----	----	3.141
13.63	1.910	282.70	3.146	0.147	----	----	2.921	----	----	----	----	3.068
13.67	1.882	282.69	3.074	0.147	----	----	2.856	----	----	----	----	3.003
13.70	1.854	282.68	3.003	0.147	----	----	2.792	----	----	----	----	2.940
13.73	1.826	282.67	2.936	0.147	----	----	2.731	----	----	----	----	2.878
13.77	1.798	282.66	2.870	0.147	----	----	2.672	----	----	----	----	2.819
13.80	1.770	282.65	2.806	0.147	----	----	2.614	----	----	----	----	2.761
13.83	1.742	282.64	2.744	0.147	----	----	2.558	----	----	----	----	2.705
13.87	1.714	282.63	2.683	0.147	----	----	2.503	----	----	----	----	2.650
13.90	1.686	282.62	2.625	0.147	----	----	2.451	----	----	----	----	2.597
13.93	1.658	282.61	2.568	0.147	----	----	2.399	----	----	----	----	2.546
13.97	1.630	282.60	2.512	0.147	----	----	2.349	----	----	----	----	2.495
14.00	1.602	282.60	2.461	0.147	----	----	2.301	----	----	----	----	2.448
14.03	1.576	282.59	2.416	0.147	----	----	2.257	----	----	----	----	2.404
14.07	1.556	282.58	2.372	0.147	----	----	2.214	----	----	----	----	2.361
14.10	1.541	282.57	2.329	0.147	----	----	2.172	----	----	----	----	2.319
14.13	1.530	282.57	2.287	0.147	----	----	2.132	----	----	----	----	2.279
14.17	1.520	282.56	2.248	0.146	----	----	2.093	----	----	----	----	2.240
14.20	1.511	282.55	2.210	0.146	----	----	2.056	----	----	----	----	2.203
14.23	1.501	282.55	2.173	0.146	----	----	2.020	----	----	----	----	2.167
14.27	1.491	282.54	2.138	0.146	----	----	1.986	----	----	----	----	2.132
14.30	1.481	282.53	2.104	0.146	----	----	1.953	----	----	----	----	2.099
14.33	1.472	282.53	2.071	0.146	----	----	1.921	----	----	----	----	2.067
14.37	1.462	282.52	2.039	0.146	----	----	1.890	----	----	----	----	2.036
14.40	1.452	282.52	2.008	0.146	----	----	1.860	----	----	----	----	2.006

Continues on next page...

Post Through Pond

**Hydrograph Discharge Table**

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
14.43	1.442	282.51	1.979	0.146	----	----	1.831	----	----	----	----	1.977
14.47	1.433	282.51	1.951	0.146	----	----	1.803	----	----	----	----	1.950
14.50	1.423	282.50	1.923	0.146	----	----	1.777	----	----	----	----	1.923
14.53	1.413	282.50	1.898	0.146	----	----	1.752	----	----	----	----	1.898
14.57	1.403	282.49	1.875	0.146	----	----	1.729	----	----	----	----	1.875
14.60	1.393	282.49	1.853	0.146	----	----	1.707	----	----	----	----	1.853
14.63	1.384	282.48	1.831	0.146	----	----	1.685	----	----	----	----	1.831
14.67	1.374	282.48	1.810	0.146	----	----	1.664	----	----	----	----	1.810
14.70	1.364	282.48	1.790	0.146	----	----	1.644	----	----	----	----	1.790
14.73	1.354	282.47	1.770	0.146	----	----	1.624	----	----	----	----	1.770
14.77	1.345	282.47	1.750	0.146	----	----	1.604	----	----	----	----	1.750
14.80	1.335	282.46	1.731	0.146	----	----	1.585	----	----	----	----	1.731
14.83	1.325	282.46	1.712	0.146	----	----	1.566	----	----	----	----	1.712
14.87	1.315	282.46	1.694	0.146	----	----	1.548	----	----	----	----	1.694
14.90	1.306	282.45	1.676	0.146	----	----	1.530	----	----	----	----	1.676
14.93	1.296	282.45	1.659	0.146	----	----	1.513	----	----	----	----	1.658
14.97	1.286	282.45	1.641	0.146	----	----	1.496	----	----	----	----	1.641
15.00	1.276	282.44	1.625	0.146	----	----	1.479	----	----	----	----	1.625
15.03	1.267	282.44	1.608	0.146	----	----	1.462	----	----	----	----	1.608
15.07	1.257	282.44	1.592	0.146	----	----	1.446	----	----	----	----	1.592
15.10	1.247	282.43	1.576	0.146	----	----	1.430	----	----	----	----	1.576
15.13	1.237	282.43	1.561	0.146	----	----	1.415	----	----	----	----	1.560
15.17	1.227	282.43	1.545	0.146	----	----	1.399	----	----	----	----	1.545
15.20	1.218	282.42	1.530	0.146	----	----	1.384	----	----	----	----	1.530
15.23	1.208	282.42	1.515	0.146	----	----	1.370	----	----	----	----	1.515
15.27	1.198	282.42	1.501	0.146	----	----	1.355	----	----	----	----	1.501
15.30	1.188	282.42	1.486	0.146	----	----	1.341	----	----	----	----	1.486
15.33	1.178	282.41	1.472	0.146	----	----	1.327	----	----	----	----	1.472

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Post Through Pond

**Hydrograph Discharge Table**

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
15.37	1.169	282.41	1.458	0.146	----	----	1.313	----	----	----	----	1.458
15.40	1.159	282.41	1.445	0.146	----	----	1.299	----	----	----	----	1.445
15.43	1.149	282.40	1.431	0.146	----	----	1.285	----	----	----	----	1.431
15.47	1.139	282.40	1.418	0.146	----	----	1.272	----	----	----	----	1.418
15.50	1.130	282.40	1.405	0.146	----	----	1.259	----	----	----	----	1.405
15.53	1.120	282.40	1.395	0.146	----	----	1.248	----	----	----	----	1.393
15.57	1.110	282.39	1.384	0.146	----	----	1.236	----	----	----	----	1.382
15.60	1.100	282.39	1.374	0.146	----	----	1.225	----	----	----	----	1.371
15.63	1.091	282.39	1.364	0.146	----	----	1.214	----	----	----	----	1.359
15.67	1.081	282.39	1.353	0.145	----	----	1.202	----	----	----	----	1.348
15.70	1.071	282.38	1.343	0.145	----	----	1.191	----	----	----	----	1.337
15.73	1.061	282.38	1.333	0.145	----	----	1.180	----	----	----	----	1.325
15.77	1.051	282.38	1.323	0.145	----	----	1.169	----	----	----	----	1.314
15.80	1.042	282.38	1.313	0.145	----	----	1.158	----	----	----	----	1.303
15.83	1.032	282.37	1.303	0.145	----	----	1.147	----	----	----	----	1.292
15.87	1.022	282.37	1.293	0.145	----	----	1.136	----	----	----	----	1.281
15.90	1.012	282.37	1.283	0.145	----	----	1.125	----	----	----	----	1.270
15.93	1.003	282.37	1.273	0.145	----	----	1.114	----	----	----	----	1.260
15.97	0.993	282.36	1.263	0.145	----	----	1.103	----	----	----	----	1.249
16.00	0.983	282.36	1.253	0.145	----	----	1.093	----	----	----	----	1.238
16.03	0.974	282.36	1.244	0.145	----	----	1.082	----	----	----	----	1.227
16.07	0.967	282.36	1.234	0.145	----	----	1.071	----	----	----	----	1.217
16.10	0.961	282.35	1.224	0.145	----	----	1.061	----	----	----	----	1.206
16.13	0.957	282.35	1.215	0.145	----	----	1.051	----	----	----	----	1.196
16.17	0.954	282.35	1.206	0.145	----	----	1.041	----	----	----	----	1.186
16.20	0.951	282.35	1.197	0.145	----	----	1.031	----	----	----	----	1.176
16.23	0.947	282.35	1.189	0.145	----	----	1.022	----	----	----	----	1.167
16.27	0.944	282.34	1.180	0.145	----	----	1.013	----	----	----	----	1.158

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Post Through Pond

**Hydrograph Discharge Table**

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
16.30	0.940	282.34	1.172	0.145	----	----	1.004	----	----	----	----	1.149
16.33	0.937	282.34	1.164	0.145	----	----	0.995	----	----	----	----	1.140
16.37	0.933	282.34	1.157	0.145	----	----	0.987	----	----	----	----	1.132
16.40	0.930	282.34	1.149	0.145	----	----	0.978	----	----	----	----	1.124
16.43	0.926	282.33	1.142	0.145	----	----	0.970	----	----	----	----	1.115
16.47	0.923	282.33	1.134	0.145	----	----	0.962	----	----	----	----	1.108
16.50	0.919	282.33	1.127	0.145	----	----	0.955	----	----	----	----	1.100
16.53	0.916	282.33	1.121	0.145	----	----	0.947	----	----	----	----	1.092
16.57	0.912	282.33	1.114	0.145	----	----	0.940	----	----	----	----	1.085
16.60	0.909	282.33	1.107	0.145	----	----	0.933	----	----	----	----	1.078
16.63	0.905	282.32	1.101	0.145	----	----	0.926	----	----	----	----	1.071
16.67	0.902	282.32	1.095	0.145	----	----	0.919	----	----	----	----	1.064
16.70	0.898	282.32	1.088	0.145	----	----	0.912	----	----	----	----	1.057
16.73	0.895	282.32	1.082	0.145	----	----	0.905	----	----	----	----	1.050
16.77	0.891	282.32	1.077	0.145	----	----	0.899	----	----	----	----	1.044
16.80	0.888	282.32	1.071	0.145	----	----	0.893	----	----	----	----	1.038
16.83	0.884	282.31	1.065	0.145	----	----	0.886	----	----	----	----	1.031
16.87	0.881	282.31	1.059	0.145	----	----	0.880	----	----	----	----	1.025
16.90	0.877	282.31	1.054	0.145	----	----	0.874	----	----	----	----	1.019
16.93	0.874	282.31	1.049	0.145	----	----	0.868	----	----	----	----	1.013
16.97	0.870	282.31	1.043	0.145	----	----	0.862	----	----	----	----	1.007
17.00	0.867	282.31	1.038	0.145	----	----	0.857	----	----	----	----	1.002
17.03	0.863	282.31	1.033	0.145	----	----	0.851	----	----	----	----	0.996
17.07	0.860	282.31	1.028	0.145	----	----	0.846	----	----	----	----	0.990
17.10	0.856	282.30	1.023	0.145	----	----	0.840	----	----	----	----	0.985
17.13	0.853	282.30	1.018	0.145	----	----	0.835	----	----	----	----	0.980
17.17	0.849	282.30	1.013	0.145	----	----	0.829	----	----	----	----	0.974
17.20	0.846	282.30	1.008	0.145	----	----	0.824	----	----	----	----	0.969

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Post Through Pond

**Hydrograph Discharge Table**

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
17.23	0.842	282.30	1.004	0.145	----	----	0.819	----	----	----	----	0.964
17.27	0.839	282.30	0.999	0.145	----	----	0.815	----	----	----	----	0.960
17.30	0.835	282.30	0.994	0.145	----	----	0.811	----	----	----	----	0.956
17.33	0.832	282.30	0.990	0.145	----	----	0.806	----	----	----	----	0.951
17.37	0.828	282.30	0.985	0.145	----	----	0.802	----	----	----	----	0.947
17.40	0.825	282.29	0.980	0.145	----	----	0.798	----	----	----	----	0.943
17.43	0.821	282.29	0.976	0.145	----	----	0.794	----	----	----	----	0.939
17.47	0.818	282.29	0.971	0.145	----	----	0.790	----	----	----	----	0.934
17.50	0.814	282.29	0.967	0.145	----	----	0.786	----	----	----	----	0.930
17.53	0.811	282.29	0.962	0.145	----	----	0.781	----	----	----	----	0.926
17.57	0.807	282.29	0.958	0.145	----	----	0.777	----	----	----	----	0.922
17.60	0.804	282.29	0.953	0.145	----	----	0.773	----	----	----	----	0.918
17.63	0.800	282.29	0.949	0.145	----	----	0.769	----	----	----	----	0.914
17.67	0.797	282.29	0.945	0.145	----	----	0.765	----	----	----	----	0.910
17.70	0.793	282.28	0.940	0.145	----	----	0.761	----	----	----	----	0.906
17.73	0.790	282.28	0.936	0.145	----	----	0.757	----	----	----	----	0.902
17.77	0.786	282.28	0.931	0.145	----	----	0.753	----	----	----	----	0.898
17.80	0.783	282.28	0.927	0.145	----	----	0.749	----	----	----	----	0.894
17.83	0.779	282.28	0.923	0.145	----	----	0.745	----	----	----	----	0.890
17.87	0.776	282.28	0.919	0.145	----	----	0.742	----	----	----	----	0.886
17.90	0.772	282.28	0.914	0.145	----	----	0.738	----	----	----	----	0.882
17.93	0.769	282.28	0.910	0.145	----	----	0.734	----	----	----	----	0.878
17.97	0.765	282.28	0.906	0.145	----	----	0.730	----	----	----	----	0.875
18.00	0.762	282.27	0.902	0.145	----	----	0.726	----	----	----	----	0.871
18.03	0.758	282.27	0.897	0.145	----	----	0.722	----	----	----	----	0.867
18.07	0.755	282.27	0.893	0.145	----	----	0.718	----	----	----	----	0.863
18.10	0.751	282.27	0.889	0.145	----	----	0.714	----	----	----	----	0.859
18.13	0.748	282.27	0.885	0.145	----	----	0.711	----	----	----	----	0.855

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Post Through Pond

**Hydrograph Discharge Table**

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
18.17	0.745	282.27	0.881	0.145	----	----	0.707	----	----	----	----	0.851
18.20	0.741	282.27	0.876	0.145	----	----	0.703	----	----	----	----	0.848
18.23	0.737	282.27	0.872	0.145	----	----	0.699	----	----	----	----	0.844
18.27	0.734	282.27	0.868	0.145	----	----	0.695	----	----	----	----	0.840
18.30	0.731	282.27	0.864	0.145	----	----	0.692	----	----	----	----	0.836
18.33	0.727	282.26	0.860	0.145	----	----	0.688	----	----	----	----	0.833
18.37	0.724	282.26	0.856	0.145	----	----	0.684	----	----	----	----	0.829
18.40	0.720	282.26	0.852	0.145	----	----	0.680	----	----	----	----	0.825
18.43	0.717	282.26	0.848	0.145	----	----	0.677	----	----	----	----	0.821
18.47	0.713	282.26	0.844	0.145	----	----	0.673	----	----	----	----	0.818
18.50	0.710	282.26	0.840	0.145	----	----	0.669	----	----	----	----	0.814
18.53	0.706	282.26	0.836	0.145	----	----	0.665	----	----	----	----	0.810
18.57	0.703	282.26	0.832	0.145	----	----	0.662	----	----	----	----	0.807
18.60	0.699	282.26	0.828	0.145	----	----	0.658	----	----	----	----	0.803
18.63	0.696	282.26	0.823	0.145	----	----	0.654	----	----	----	----	0.799
18.67	0.692	282.25	0.819	0.145	----	----	0.651	----	----	----	----	0.796
18.70	0.689	282.25	0.816	0.145	----	----	0.647	----	----	----	----	0.792
18.73	0.685	282.25	0.812	0.145	----	----	0.643	----	----	----	----	0.788
18.77	0.682	282.25	0.808	0.145	----	----	0.640	----	----	----	----	0.785
18.80	0.678	282.25	0.804	0.145	----	----	0.636	----	----	----	----	0.781
18.83	0.675	282.25	0.800	0.145	----	----	0.633	----	----	----	----	0.777
18.87	0.671	282.25	0.796	0.145	----	----	0.629	----	----	----	----	0.774
18.90	0.668	282.25	0.792	0.145	----	----	0.625	----	----	----	----	0.770
18.93	0.664	282.25	0.788	0.145	----	----	0.622	----	----	----	----	0.766
18.97	0.661	282.25	0.784	0.145	----	----	0.618	----	----	----	----	0.763
19.00	0.657	282.24	0.780	0.145	----	----	0.614	----	----	----	----	0.759
19.03	0.654	282.24	0.776	0.145	----	----	0.611	----	----	----	----	0.755
19.07	0.650	282.24	0.772	0.145	----	----	0.607	----	----	----	----	0.752

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Post Through Pond

**Hydrograph Discharge Table**

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
19.10	0.647	282.24	0.768	0.145	----	----	0.604	----	----	----	----	0.748
19.13	0.643	282.24	0.764	0.145	----	----	0.600	----	----	----	----	0.745
19.17	0.640	282.24	0.760	0.145	----	----	0.596	----	----	----	----	0.741
19.20	0.636	282.24	0.756	0.145	----	----	0.593	----	----	----	----	0.737
19.23	0.633	282.24	0.752	0.145	----	----	0.589	----	----	----	----	0.734
19.27	0.629	282.24	0.748	0.145	----	----	0.585	----	----	----	----	0.730
19.30	0.626	282.24	0.744	0.145	----	----	0.582	----	----	----	----	0.727
19.33	0.622	282.24	0.740	0.145	----	----	0.578	----	----	----	----	0.723
19.37	0.619	282.23	0.736	0.145	----	----	0.575	----	----	----	----	0.719
19.40	0.615	282.23	0.733	0.145	----	----	0.571	----	----	----	----	0.716
19.43	0.612	282.23	0.729	0.145	----	----	0.568	----	----	----	----	0.712
19.47	0.608	282.23	0.725	0.145	----	----	0.564	----	----	----	----	0.709
19.50	0.605	282.23	0.721	0.145	----	----	0.560	----	----	----	----	0.705
19.53	0.601	282.23	0.717	0.145	----	----	0.557	----	----	----	----	0.702
19.57	0.598	282.23	0.713	0.145	----	----	0.553	----	----	----	----	0.698
19.60	0.594	282.23	0.709	0.145	----	----	0.550	----	----	----	----	0.694
19.63	0.591	282.23	0.705	0.145	----	----	0.546	----	----	----	----	0.691
19.67	0.587	282.23	0.701	0.145	----	----	0.543	----	----	----	----	0.687
19.70	0.584	282.22	0.698	0.145	----	----	0.539	----	----	----	----	0.684
19.73	0.580	282.22	0.694	0.145	----	----	0.536	----	----	----	----	0.680
19.77	0.577	282.22	0.690	0.145	----	----	0.532	----	----	----	----	0.677
19.80	0.573	282.22	0.686	0.145	----	----	0.528	----	----	----	----	0.673
19.83	0.570	282.22	0.682	0.145	----	----	0.525	----	----	----	----	0.670
19.87	0.566	282.22	0.678	0.145	----	----	0.521	----	----	----	----	0.666
19.90	0.563	282.22	0.674	0.145	----	----	0.518	----	----	----	----	0.662
19.93	0.559	282.22	0.670	0.145	----	----	0.514	----	----	----	----	0.659
19.97	0.556	282.22	0.667	0.145	----	----	0.511	----	----	----	----	0.655
20.00	0.552	282.22	0.663	0.145	----	----	0.507	----	----	----	----	0.652

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Post Through Pond

**Hydrograph Discharge Table**

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
20.03	0.549	282.22	0.659	0.145	----	----	0.504	----	----	----	----	0.648
20.07	0.547	282.21	0.655	0.145	----	----	0.500	----	----	----	----	0.645
20.10	0.545	282.21	0.651	0.145	----	----	0.497	----	----	----	----	0.641
20.13	0.544	282.21	0.648	0.145	----	----	0.493	----	----	----	----	0.638
20.17	0.544	282.21	0.644	0.145	----	----	0.490	----	----	----	----	0.635
20.20	0.543	282.21	0.641	0.145	----	----	0.487	----	----	----	----	0.632
20.23	0.542	282.21	0.637	0.145	----	----	0.484	----	----	----	----	0.628
20.27	0.542	282.21	0.634	0.145	----	----	0.481	----	----	----	----	0.625
20.30	0.541	282.21	0.631	0.145	----	----	0.478	----	----	----	----	0.622
20.33	0.540	282.21	0.628	0.145	----	----	0.475	----	----	----	----	0.620
20.37	0.539	282.21	0.624	0.145	----	----	0.472	----	----	----	----	0.617
20.40	0.539	282.21	0.621	0.145	----	----	0.469	----	----	----	----	0.614
20.43	0.538	282.21	0.619	0.145	----	----	0.467	----	----	----	----	0.611
20.47	0.537	282.20	0.616	0.145	----	----	0.464	----	----	----	----	0.609
20.50	0.537	282.20	0.613	0.145	----	----	0.462	----	----	----	----	0.606
20.53	0.536	282.20	0.610	0.145	----	----	0.459	----	----	----	----	0.604
20.57	0.535	282.20	0.608	0.145	----	----	0.457	----	----	----	----	0.602
20.60	0.535	282.20	0.605	0.145	----	----	0.455	----	----	----	----	0.599
20.63	0.534	282.20	0.603	0.145	----	----	0.452	----	----	----	----	0.597
20.67	0.533	282.20	0.600	0.145	----	----	0.450	----	----	----	----	0.595
20.70	0.532	282.20	0.598	0.145	----	----	0.448	----	----	----	----	0.593
20.73	0.532	282.20	0.596	0.145	----	----	0.446	----	----	----	----	0.591
20.77	0.531	282.20	0.594	0.145	----	----	0.444	----	----	----	----	0.589
20.80	0.530	282.20	0.593	0.145	----	----	0.443	----	----	----	----	0.587
20.83	0.530	282.20	0.592	0.145	----	----	0.441	----	----	----	----	0.586
20.87	0.529	282.20	0.590	0.145	----	----	0.440	----	----	----	----	0.584
20.90	0.528	282.20	0.589	0.145	----	----	0.438	----	----	----	----	0.583
20.93	0.528	282.20	0.587	0.145	----	----	0.437	----	----	----	----	0.581

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Post Through Pond

**Hydrograph Discharge Table**

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
20.97	0.527	282.20	0.586	0.145	----	----	0.435	----	----	----	----	0.580
21.00	0.526	282.20	0.584	0.145	----	----	0.434	----	----	----	----	0.578
21.03	0.526	282.20	0.583	0.145	----	----	0.432	----	----	----	----	0.577
21.07	0.525	282.19	0.582	0.145	----	----	0.431	----	----	----	----	0.576
21.10	0.524	282.19	0.580	0.145	----	----	0.430	----	----	----	----	0.574
21.13	0.523	282.19	0.579	0.145	----	----	0.428	----	----	----	----	0.573
21.17	0.523	282.19	0.578	0.145	----	----	0.427	----	----	----	----	0.572
21.20	0.522	282.19	0.576	0.145	----	----	0.426	----	----	----	----	0.570
21.23	0.521	282.19	0.575	0.145	----	----	0.424	----	----	----	----	0.569
21.27	0.521	282.19	0.574	0.145	----	----	0.423	----	----	----	----	0.568
21.30	0.520	282.19	0.573	0.145	----	----	0.422	----	----	----	----	0.566
21.33	0.519	282.19	0.571	0.145	----	----	0.420	----	----	----	----	0.565
21.37	0.519	282.19	0.570	0.145	----	----	0.419	----	----	----	----	0.564
21.40	0.518	282.19	0.569	0.145	----	----	0.418	----	----	----	----	0.563
21.43	0.517	282.19	0.568	0.145	----	----	0.417	----	----	----	----	0.561
21.47	0.516	282.19	0.567	0.145	----	----	0.416	----	----	----	----	0.560
21.50	0.516	282.19	0.566	0.145	----	----	0.414	----	----	----	----	0.559
21.53	0.515	282.19	0.564	0.145	----	----	0.413	----	----	----	----	0.558
21.57	0.514	282.19	0.563	0.145	----	----	0.412	----	----	----	----	0.557
21.60	0.514	282.19	0.562	0.145	----	----	0.411	----	----	----	----	0.555
21.63	0.513	282.19	0.561	0.145	----	----	0.410	----	----	----	----	0.554
21.67	0.512	282.19	0.560	0.145	----	----	0.409	----	----	----	----	0.553
21.70	0.512	282.19	0.559	0.145	----	----	0.407	----	----	----	----	0.552
21.73	0.511	282.19	0.558	0.145	----	----	0.406	----	----	----	----	0.551
21.77	0.510	282.19	0.557	0.145	----	----	0.405	----	----	----	----	0.550
21.80	0.509	282.19	0.556	0.145	----	----	0.404	----	----	----	----	0.549
21.83	0.509	282.18	0.555	0.145	----	----	0.403	----	----	----	----	0.548
21.87	0.508	282.18	0.554	0.145	----	----	0.402	----	----	----	----	0.547

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Post Through Pond

**Hydrograph Discharge Table**

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
21.90	0.507	282.18	0.553	0.145	----	----	0.401	----	----	----	----	0.546
21.93	0.507	282.18	0.552	0.145	----	----	0.400	----	----	----	----	0.544
21.97	0.506	282.18	0.551	0.145	----	----	0.399	----	----	----	----	0.543
22.00	0.505	282.18	0.550	0.145	----	----	0.398	----	----	----	----	0.542
22.03	0.505	282.18	0.549	0.145	----	----	0.397	----	----	----	----	0.541
22.07	0.504	282.18	0.548	0.145	----	----	0.396	----	----	----	----	0.540
22.10	0.503	282.18	0.547	0.145	----	----	0.395	----	----	----	----	0.539
22.13	0.502	282.18	0.546	0.145	----	----	0.394	----	----	----	----	0.538
22.17	0.502	282.18	0.545	0.145	----	----	0.393	----	----	----	----	0.537
22.20	0.501	282.18	0.544	0.145	----	----	0.392	----	----	----	----	0.536
22.23	0.500	282.18	0.543	0.145	----	----	0.391	----	----	----	----	0.535
22.27	0.500	282.18	0.542	0.145	----	----	0.390	----	----	----	----	0.535
22.30	0.499	282.18	0.541	0.145	----	----	0.389	----	----	----	----	0.534
22.33	0.498	282.18	0.540	0.145	----	----	0.388	----	----	----	----	0.533
22.37	0.498	282.18	0.539	0.144	----	----	0.387	----	----	----	----	0.532
22.40	0.497	282.18	0.539	0.144	----	----	0.386	----	----	----	----	0.531
22.43	0.496	282.18	0.538	0.144	----	----	0.385	----	----	----	----	0.530
22.47	0.496	282.18	0.537	0.144	----	----	0.384	----	----	----	----	0.529
22.50	0.495	282.18	0.536	0.144	----	----	0.383	----	----	----	----	0.528
22.53	0.494	282.18	0.535	0.144	----	----	0.383	----	----	----	----	0.527
22.57	0.493	282.18	0.534	0.144	----	----	0.382	----	----	----	----	0.526
22.60	0.493	282.18	0.533	0.144	----	----	0.381	----	----	----	----	0.525
22.63	0.492	282.18	0.532	0.144	----	----	0.380	----	----	----	----	0.524
22.67	0.491	282.18	0.532	0.144	----	----	0.379	----	----	----	----	0.523
22.70	0.491	282.18	0.531	0.144	----	----	0.378	----	----	----	----	0.523
22.73	0.490	282.18	0.530	0.144	----	----	0.377	----	----	----	----	0.522
22.77	0.489	282.18	0.529	0.144	----	----	0.376	----	----	----	----	0.521
22.80	0.488	282.18	0.528	0.144	----	----	0.376	----	----	----	----	0.520

Continues on next page...

Post Through Pond

**Hydrograph Discharge Table**

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
22.83	0.488	282.18	0.527	0.144	----	----	0.375	----	----	----	----	0.519
22.87	0.487	282.17	0.527	0.144	----	----	0.374	----	----	----	----	0.518
22.90	0.486	282.17	0.526	0.144	----	----	0.373	----	----	----	----	0.517
22.93	0.486	282.17	0.525	0.144	----	----	0.372	----	----	----	----	0.517
22.97	0.485	282.17	0.524	0.144	----	----	0.371	----	----	----	----	0.516
23.00	0.484	282.17	0.523	0.144	----	----	0.370	----	----	----	----	0.515
23.03	0.484	282.17	0.523	0.144	----	----	0.370	----	----	----	----	0.514
23.07	0.483	282.17	0.522	0.144	----	----	0.369	----	----	----	----	0.513
23.10	0.482	282.17	0.521	0.144	----	----	0.368	----	----	----	----	0.512
23.13	0.481	282.17	0.520	0.144	----	----	0.367	----	----	----	----	0.512
23.17	0.481	282.17	0.519	0.144	----	----	0.366	----	----	----	----	0.511
23.20	0.480	282.17	0.519	0.144	----	----	0.365	----	----	----	----	0.510
23.23	0.479	282.17	0.518	0.144	----	----	0.365	----	----	----	----	0.509
23.27	0.479	282.17	0.517	0.144	----	----	0.364	----	----	----	----	0.508
23.30	0.478	282.17	0.516	0.144	----	----	0.363	----	----	----	----	0.507
23.33	0.477	282.17	0.515	0.144	----	----	0.362	----	----	----	----	0.507
23.37	0.477	282.17	0.515	0.144	----	----	0.361	----	----	----	----	0.506
23.40	0.476	282.17	0.514	0.144	----	----	0.361	----	----	----	----	0.505
23.43	0.475	282.17	0.513	0.144	----	----	0.360	----	----	----	----	0.504
23.47	0.475	282.17	0.512	0.144	----	----	0.359	----	----	----	----	0.503
23.50	0.474	282.17	0.512	0.144	----	----	0.358	----	----	----	----	0.503
23.53	0.473	282.17	0.511	0.144	----	----	0.357	----	----	----	----	0.502
23.57	0.472	282.17	0.510	0.144	----	----	0.357	----	----	----	----	0.501
23.60	0.472	282.17	0.509	0.144	----	----	0.356	----	----	----	----	0.500
23.63	0.471	282.17	0.509	0.144	----	----	0.355	----	----	----	----	0.499
23.67	0.470	282.17	0.508	0.144	----	----	0.354	----	----	----	----	0.499
23.70	0.470	282.17	0.507	0.144	----	----	0.353	----	----	----	----	0.498
23.73	0.469	282.17	0.506	0.144	----	----	0.353	----	----	----	----	0.497

Continues on next page...

Post Through Pond

**Hydrograph Discharge Table**

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
23.77	0.468	282.17	0.506	0.144	----	----	0.352	----	----	----	----	0.496
23.80	0.468	282.17	0.505	0.144	----	----	0.351	----	----	----	----	0.496
23.83	0.467	282.17	0.504	0.144	----	----	0.350	----	----	----	----	0.495
23.87	0.466	282.17	0.503	0.144	----	----	0.350	----	----	----	----	0.494
23.90	0.465	282.17	0.503	0.144	----	----	0.349	----	----	----	----	0.493
23.93	0.465	282.17	0.502	0.144	----	----	0.348	----	----	----	----	0.493
23.97	0.464	282.17	0.501	0.144	----	----	0.347	----	----	----	----	0.492
24.00	0.463	282.17	0.500	0.144	----	----	0.347	----	----	----	----	0.491
24.03	0.370	282.16	0.498	0.144	----	----	0.345	----	----	----	----	0.489
24.07	0.185	282.16	0.493	0.144	----	----	0.339	----	----	----	----	0.483
24.10	0.062	282.16	0.484	0.144	----	----	0.329	----	----	----	----	0.474
24.13	0.000	282.16	0.472	0.144	----	----	0.317	----	----	----	----	0.461
24.17	0.000	282.15	0.460	0.144	----	----	0.305	----	----	----	----	0.449
24.20	0.000	282.15	0.448	0.144	----	----	0.292	----	----	----	----	0.437

*...End*

# Pond Report

5

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Wednesday, 02 / 8 / 2023

## Pond No. 1 - Wet Pond

### Pond Data

Contours -User-defined contour areas. Average end area method used for volume calculation. Beginning Elevation = 280.00 ft

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	280.00	8,385	0	0
0.50	280.50	9,635	4,505	4,505
1.00	281.00	10,395	5,008	9,513
1.70	281.70	11,535	7,676	17,188
2.00	282.00	11,940	3,521	20,709
3.00	283.00	13,325	12,633	33,342
4.00	284.00	14,765	14,045	47,387
5.00	285.00	16,265	15,515	62,902

### Culvert / Orifice Structures

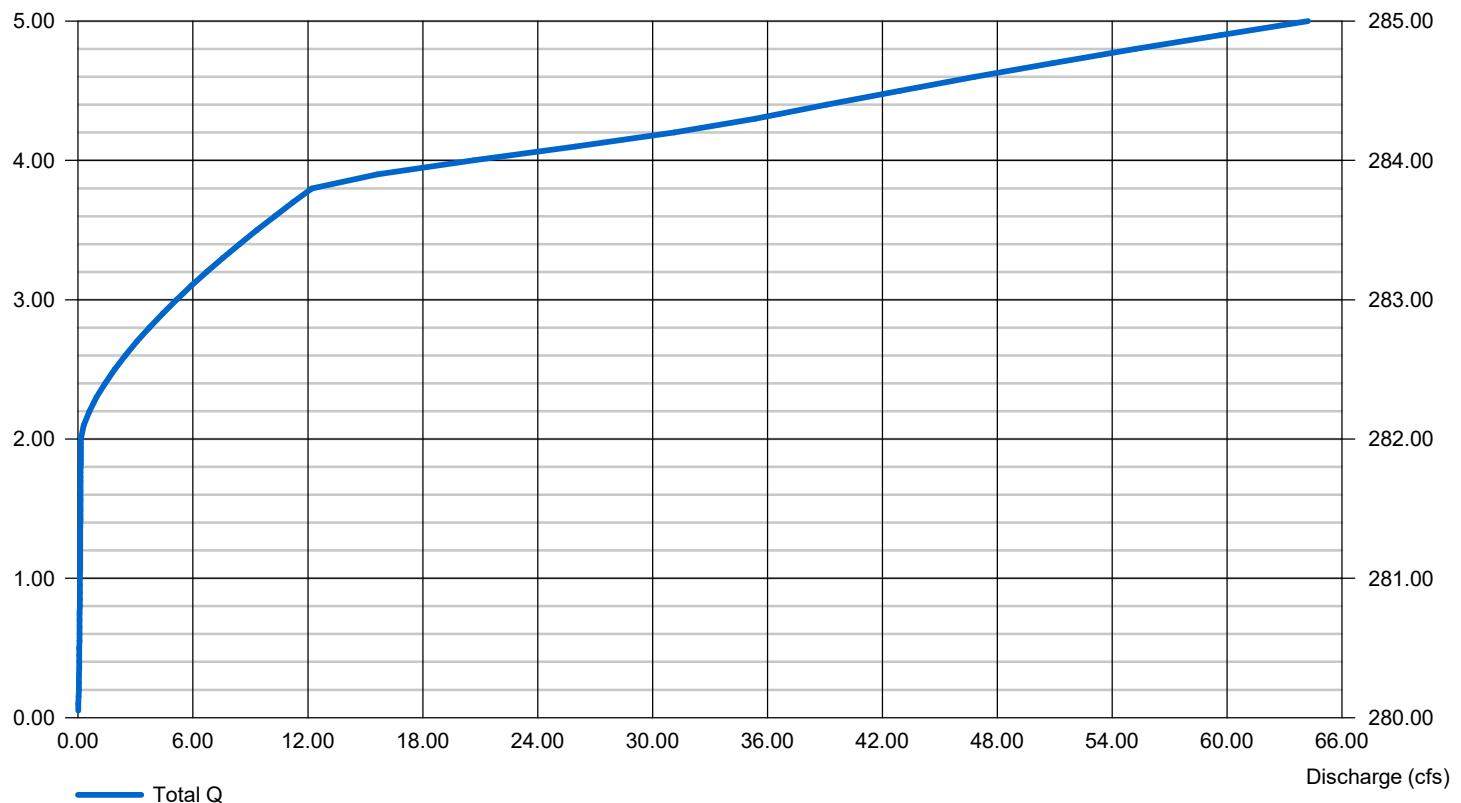
	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 24.00	2.00	Inactive	Inactive	Crest Len (ft)	= 1.50	20.50	10.00	Inactive
Span (in)	= 24.00	2.00	0.00	0.00	Crest El. (ft)	= 282.00	283.80	283.80	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	2.60	2.60	3.33
Invert El. (ft)	= 280.00	280.00	0.00	0.00	Weir Type	= Rect	Broad	Broad	---
Length (ft)	= 32.00	0.50	0.00	0.00	Multi-Stage	= Yes	Yes	No	No
Slope (%)	= 1.56	1.00	0.00	n/a	Exfil.(in/hr)	= 0.000 (by Contour)			
N-Value	= .013	.013	.013	n/a	TW Elev. (ft)	= 0.00			
Orifice Coeff.	= 0.60	0.60	0.60	0.60					
Multi-Stage	= n/a	Yes	No	No					

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage (ft)

### Stage / Discharge

Elev (ft)



# Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

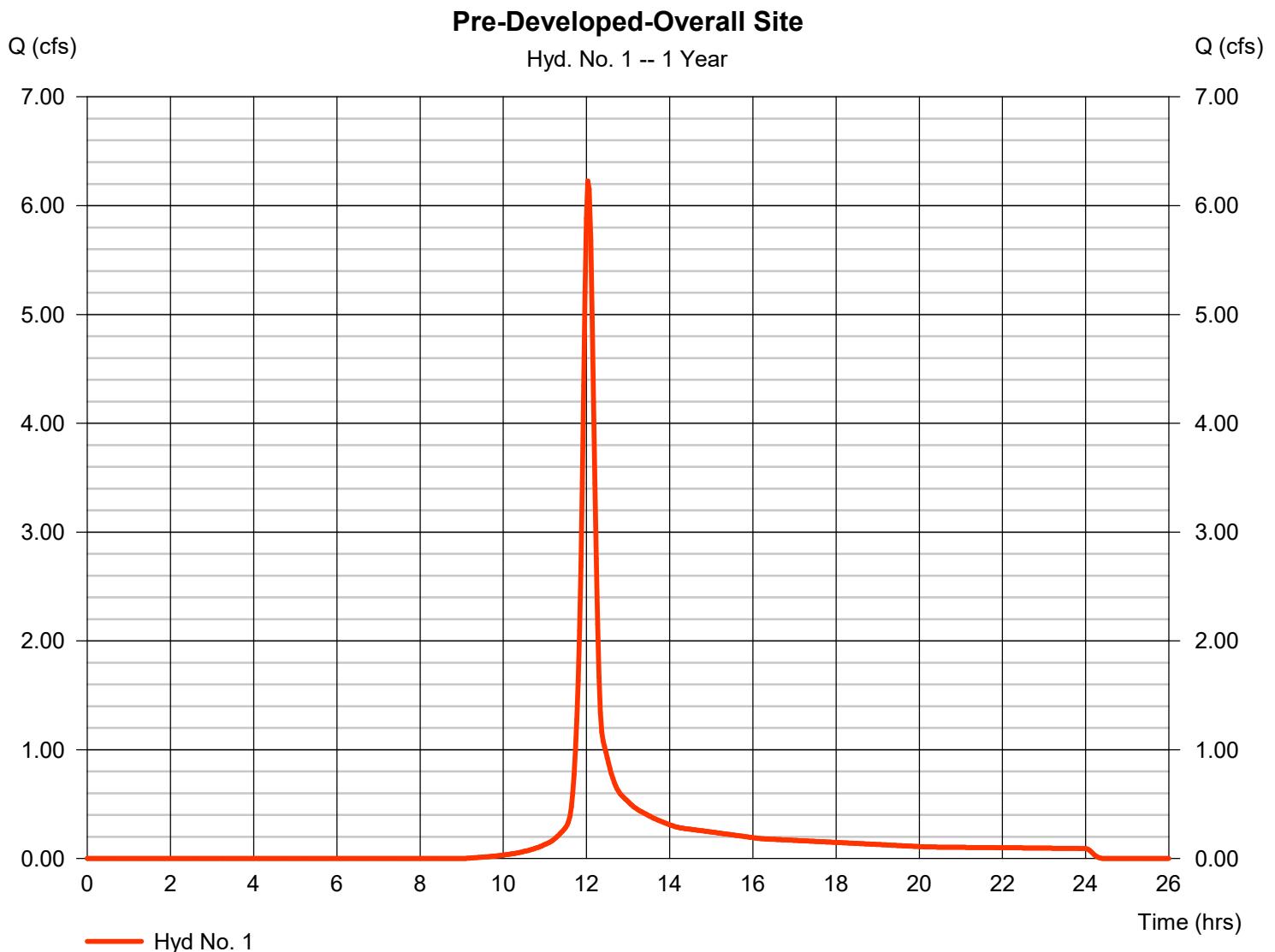
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	6.225	2	722	17,526	----	----	----	Pre-Developed-Overall Site
2	SCS Runoff	20.08	2	716	43,652	----	----	----	Post Developed to Pond
3	Reservoir	1.561	2	748	42,932	2	282.43	26,143	Post Through Pond
4	SCS Runoff	0.800	2	720	2,079	----	----	----	Post Developed Bypass
6	SCS Runoff	2.661	2	144	10,560	----	----	----	1.0 Post-Developed to Pond
7	Reservoir	0.098	2	364	10,415	6	280.99	9,385	1.0inPost Through Pond
Wet Pond1-Zebulon.gpw				Return Period: 1 Year				Wednesday, 02 / 8 / 2023	

# Hydrograph Report

## Hyd. No. 1

### Pre-Developed-Overall Site

Hydrograph type	= SCS Runoff	Peak discharge	= 6.225 cfs
Storm frequency	= 1 yrs	Time to peak	= 12.03 hrs
Time interval	= 2 min	Hyd. volume	= 17,526 cuft
Drainage area	= 3.710 ac	Curve number	= 83
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 14.00 min
Total precip.	= 2.86 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

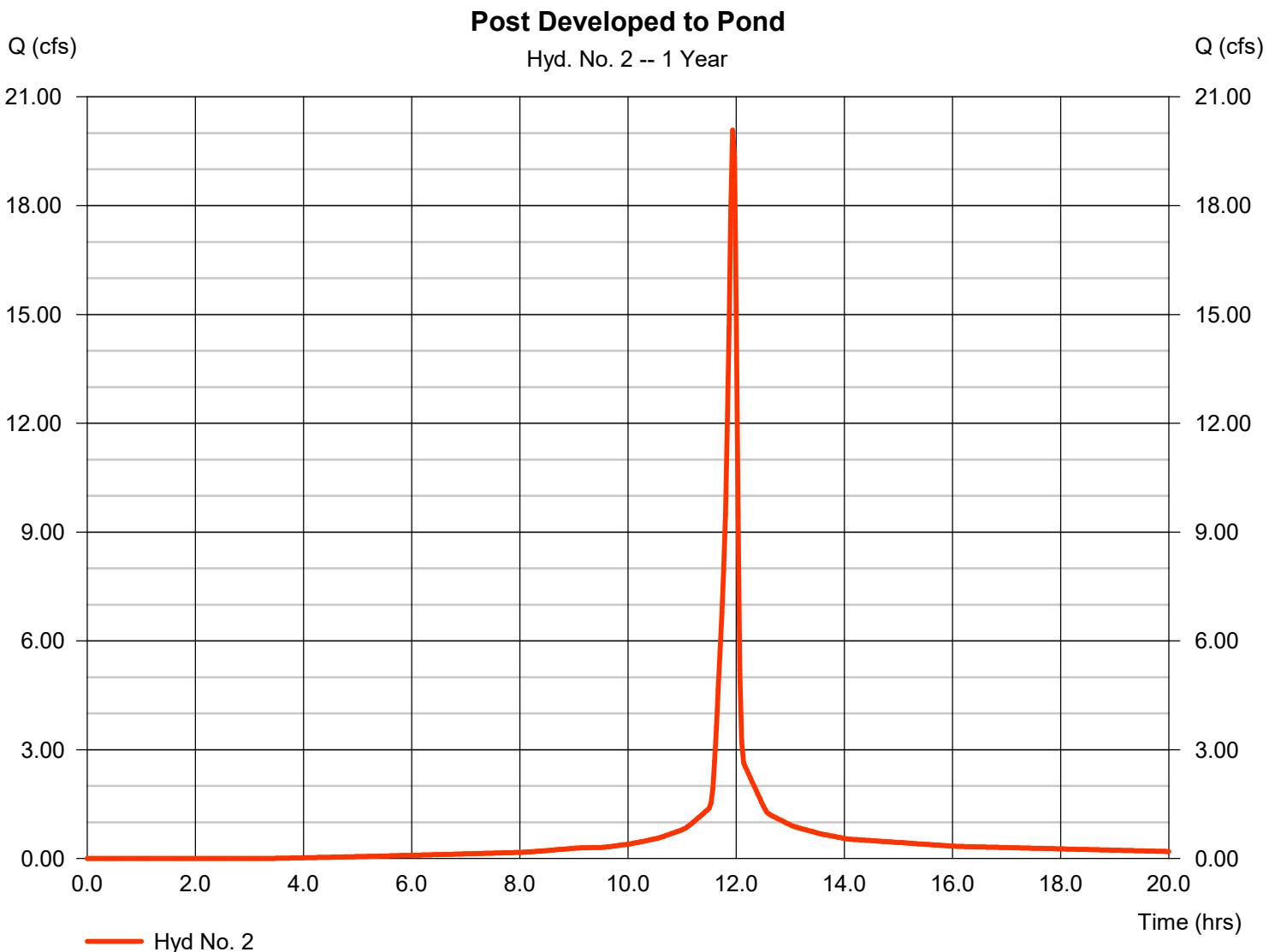


# Hydrograph Report

## Hyd. No. 2

Post Developed to Pond

Hydrograph type	= SCS Runoff	Peak discharge	= 20.08 cfs
Storm frequency	= 1 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 43,652 cuft
Drainage area	= 5.570 ac	Curve number	= 94.9
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 2.86 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

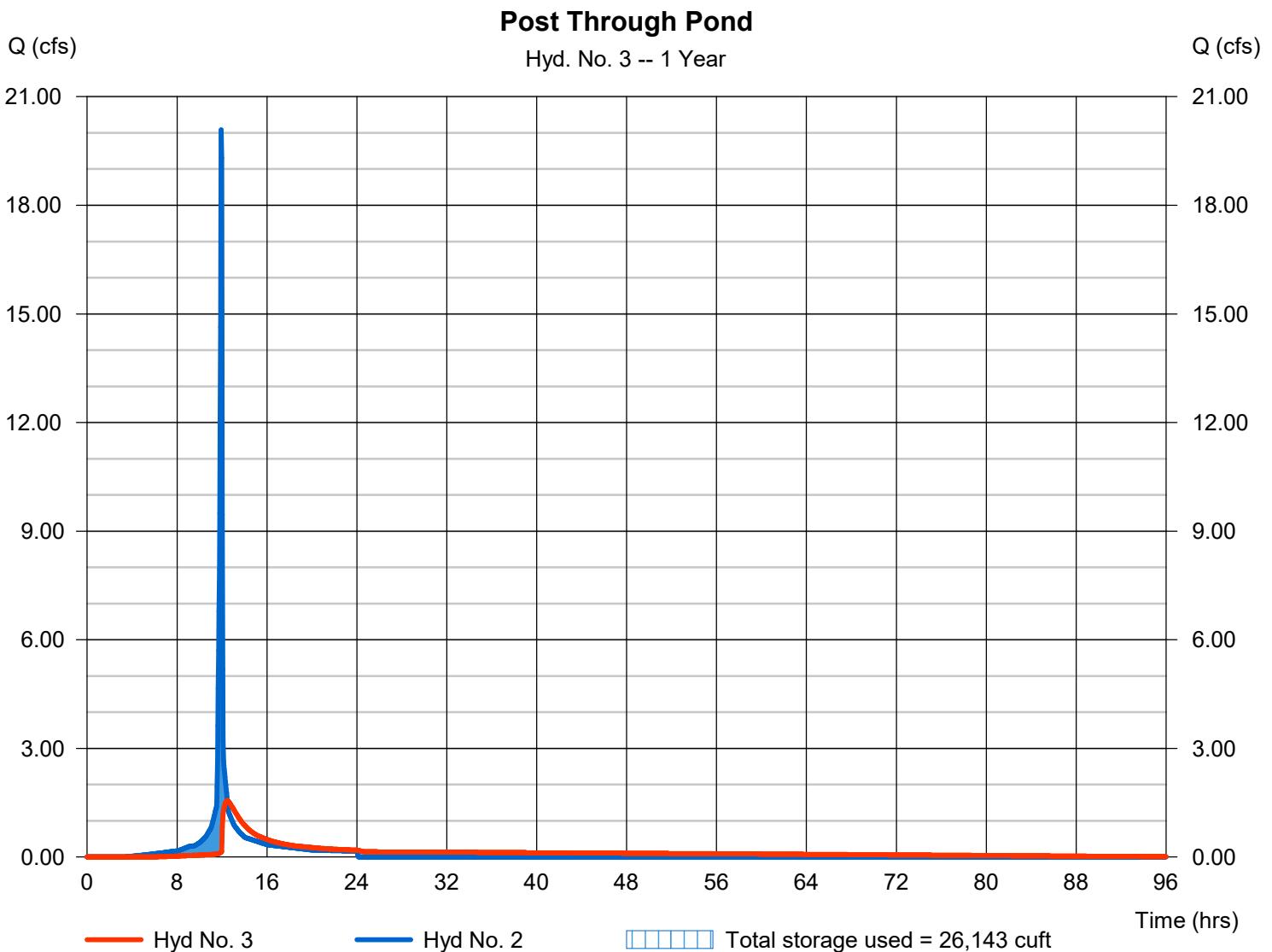
Wednesday, 02 / 8 / 2023

## Hyd. No. 3

### Post Through Pond

Hydrograph type	= Reservoir	Peak discharge	= 1.561 cfs
Storm frequency	= 1 yrs	Time to peak	= 12.47 hrs
Time interval	= 2 min	Hyd. volume	= 42,932 cuft
Inflow hyd. No.	= 2 - Post Developed to Pond	Max. Elevation	= 282.43 ft
Reservoir name	= Wet Pond	Max. Storage	= 26,143 cuft

Storage Indication method used.



# Hydrograph Report

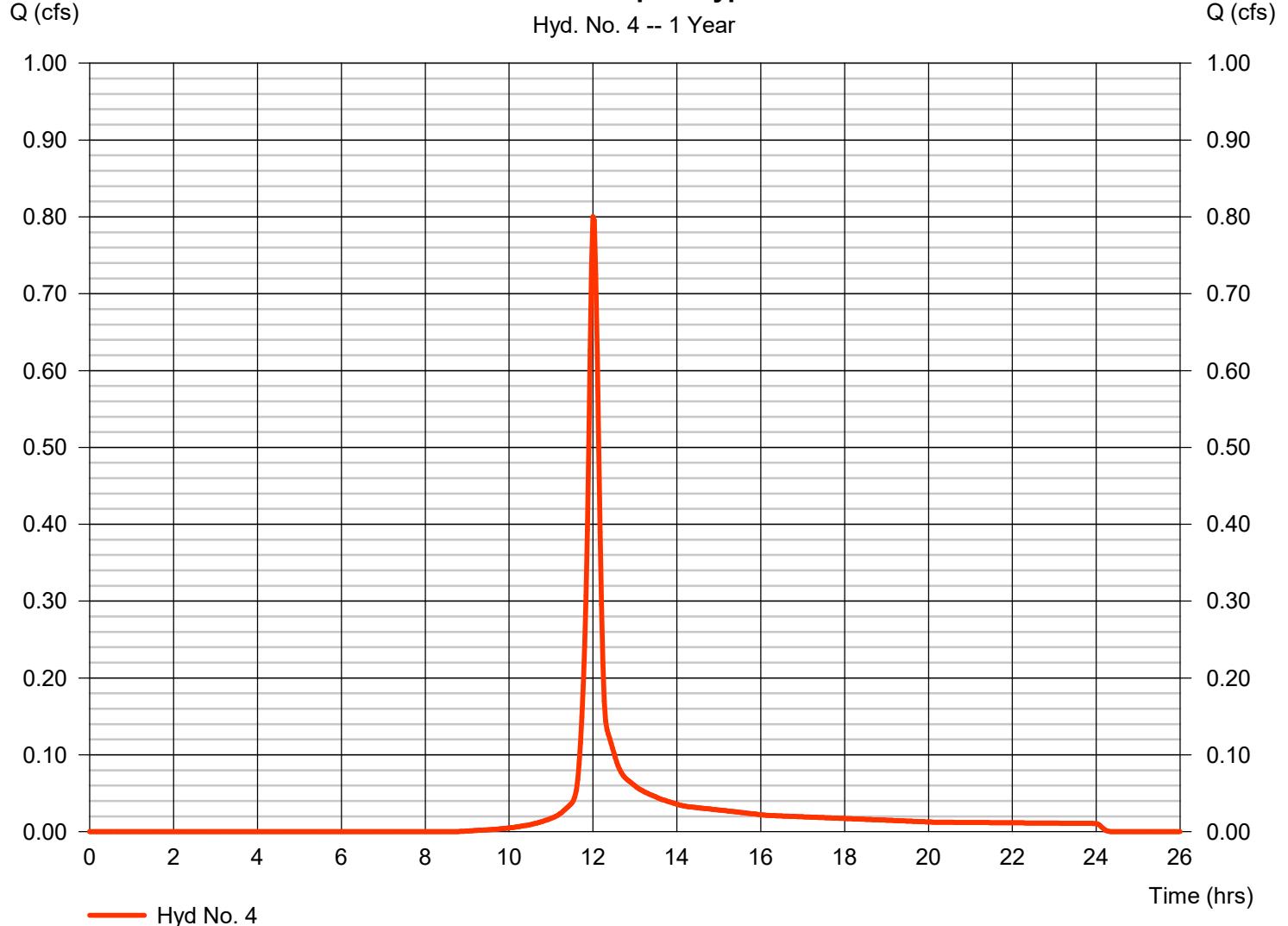
## Hyd. No. 4

### Post Developed Bypass

Hydrograph type	= SCS Runoff	Peak discharge	= 0.800 cfs
Storm frequency	= 1 yrs	Time to peak	= 12.00 hrs
Time interval	= 2 min	Hyd. volume	= 2,079 cuft
Drainage area	= 0.400 ac	Curve number	= 83.8
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.00 min
Total precip.	= 2.86 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

**Post Developed Bypass**

Hyd. No. 4 -- 1 Year



# Hydrograph Report

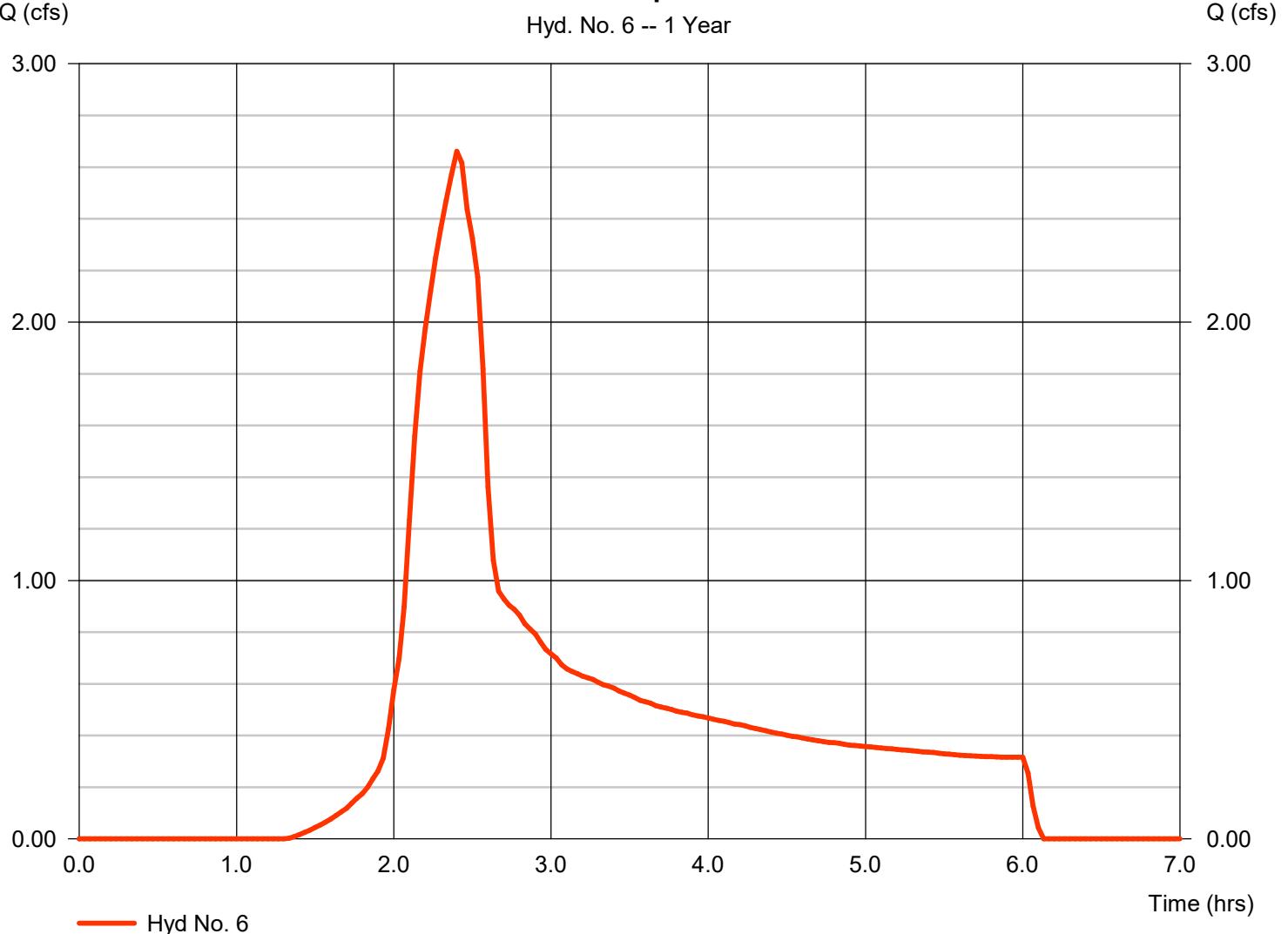
## Hyd. No. 6

### 1.0 Post-Developed to Pond

Hydrograph type	= SCS Runoff	Peak discharge	= 2.661 cfs
Storm frequency	= 1 yrs	Time to peak	= 2.40 hrs
Time interval	= 2 min	Hyd. volume	= 10,560 cuft
Drainage area	= 5.570 ac	Curve number	= 94.9
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 1.00 in	Distribution	= SCS 6-Hr
Storm duration	= 6.00 hrs	Shape factor	= 484

### 1.0 Post-Developed to Pond

Hyd. No. 6 -- 1 Year



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Wednesday, 02 / 8 / 2023

## Hyd. No. 7

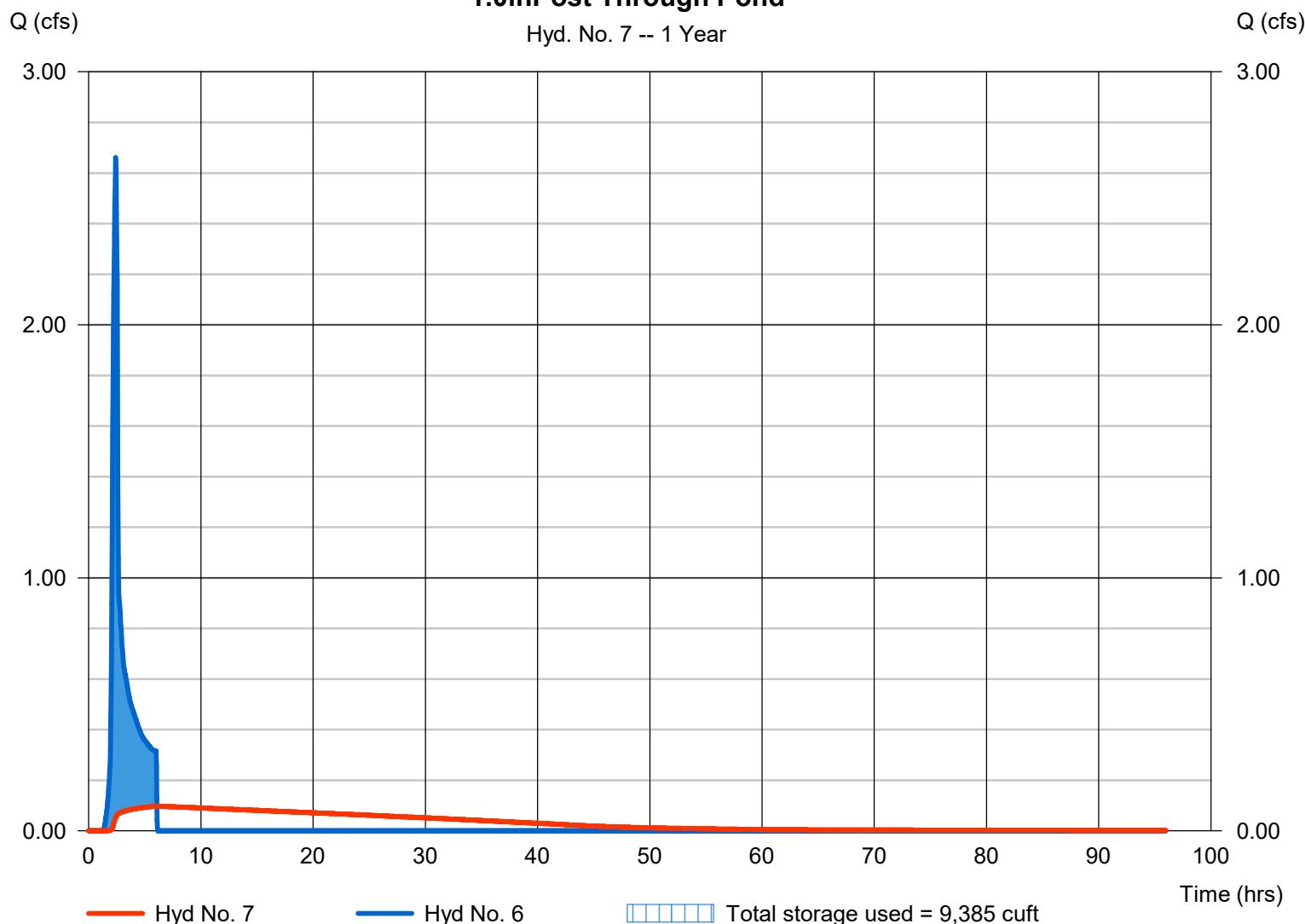
### 1.0inPost Through Pond

Hydrograph type	= Reservoir	Peak discharge	= 0.098 cfs
Storm frequency	= 1 yrs	Time to peak	= 6.07 hrs
Time interval	= 2 min	Hyd. volume	= 10,415 cuft
Inflow hyd. No.	= 6 - 1.0 Post-Developed to Pond	Max. Elevation	= 280.99 ft
Reservoir name	= Wet Pond	Max. Storage	= 9,385 cuft

Storage Indication method used.

### 1.0inPost Through Pond

Hyd. No. 7 -- 1 Year



# Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	15.39	2	722	43,464	----	----	----	Pre-Developed-Overall Site
2	SCS Runoff	38.04	2	716	86,377	----	----	----	Post Developed to Pond
3	Reservoir	12.59	2	724	85,613	2	283.81	44,734	Post Through Pond
4	SCS Runoff	1.936	2	720	5,074	----	----	----	Post Developed Bypass
6	SCS Runoff	0.000	2	n/a	0	----	----	----	1.0 Post-Developed to Pond
7	Reservoir	0.000	2	n/a	0	6	280.00	0.000	1.0inPost Through Pond
Wet Pond1-Zebulon.gpw				Return Period: 10 Year			Wednesday, 02 / 8 / 2023		

# Hydrograph Report

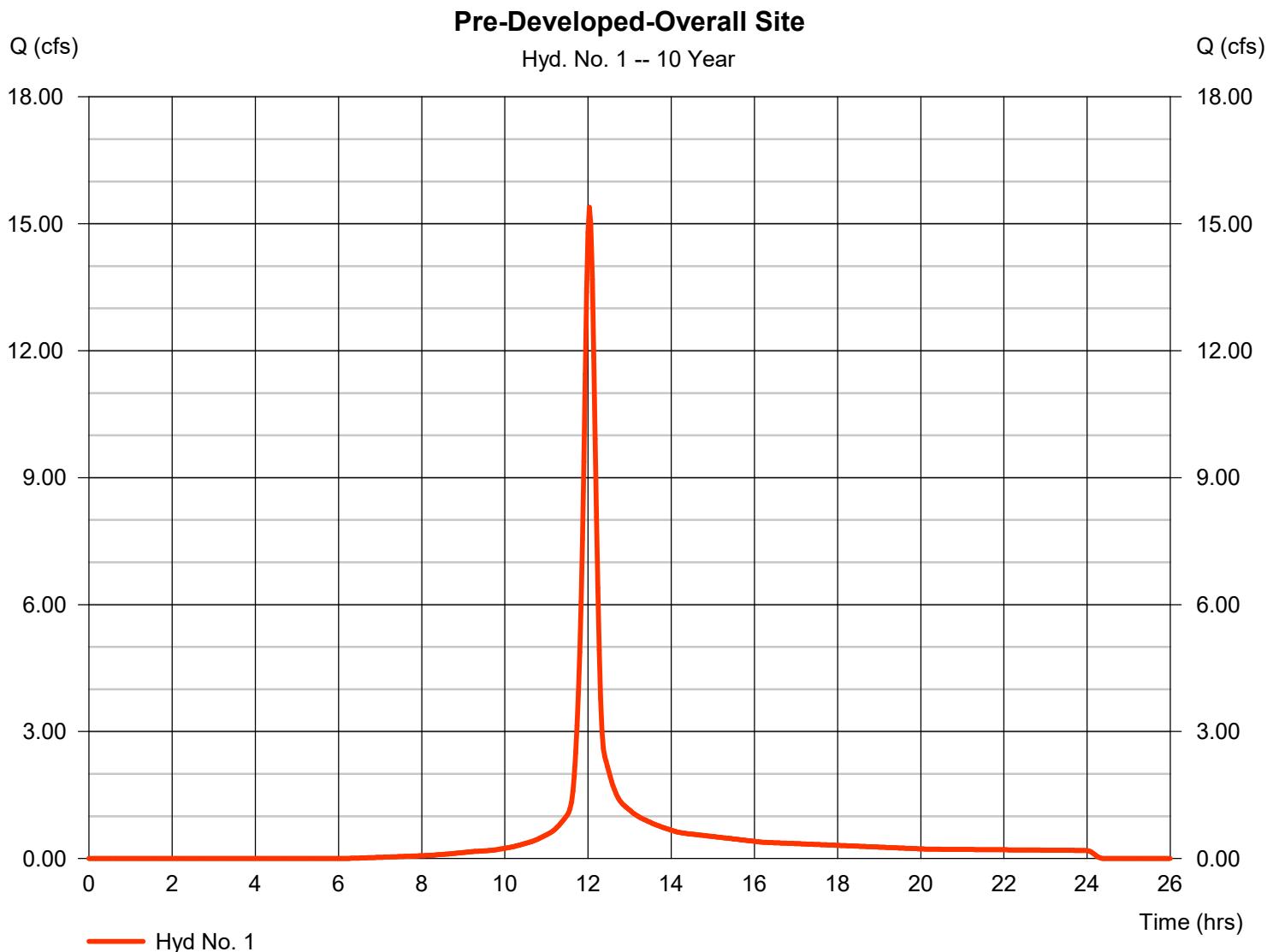
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Wednesday, 02 / 8 / 2023

## Hyd. No. 1

### Pre-Developed-Overall Site

Hydrograph type	= SCS Runoff	Peak discharge	= 15.39 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.03 hrs
Time interval	= 2 min	Hyd. volume	= 43,464 cuft
Drainage area	= 3.710 ac	Curve number	= 83
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 14.00 min
Total precip.	= 5.15 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

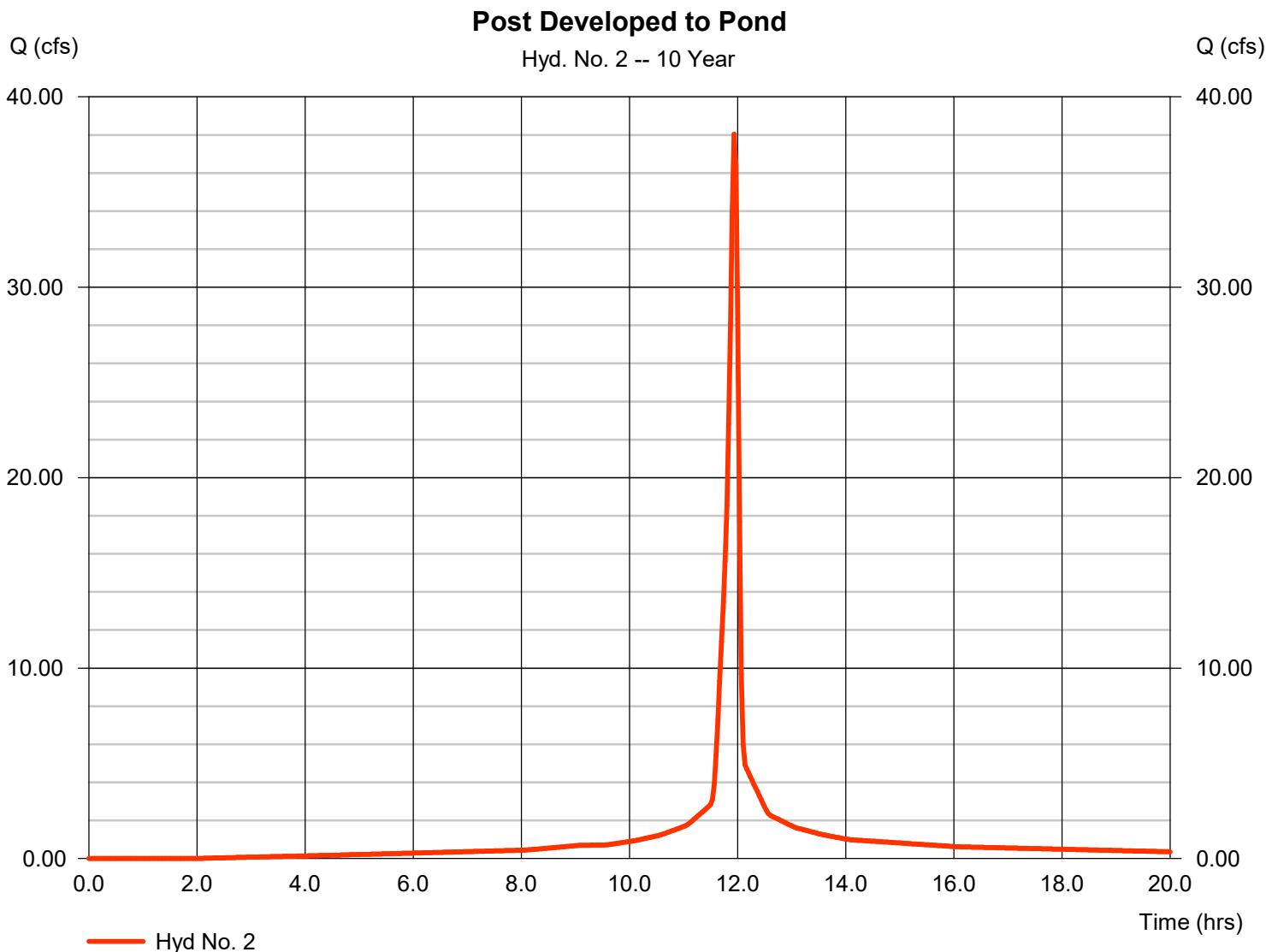


# Hydrograph Report

## Hyd. No. 2

Post Developed to Pond

Hydrograph type	= SCS Runoff	Peak discharge	= 38.04 cfs
Storm frequency	= 10 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 86,377 cuft
Drainage area	= 5.570 ac	Curve number	= 94.9
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.15 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

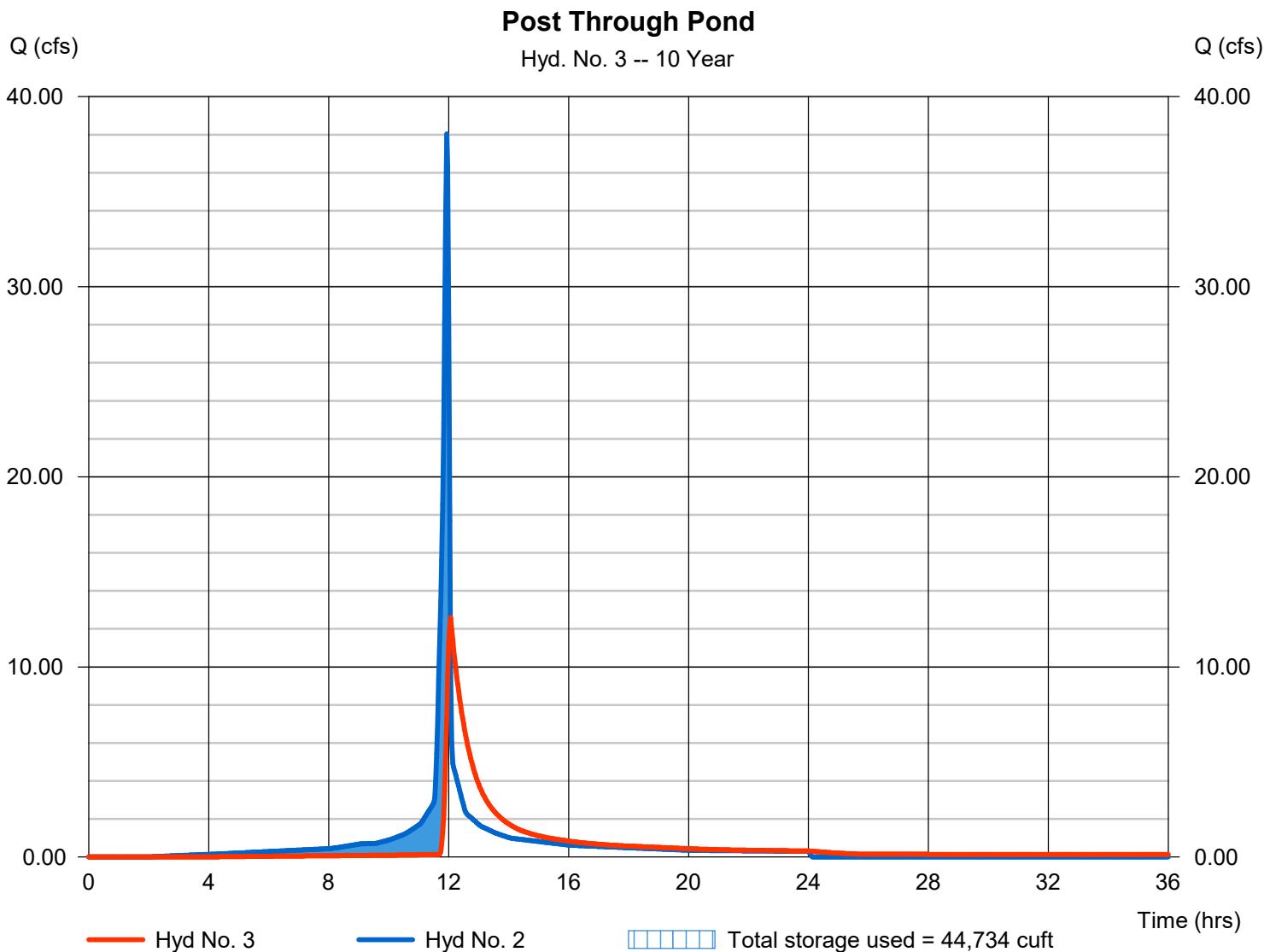
Wednesday, 02 / 8 / 2023

## Hyd. No. 3

Post Through Pond

Hydrograph type	= Reservoir	Peak discharge	= 12.59 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 85,613 cuft
Inflow hyd. No.	= 2 - Post Developed to Pond	Max. Elevation	= 283.81 ft
Reservoir name	= Wet Pond	Max. Storage	= 44,734 cuft

Storage Indication method used.



# Hydrograph Report

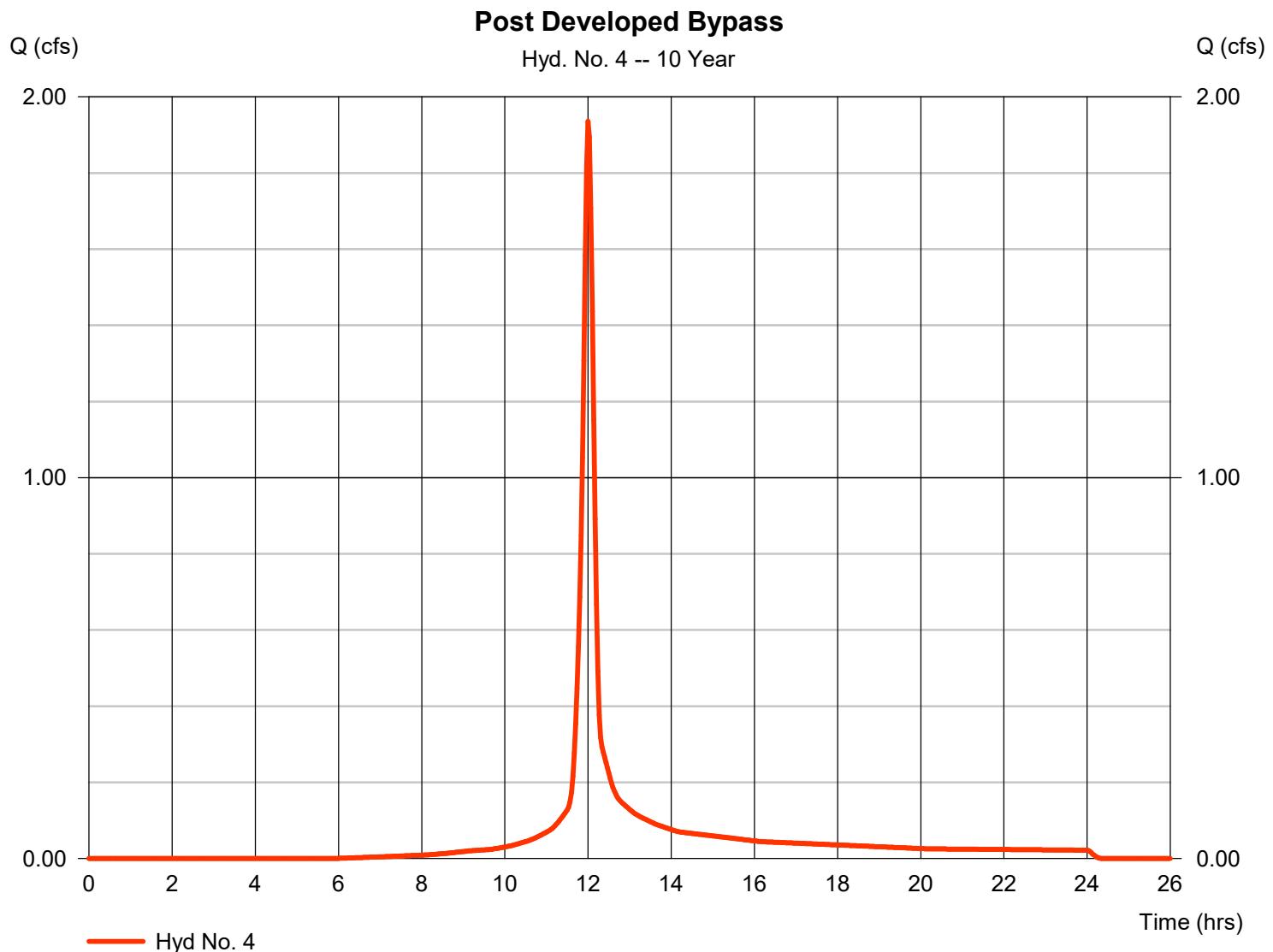
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Wednesday, 02 / 8 / 2023

## Hyd. No. 4

### Post Developed Bypass

Hydrograph type	= SCS Runoff	Peak discharge	= 1.936 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.00 hrs
Time interval	= 2 min	Hyd. volume	= 5,074 cuft
Drainage area	= 0.400 ac	Curve number	= 83.8
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.00 min
Total precip.	= 5.15 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

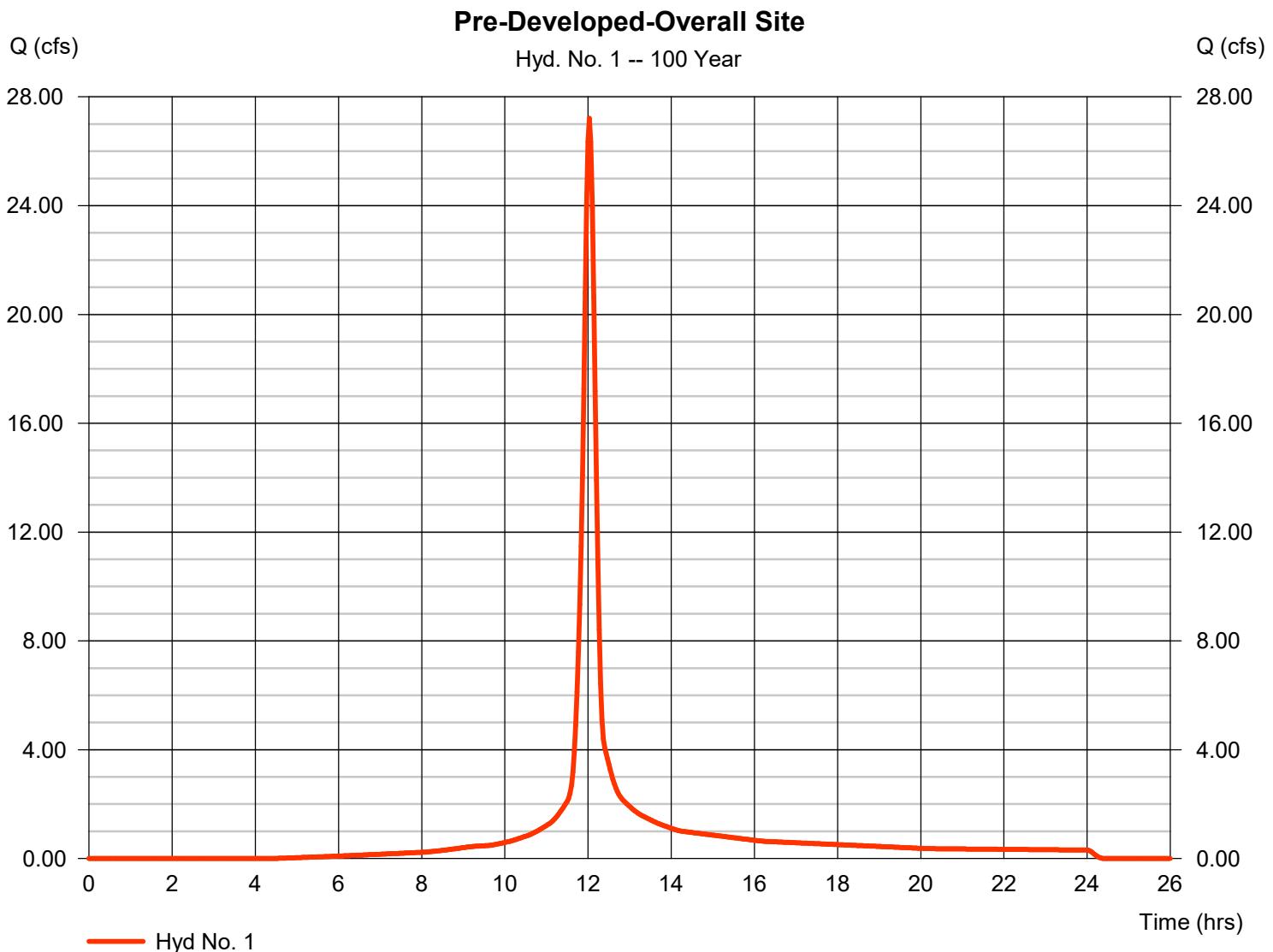
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	27.21	2	722	78,612	----	----	----	Pre-Developed-Overall Site
2	SCS Runoff	60.14	2	716	140,257	----	----	----	Post Developed to Pond
3	Reservoir	43.50	2	720	139,470	2	284.52	55,383	Post Through Pond
4	SCS Runoff	3.389	2	720	9,106	----	----	----	Post Developed Bypass
6	SCS Runoff	0.000	2	n/a	0	----	----	----	1.0 Post-Developed to Pond
7	Reservoir	0.000	2	n/a	0	6	280.00	0.000	1.0inPost Through Pond
Wet Pond1-Zebulon.gpw				Return Period: 100 Year				Wednesday, 02 / 8 / 2023	

# Hydrograph Report

## Hyd. No. 1

### Pre-Developed-Overall Site

Hydrograph type	= SCS Runoff	Peak discharge	= 27.21 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.03 hrs
Time interval	= 2 min	Hyd. volume	= 78,612 cuft
Drainage area	= 3.710 ac	Curve number	= 83
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 14.00 min
Total precip.	= 8.01 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Wednesday, 02 / 8 / 2023

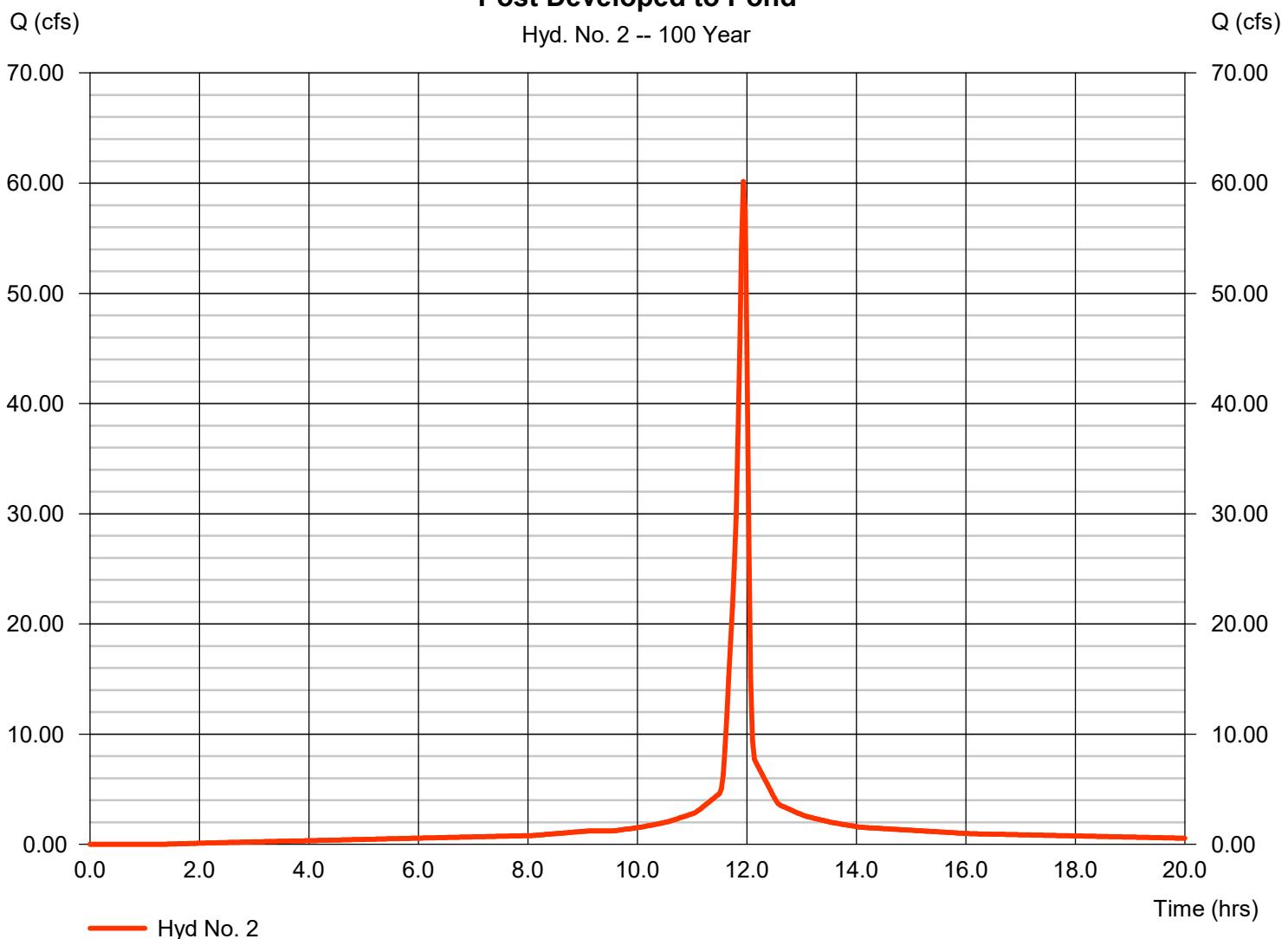
## Hyd. No. 2

Post Developed to Pond

Hydrograph type	= SCS Runoff	Peak discharge	= 60.14 cfs
Storm frequency	= 100 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 140,257 cuft
Drainage area	= 5.570 ac	Curve number	= 94.9
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 8.01 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

**Post Developed to Pond**

Hyd. No. 2 -- 100 Year



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

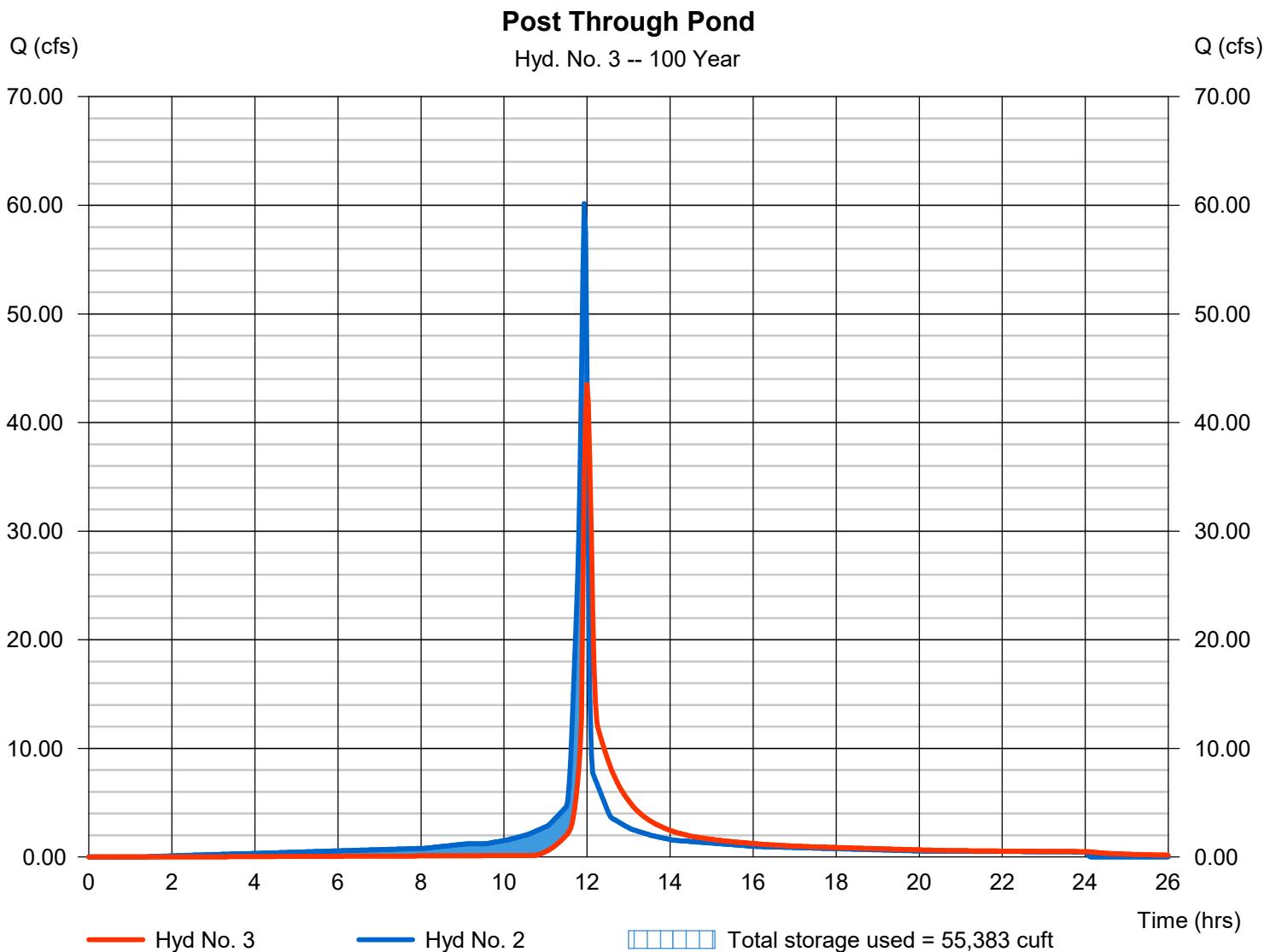
Wednesday, 02 / 8 / 2023

## Hyd. No. 3

Post Through Pond

Hydrograph type	= Reservoir	Peak discharge	= 43.50 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.00 hrs
Time interval	= 2 min	Hyd. volume	= 139,470 cuft
Inflow hyd. No.	= 2 - Post Developed to Pond	Max. Elevation	= 284.52 ft
Reservoir name	= Wet Pond	Max. Storage	= 55,383 cuft

Storage Indication method used.



# Hydrograph Report

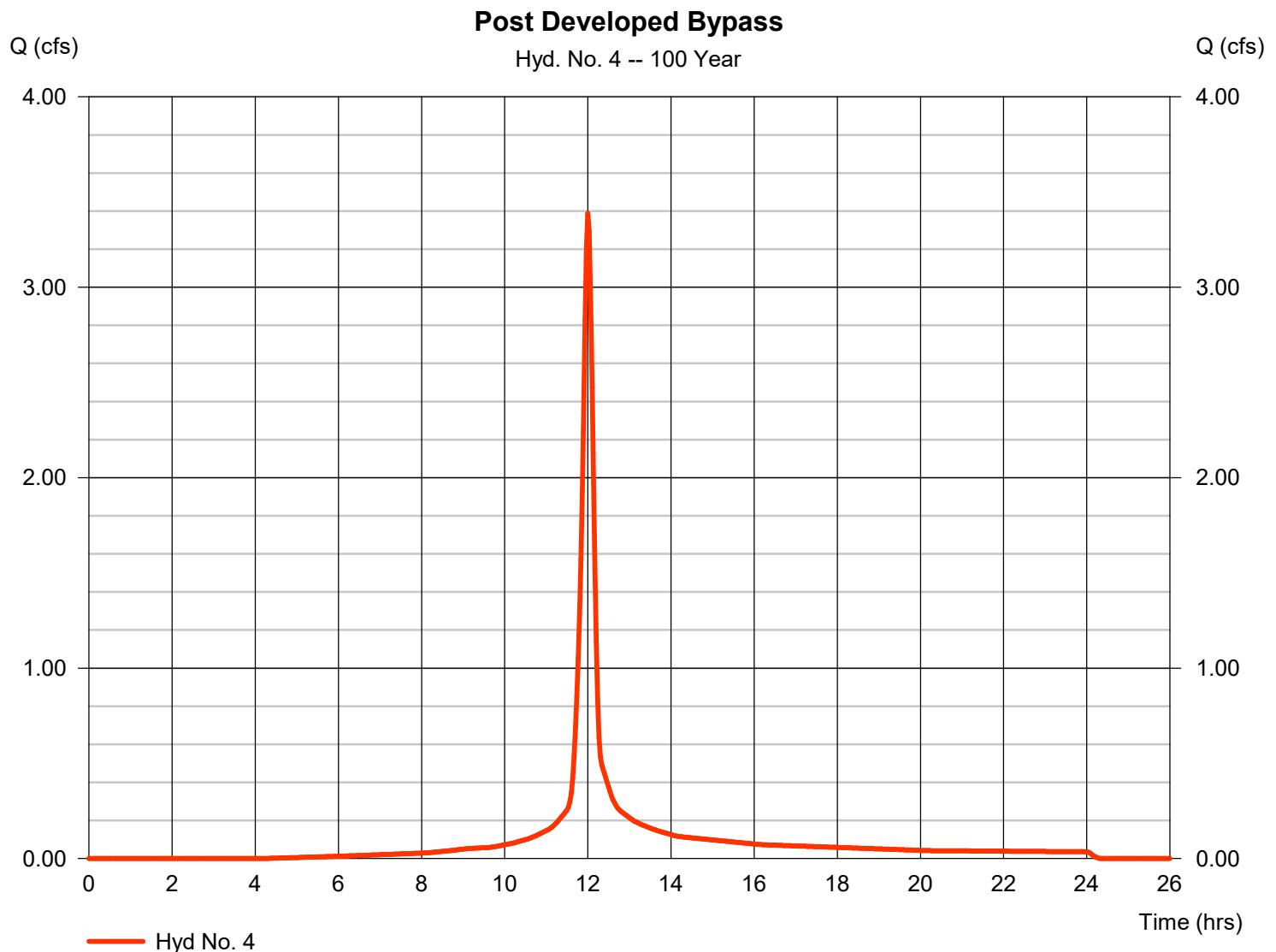
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Wednesday, 02 / 8 / 2023

## Hyd. No. 4

### Post Developed Bypass

Hydrograph type	= SCS Runoff	Peak discharge	= 3.389 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.00 hrs
Time interval	= 2 min	Hyd. volume	= 9,106 cuft
Drainage area	= 0.400 ac	Curve number	= 83.8
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.00 min
Total precip.	= 8.01 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

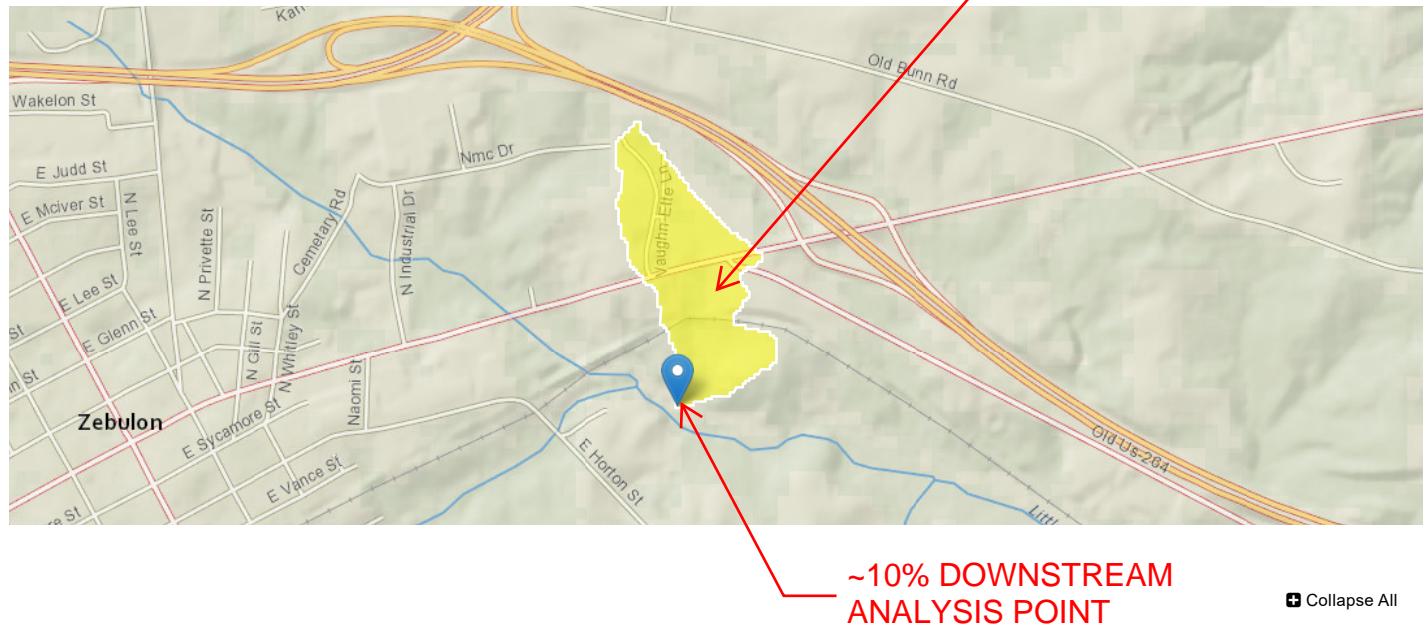


TIME OF CONCENTRATION																														
Existing Conditions																														
SCS Methodology																														
<b>SHEET FLOW:</b>																														
$T_c = (0.007(nL)^{0.8}/(P2^{0.5})(s^{0.4})$ 2-year/24-hr Rainfall Depth TP-40 (in) $n^*$ $T_{c1}$ (min)						<b>SHALLOW CONC FLOW:</b> SEGMENT 1						<b>OPEN CHANNEL</b> <b>FLOW:</b> SEGMENT 1 Manning's Equation: $V = 1.49R^{2/3}S^{1/2} / n$						<b>TOTAL</b>												
Basin	Comments	Length	Elev1	Elev2	Slope	TP-40 (in)	Manning's	$T_{c1}$	Length	Elev2	Elev3	Slope	Condition	Vavg	$T_{c2}$	Cross Sectional Flow Area (ft <sup>2</sup> )	Wetted Perimeter	Hydraulic Radius	Length	Elev3	Elev4	Slope	Manning's	V	$T_{c3}$	$T_{cTOTAL}$	$T_c(\text{minimum})$	Tlag	Basin	
1	Stream	100	292.5	290.0	0.025	3.46	0.24	12.55	286.5	290.0	278.2	0.04119	Unpaved	3.20	1.49											14.04	14.04	0.14	1	
2	Stream	100	290.7	289.5	0.012	3.46	0.24	16.83	389	289.5	283.2	0.01620	Unpaved	2.10	3.09												19.92	19.92	0.20	2

## DOWNSTREAM IMPACT ANALYSIS

## StreamStats Report

**Region ID:** NC  
**Workspace ID:** NC2023011124350202000  
**Clicked Point (Latitude, Longitude):** 35.82526, -78.29649  
**Time:** 2023-01-11 07:44:10 -0500



### Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
DRNAREA	Area that drains to a point on a stream	0.0784	square miles
LC06IMP	Percentage of impervious area determined from NLCD 2006 impervious dataset	8.42	percent
PCTREG1	Percentage of drainage area located in Region 1 - Piedmont / Ridge and Valley	100	percent
PCTREG2	Percentage of drainage area located in Region 2 - Blue Ridge	0	percent
PCTREG3	Percentage of drainage area located in Region 3 - Sandhills	0	percent
PCTREG4	Percentage of drainage area located in Region 4 - Coastal Plains	0	percent
PCTREG5	Percentage of drainage area located in Region 5 - Lower Tifton Uplands	0	percent

### Peak-Flow Statistics

Peak-Flow Statistics Parameters [Region 1 Piedmont rural under 1 sqmi 2014 5030]

50.176 AC

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	0.0784	square miles	0.1	1
LC06IMP	Percent Impervious NLCD2006	8.42	percent	0	47.9

Peak-Flow Statistics Disclaimers [Region 1 Piedmont rural under 1 sqmi 2014 5030]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

Peak-Flow Statistics Flow Report [Region 1 Piedmont rural under 1 sqmi 2014 5030]

Statistic	Value	Unit
50-percent AEP flood	34.7	ft^3/s
20-percent AEP flood	52.6	ft^3/s
10-percent AEP flood	64.8	ft^3/s

Statistic	Value	Unit
4-percent AEP flood	79.8	ft^3/s
2-percent AEP flood	90.8	ft^3/s
1-percent AEP flood	102	ft^3/s
0.5-percent AEP flood	113	ft^3/s
0.2-percent AEP flood	131	ft^3/s

*Peak-Flow Statistics Citations*

**Feaster, T.D., Gotvald, A.J., and Weaver, J.C., 2014, Methods for estimating the magnitude and frequency of floods for urban and small, rural streams in Georgia, South Carolina, and North Carolina, 2011 (ver. 1.1, March 2014): U.S. Geological Survey Scientific Investigations Report 2014-5030, 104 p. (<http://pubs.usgs.gov/sir/2014/5030/>)**

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Application Version: 4.11.1

StreamStats Services Version: 1.2.22

NSS Services Version: 2.2.1



0 400 800 1600 ft  
1 inch equals 800 feet

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## STORM DRAINAGE SYSTEM

Bowman North Carolina, Ltd.  
Tractor Supply Co, Zebulon, NC

Rational Runoff Coefficient "C"

Catch Basin#100

Drainage Area (acres): 0.91

Proposed Land Uses:

<u>Land Use Description</u>	<u>Acres</u>	<u>% Site</u>	<u>Runoff "C"</u>	<u>"C"</u>
Roofs	0.00	0%	0.95	0.00
Asphalt/Concrete Pavement	0.54	60%	0.95	0.57
Lawn	0.36	40%	0.3	0.12
Wooded	0.00	0%	0.2	0.00
Total Area=	0.91		Cumulative "C" =	0.69
			i10=	7.22
			Q10=	4.51

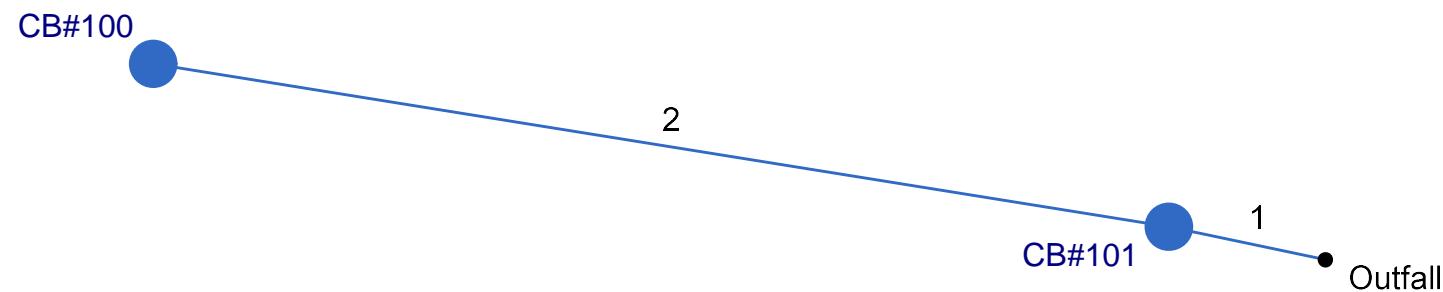
Catch Basin#101

Drainage Area (acres): 0.26

Proposed Land Uses:

<u>Land Use Description</u>	<u>Acres</u>	<u>% Site</u>	<u>Runoff "C"</u>	<u>"C"</u>
Roofs	0.00	0%	0.95	0.00
Asphalt/Concrete Pavement	0.18	68%	0.95	0.64
Lawn	0.09	32%	0.3	0.10
Wooded	0.00	0%	0.2	0.00
Total Area=	0.26		Cumulative "C" =	0.74
			i10=	7.22
			Q10=	1.41

# Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



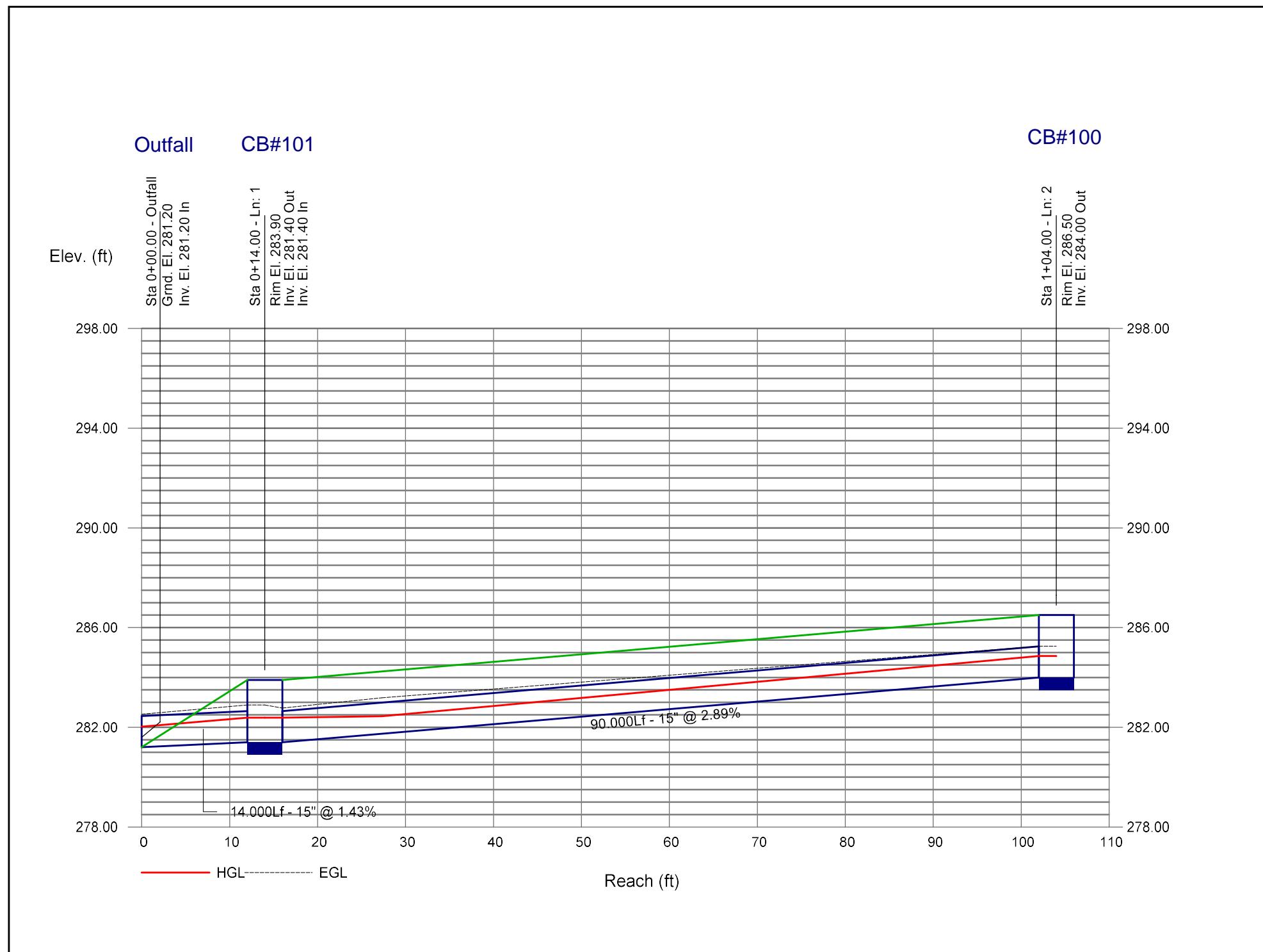
Project File: 100 System.stm

Number of lines: 2

Date: 1/4/2023

# Storm Sewer Profile

Proj. file: 100 System.stm



# Storm Sewer Inventory Report

Page 1

Line No.	Alignment				Flow Data				Physical Data								Line ID
	Dnstr Line No.	Line Length (ft)	Defl angle (deg)	Junc Type	Known Q (cfs)	Drng Area (ac)	Runoff Coeff (C)	Inlet Time (min)	Invert El Dn (ft)	Line Slope (%)	Invert El Up (ft)	Line Size (in)	Line Shape	N Value (n)	J-Loss Coeff (K)	Inlet/Rim El (ft)	
1	End	14.000	-168.063	Curb	1.41	0.00	0.00	0.0	281.20	1.43	281.40	15	Cir	0.013	0.50	283.90	
2	1	90.000	-2.783	Curb	4.51	0.00	0.00	0.0	281.40	2.89	284.00	15	Cir	0.013	1.00	286.50	
Project File: 100 System.stm										Number of lines: 2				Date: 1/4/2023			

# Storm Sewer Summary Report

Line No.	Line ID	Flow rate (cfs)	Line Size (in)	Line shape	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line Slope (%)	HGL Down (ft)	HGL Up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns Line No.	Junction Type
1		5.92	15	Cir	14.000	281.20	281.40	1.428	282.02	282.38	n/a	282.38	End	Curb-Horiz
2		4.51	15	Cir	90.000	281.40	284.00	2.889	282.38	284.86	n/a	284.86 j	1	Curb-Horiz
Project File: 100 System.stm						Number of lines: 2			Run Date: 1/4/2023					
NOTES: Return period = 10 Yrs. ;j - Line contains hyd. jump.														

# Hydraulic Grade Line Computations

Line	Size (in)	Q (cfs)	Downstream							Len (ft)	Upstream							Check		JL coeff	Minor loss (ft)		
			Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)		Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Energy loss (ft)			
1	15	5.92	281.20	282.02	0.82	0.85	6.93	0.51	282.53	0.000	14.000	281.40	282.38	0.98**	1.04	5.72	0.51	282.89	0.000	0.000	n/a	0.50	n/a
2	15	4.51	281.40	282.38	0.98	0.90	4.35	0.39	282.77	0.000	90.000	284.00	284.86 j	0.86**	0.90	5.01	0.39	285.25	0.000	0.000	n/a	1.00	n/a

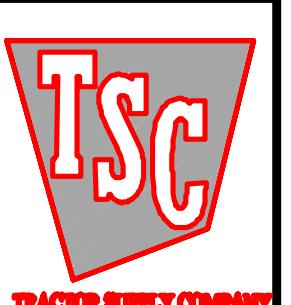
Project File: 100 System.stm

Number of lines: 2

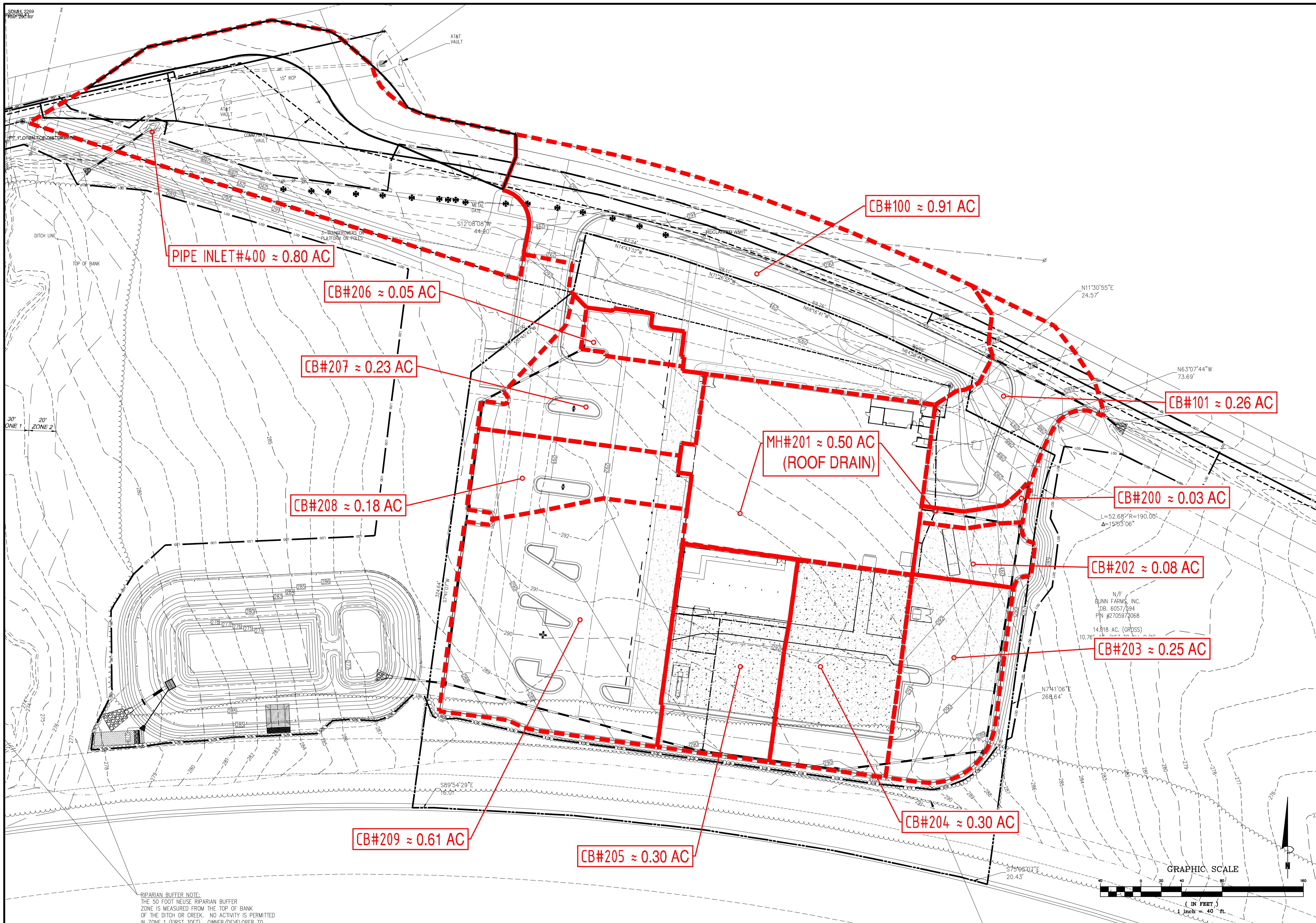
Run Date: 1/4/2023

Notes: ; \*\* Critical depth.; j-Line contains hyd. jump ; c = cir e = ellip b = box

# Bowman



POST DEVELOPED DRAINAGE AREA TO INI ETC



RIPARIAN BUFFER NOTE:  
THE 50 FOOT NEUSE RIPARIAN BUFFER  
ZONE IS MEASURED FROM THE TOP OF BANK  
OF THE DITCH OR CREEK. NO ACTIVITY IS PERMITTED  
IN ZONE 1 (FIRST 30FT) OWNER/DEVELOPER TO

PLAN STATUS		
1/10/23	1ST CD SUBMISSION	
2/10/23	2ND CD SUBMISSION	
DATE	DESCRIPTION	
MEL DESIGN	MEL DRAWN	XXX CHKD
SCALE	H: V:	
JOB No. 220127-01-001		
DATE January 10, 2023		
FILE No. 220127-D-CP-001		
SHEET		

Rational Runoff Coefficient "C"

Catch Basin#200

Drainage Area (acres): 0.03

Proposed Land Uses:

<u>Land Use Description</u>	<u>Acres</u>	<u>% Site</u>	<u>Runoff "C"</u>	<u>"C"</u>
Roofs	0.00	0%	0.95	0.00
Asphalt/Concrete Pavement	0.03	100%	0.95	0.95
Lawn	0.00	0%	0.3	0.00
Wooded	0.00	0%	0.2	0.00
Total Area=	0.03		Cumulative "C" = 0.95 i10= 7.22 Q10= 0.17	

Manhole#201

Drainage Area (acres): 0.50

Proposed Land Uses:

<u>Land Use Description</u>	<u>Acres</u>	<u>% Site</u>	<u>Runoff "C"</u>	<u>"C"</u>
Roofs	0.50	100%	0.95	0.95
Asphalt/Concrete Pavement	0.00	0%	0.95	0.00
Lawn	0.00	0%	0.3	0.00
Wooded	0.00	0%	0.2	0.00
Total Area=	0.50		Cumulative "C" = 0.95 i10= 7.22 Q10= 3.45	

Catch Basin#202

Drainage Area (acres): 0.08

Proposed Land Uses:

<u>Land Use Description</u>	<u>Acres</u>	<u>% Site</u>	<u>Runoff "C"</u>	<u>"C"</u>
Roofs	0.00	0%	0.95	0.00
Asphalt/Concrete Pavement	0.08	100%	0.95	0.95
Lawn	0.00	0%	0.3	0.00
Wooded	0.00	0%	0.2	0.00
Total Area=	0.08		Cumulative "C" = 0.95 i10= 7.22 Q10= 0.55	

Catch Basin#203

Drainage Area (acres): 0.25

Proposed Land Uses:

<u>Land Use Description</u>	<u>Acres</u>	<u>% Site</u>	<u>Runoff "C"</u>	<u>"C"</u>
Roofs	0.00	0%	0.95	0.00
Asphalt/Concrete Pavement	0.24	96%	0.95	0.91
Lawn	0.01	4%	0.3	0.01
Wooded	0.00	0%	0.2	0.00
Total Area=	0.25		Cumulative "C" = 0.92 i10= 7.22 Q10= 1.66	

Catch Basin#204

Drainage Area (acres): 0.30

Proposed Land Uses:

<u>Land Use Description</u>	<u>Acres</u>	<u>% Site</u>	<u>Runoff "C"</u>	<u>"C"</u>
Roofs	0.00	0%	0.95	0.00
Asphalt/Concrete Pavement	0.29	98%	0.95	0.93
Lawn	0.01	2%	0.3	0.01
Wooded	0.00	0%	0.2	0.00
Total Area=	0.30		Cumulative "C" =	0.94
		i10=		7.22
		Q10=		2.02

Catch Basin#205

Drainage Area (acres): 0.30

Proposed Land Uses:

<u>Land Use Description</u>	<u>Acres</u>	<u>% Site</u>	<u>Runoff "C"</u>	<u>"C"</u>
Roofs	0.10	34%	0.95	0.32
Asphalt/Concrete Pavement	0.19	64%	0.95	0.61
Lawn	0.01	2%	0.3	0.01
Wooded	0.00	0%	0.2	0.00
Total Area=	0.30		Cumulative "C" =	0.94
		i10=		7.22
		Q10=		1.99

Catch Basin#206

Drainage Area (acres): 0.05

Proposed Land Uses:

<u>Land Use Description</u>	<u>Acres</u>	<u>% Site</u>	<u>Runoff "C"</u>	<u>"C"</u>
Roofs	0.00	0%	0.95	0.00
Asphalt/Concrete Pavement	0.05	97%	0.95	0.92
Lawn	0.00	3%	0.3	0.01
Wooded	0.00	0%	0.2	0.00
Total Area=	0.05		Cumulative "C" =	0.93
		i10=		7.22
		Q10=		0.36

Catch Basin#207

Drainage Area (acres): 0.23

Proposed Land Uses:

<u>Land Use Description</u>	<u>Acres</u>	<u>% Site</u>	<u>Runoff "C"</u>	<u>"C"</u>
Roofs	0.00	0%	0.95	0.00
Asphalt/Concrete Pavement	0.20	88%	0.95	0.83
Lawn	0.03	12%	0.3	0.04
Wooded	0.00	0%	0.2	0.00
Total Area=	0.23		Cumulative "C" =	0.87
			i10=	7.22
			Q10=	1.42

Catch Basin#208

Drainage Area (acres): 0.18

Proposed Land Uses:

<u>Land Use Description</u>	<u>Acres</u>	<u>% Site</u>	<u>Runoff "C"</u>	<u>"C"</u>
Roofs	0.00	0%	0.95	0.00
Asphalt/Concrete Pavement	0.17	95%	0.95	0.90
Lawn	0.01	5%	0.3	0.02
Wooded	0.00	0%	0.2	0.00
Total Area=	0.18		Cumulative "C" =	0.92
			i10=	7.22
			Q10=	1.16

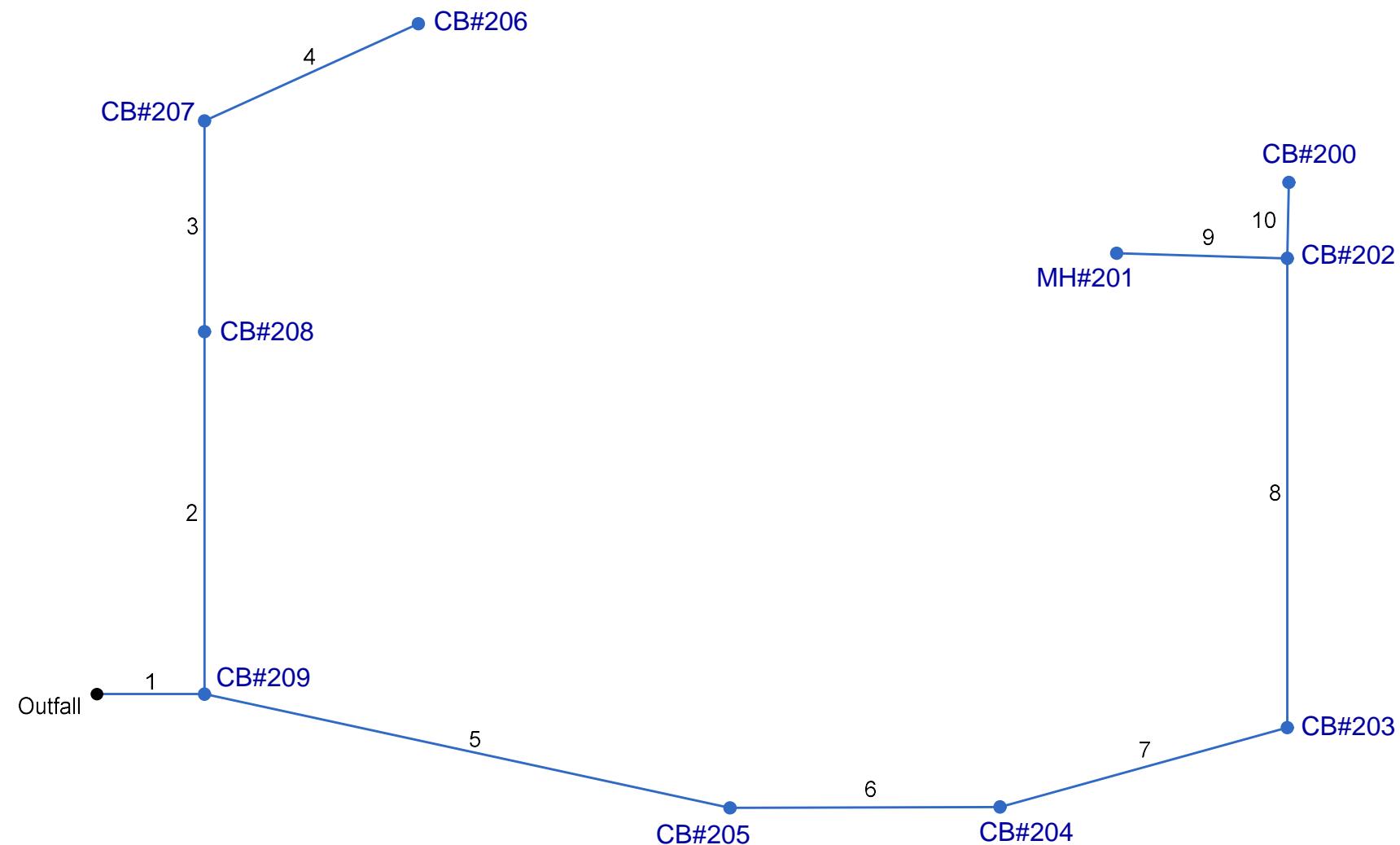
Catch Basin#209

Drainage Area (acres): 0.61

Proposed Land Uses:

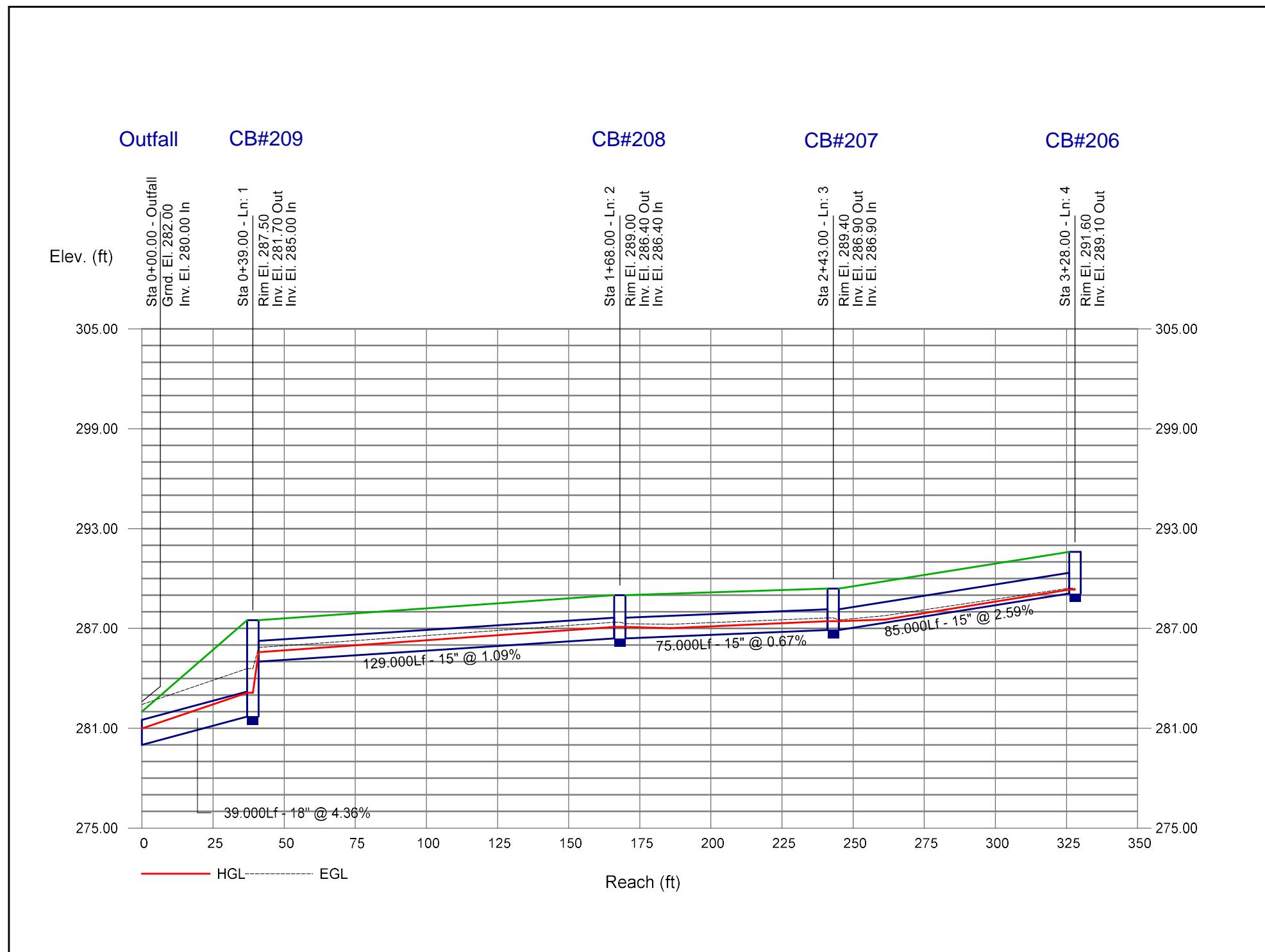
<u>Land Use Description</u>	<u>Acres</u>	<u>% Site</u>	<u>Runoff "C"</u>	<u>"C"</u>
Roofs	0.00	0%	0.95	0.00
Asphalt/Concrete Pavement	0.58	95%	0.95	0.90
Lawn	0.03	5%	0.3	0.02
Wooded	0.00	0%	0.2	0.00
Total Area=	0.61		Cumulative "C" =	0.91
			i10=	7.22
			Q10=	4.03

# Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



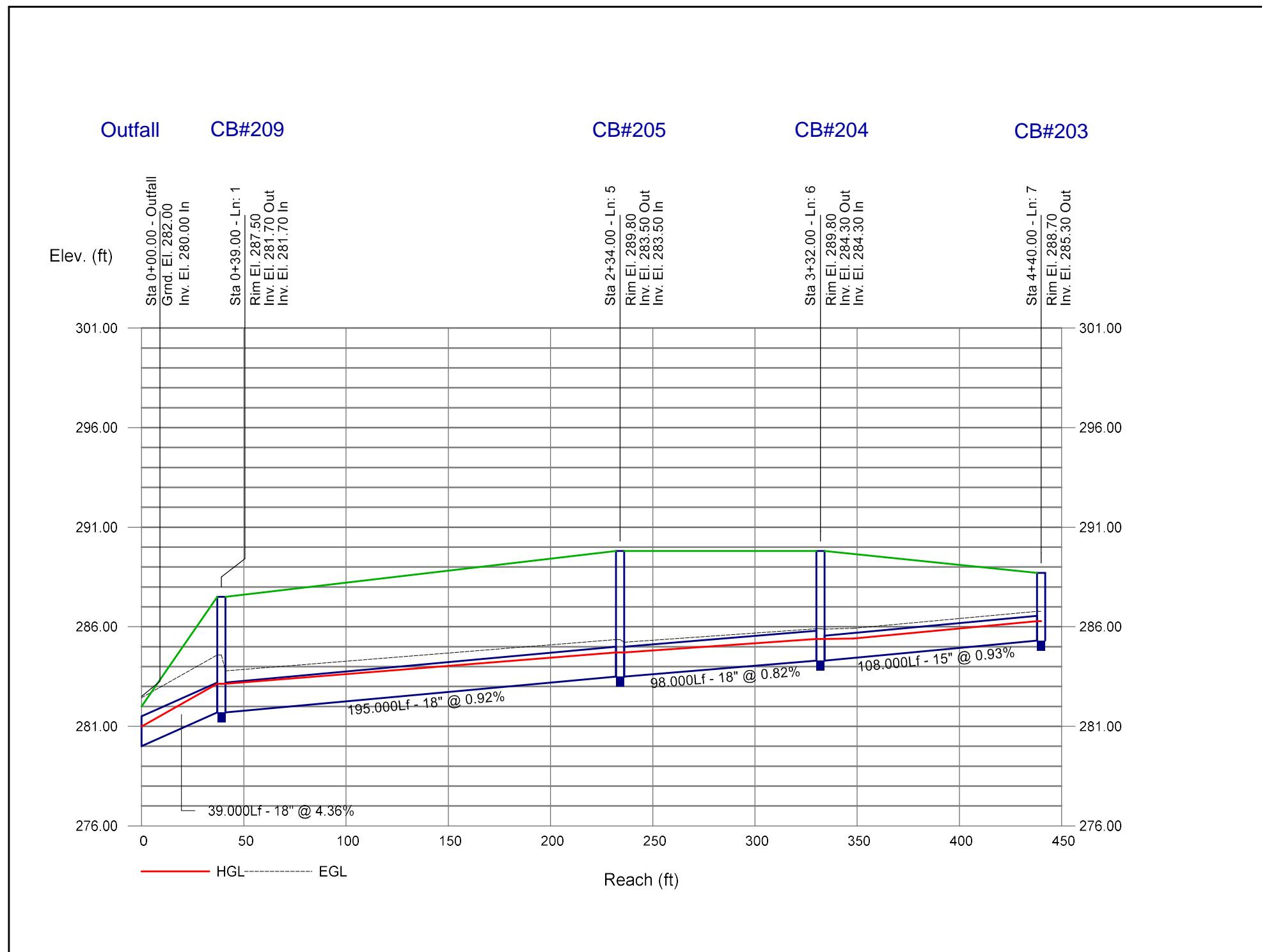
# Storm Sewer Profile

Proj. file: 200 System.stm



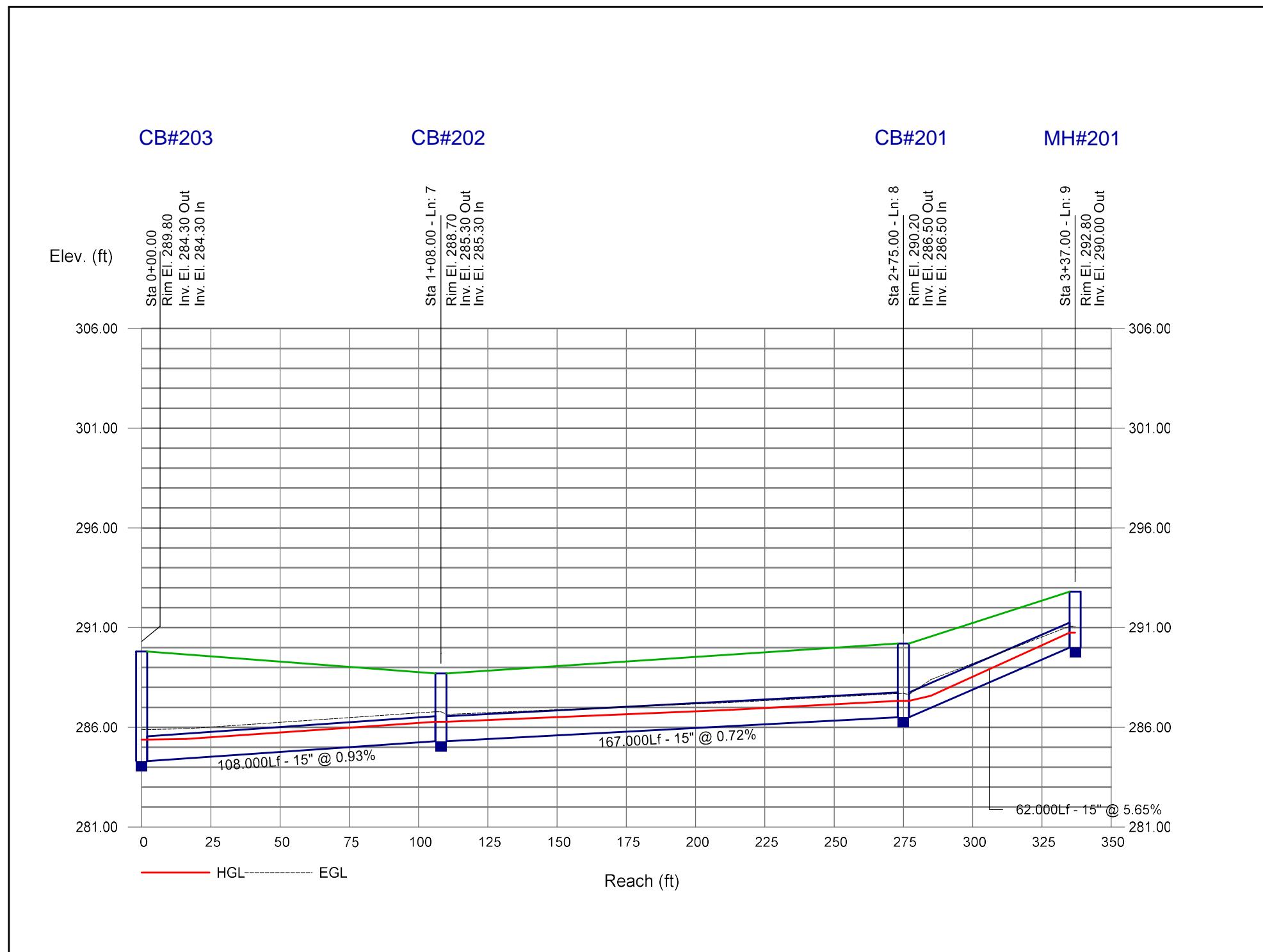
# Storm Sewer Profile

Proj. file: 200 System.stm



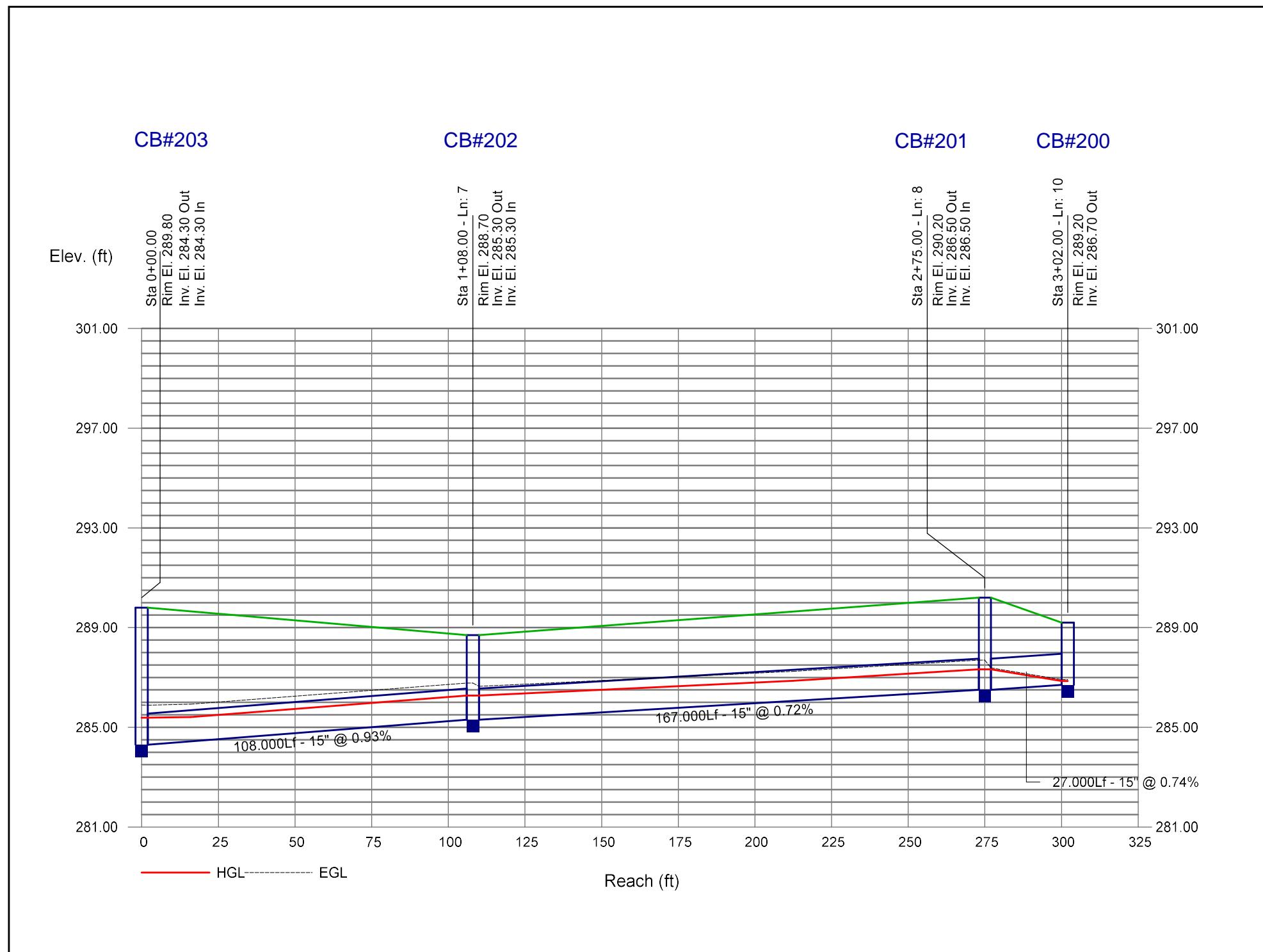
# Storm Sewer Profile

Proj. file: 200 System.stm



# Storm Sewer Profile

Proj. file: 200 System.stm



# Storm Sewer Inventory Report

Page 1

Line No.	Alignment				Flow Data				Physical Data								Line ID
	Dnstr Line No.	Line Length (ft)	Defl angle (deg)	Junc Type	Known Q (cfs)	Drng Area (ac)	Runoff Coeff (C)	Inlet Time (min)	Invert El Dn (ft)	Line Slope (%)	Invert El Up (ft)	Line Size (in)	Line Shape	N Value (n)	J-Loss Coeff (K)	Inlet/Rim El (ft)	
1	End	39.000	0.000	Curb	4.03	0.00	0.00	5.0	280.00	4.36	281.70	18	Cir	0.013	1.89	287.50	
2	1	129.000	-90.000	Curb	1.16	0.00	0.00	5.0	285.00	1.09	286.40	15	Cir	0.013	0.50	289.00	
3	2	75.000	0.000	Curb	1.42	0.00	0.00	5.0	286.40	0.67	286.90	15	Cir	0.013	1.39	289.40	
4	3	85.000	65.995	Curb	0.36	0.00	0.00	5.0	286.90	2.59	289.10	15	Cir	0.013	1.00	291.60	
5	1	195.000	11.990	Curb	1.99	0.00	0.00	5.0	281.70	0.92	283.50	18	Cir	0.013	0.50	289.80	
6	5	98.000	-12.199	Curb	2.02	0.00	0.00	5.0	283.50	0.82	284.30	18	Cir	0.013	0.50	289.80	
7	6	108.000	-14.948	Curb	1.66	0.00	0.00	5.0	284.30	0.93	285.30	15	Cir	0.013	1.46	288.70	
8	7	167.000	-74.829	Curb	0.55	0.00	0.00	5.0	285.30	0.72	286.50	15	Cir	0.013	1.50	290.20	
9	8	62.000	-88.331	MH	3.45	0.00	0.00	0.0	286.50	5.65	290.00	15	Cir	0.013	1.00	292.80	
10	8	27.000	1.183	Curb	0.17	0.00	0.00	0.0	286.50	0.74	286.70	15	Cir	0.013	1.00	289.20	

Project File: 200 System.stm

Number of lines: 10

Date: 1/4/2023

# Storm Sewer Summary Report

Line No.	Line ID	Flow rate (cfs)	Line Size (in)	Line shape	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line Slope (%)	HGL Down (ft)	HGL Up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns Line No.	Junction Type	
1		16.81	18	Cir	39.000	280.00	281.70	4.359	280.98	283.14	2.74	283.14	End	Curb-Horiz	
		2.94	15	Cir	129.000	285.00	286.40	1.085	285.58	287.09	0.14	287.09	1	Curb-Horiz	
		1.78	15	Cir	75.000	286.40	286.90	0.667	287.09	287.43	n/a	287.43 j	2	Curb-Horiz	
		0.36	15	Cir	85.000	286.90	289.10	2.588	287.43	289.33	n/a	289.33 j	3	Curb-Horiz	
		9.84	18	Cir	195.000	281.70	283.50	0.923	283.14	284.71	n/a	284.71	1	Curb-Horiz	
		7.85	18	Cir	98.000	283.50	284.30	0.816	284.71	285.38	0.26	285.38	5	Curb-Horiz	
		5.83	15	Cir	108.000	284.30	285.30	0.926	285.38	286.28	n/a	286.28 j	6	Curb-Horiz	
		4.17	15	Cir	167.000	285.30	286.50	0.719	286.28	287.33	n/a	287.33 j	7	Curb-Horiz	
		3.45	15	Cir	62.000	286.50	290.00	5.645	287.33	290.75	n/a	290.75 j	8	Manhole	
		0.17	15	Cir	27.000	286.50	286.70	0.741	287.33	286.86	n/a	286.86	8	Curb-Horiz	
Project File: 200 System.stm								Number of lines: 10			Run Date: 1/4/2023				
NOTES: Return period = 10 Yrs. ; j - Line contains hyd. jump.															

# Hydraulic Grade Line Computations

Line	Size (in)	Q (cfs)	Downstream							Len (ft)	Upstream							Check		JL coeff	Minor loss (ft)		
			Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)		Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Energy loss (ft)			
1	18	16.81	280.00	280.98	0.98	1.23	13.67	1.45	282.43	0.000	39.000	281.70	283.14	1.44**	1.74	9.65	1.45	284.59	0.000	0.000	n/a	1.89	2.74
2	15	2.94	285.00	285.58	0.58*	0.56	5.29	0.28	285.86	0.000	129.000	286.40	287.09	0.69**	0.69	4.24	0.28	287.37	0.000	0.000	n/a	0.50	0.14
3	15	1.78	286.40	287.09	0.69	0.49	2.57	0.20	287.29	0.000	75.000	286.90	287.43 j	0.53**	0.49	3.60	0.20	287.63	0.000	0.000	n/a	1.39	0.28
4	15	0.36	286.90	287.43	0.53	0.16	0.73	0.08	287.51	0.000	85.000	289.10	289.33 j	0.23**	0.16	2.28	0.08	289.41	0.000	0.000	n/a	1.00	0.08
5	18	9.84	281.70	283.14	1.44	1.53	5.65	0.65	283.78	0.000	195.000	283.50	284.71	1.21**	1.53	6.45	0.65	285.36	0.000	0.000	n/a	0.50	n/a
6	18	7.85	283.50	284.71	1.21	1.37	5.14	0.51	285.22	0.000	98.000	284.30	285.38	1.08**	1.37	5.74	0.51	285.90	0.000	0.000	n/a	0.50	0.26
7	15	5.83	284.30	285.38	1.08	1.03	5.16	0.50	285.88	0.000	108.000	285.30	286.28 j	0.98**	1.03	5.67	0.50	286.78	0.000	0.000	n/a	1.46	n/a
8	15	4.17	285.30	286.28	0.98	0.86	4.05	0.37	286.64	0.000	167.000	286.50	287.33 j	0.83**	0.86	4.85	0.37	287.69	0.000	0.000	n/a	1.50	0.55
9	15	3.45	286.50	287.33	0.83	0.77	4.01	0.31	287.64	0.000	62.000	290.00	290.75 j	0.75**	0.77	4.50	0.31	291.06	0.000	0.000	n/a	1.00	n/a
10	15	0.17	286.50	287.33	0.83	0.09	0.20	0.05	287.38	0.000	27.000	286.70	286.86	0.16**	0.09	1.87	0.05	286.91	0.000	0.000	n/a	1.00	n/a

Project File: 200 System.stm

Number of lines: 10

Run Date: 1/4/2023

Notes: \* Normal depth assumed; \*\* Critical depth.; j-Line contains hyd. jump ; c = cir e = ellip b = box

# Bowman

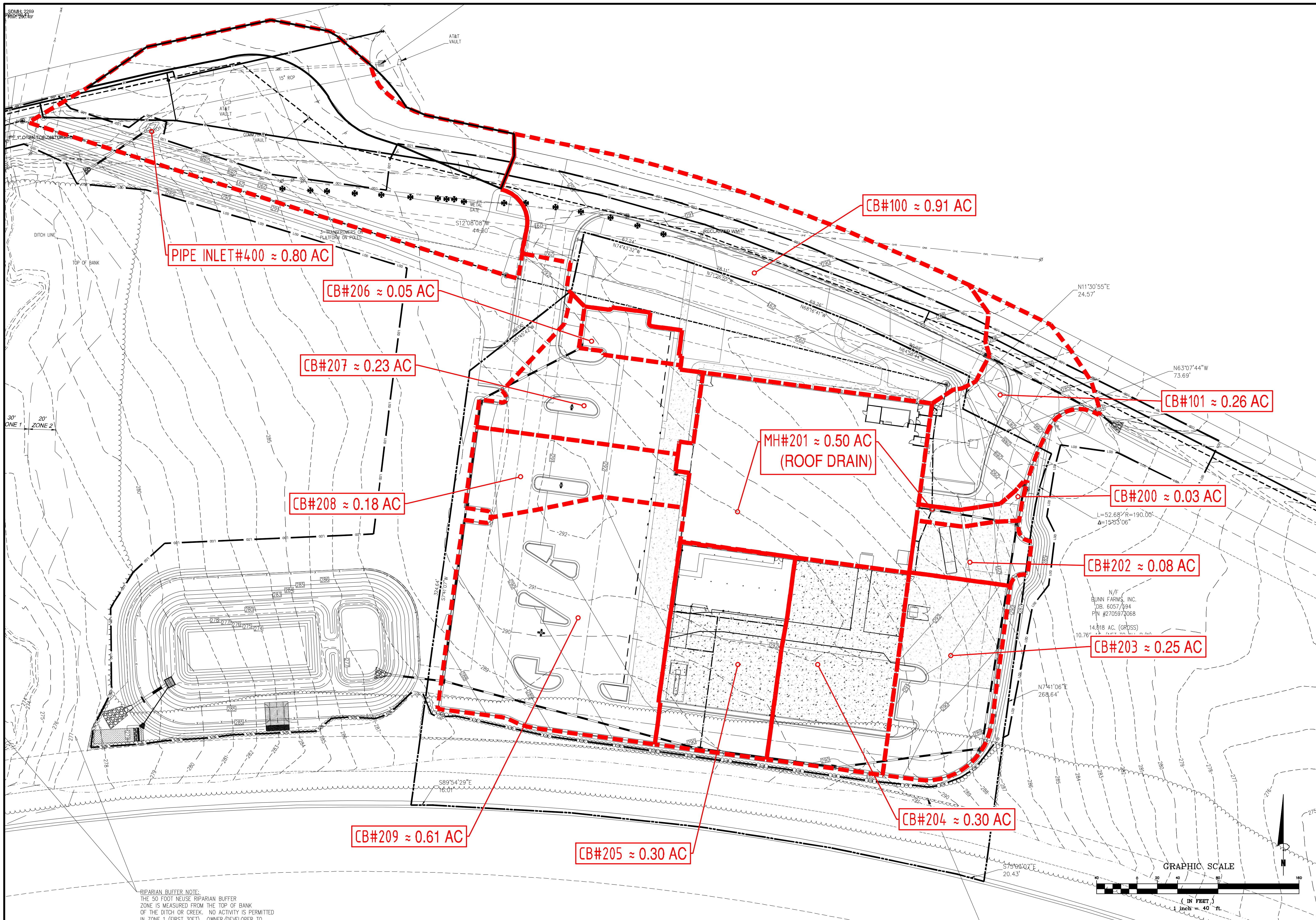


**TSC**  
TRACTOR SUPPLY COMPANY

POS I-DEVELOPED DRAINAGE AREA 10 INLETS

Tractor Supply  
Old US Highway 264  
Zebulon, NC Wake County

POST-DEVEI OPERATED DRAINAGE AREA TO INITIATE



RIPARIAN BUFFER NOTE:  
THE 50 FOOT NEUSE RIPARIAN BUFFER  
ZONE IS MEASURED FROM THE TOP OF BANK  
OF THE DITCH OR CREEK. NO ACTIVITY IS PERMITTED  
IN ZONE 1 (FIRST 30FT) OWNER/DEVELOPER TO

PLAN STATUS		
1/10/23	1ST CD SUBMISSION	
2/10/23	2ND CD SUBMISSION	
DATE	DESCRIPTION	
MEL DESIGN	MEL DRAWN	XXX CHKD
SCALE	H: V:	
JOB No. 220127-01-001		
DATE January 10, 2023		
FILE No. 220127-D-CP-001		
SHEET		

Bowman North Carolina, Ltd.  
Tractor Supply Co, Zebulon, NC

Rational Runoff Coefficient "C"

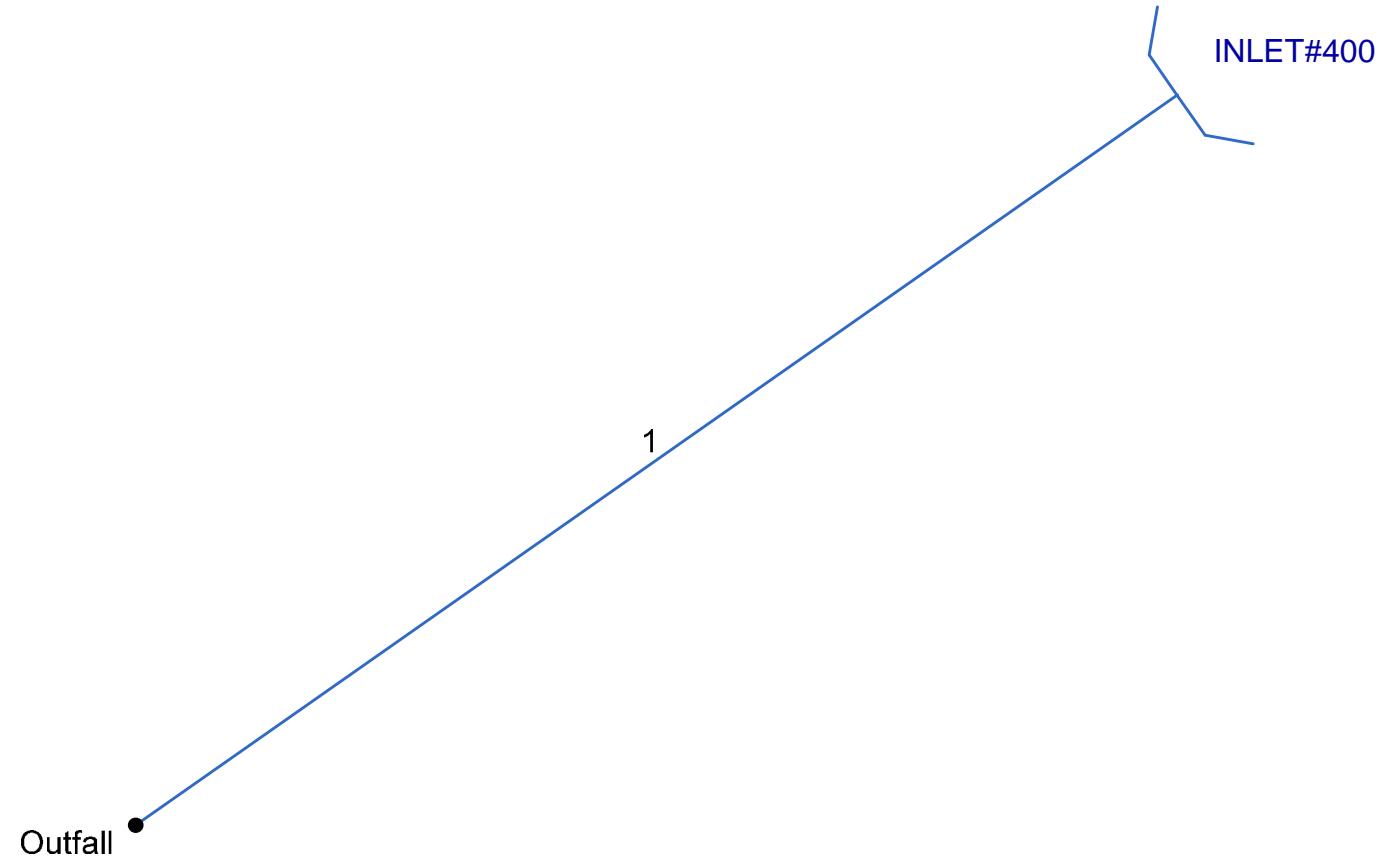
Pipe Inlet#400

Drainage Area (acres): 0.80

Proposed Land Uses:

<u>Land Use Description</u>	<u>Acres</u>	<u>% Site</u>	<u>Runoff "C"</u>	<u>"C"</u>
Roofs	0.00	0%	0.95	0.00
Asphalt/Concrete Pavement	0.22	27%	0.95	0.26
Lawn	0.58	73%	0.3	0.22
Wooded	0.00	0%	0.2	0.00
Total Area=	0.80	Cumulative "C" =	0.48	
		i10=	7.22	
		Q10=	2.76	

# Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



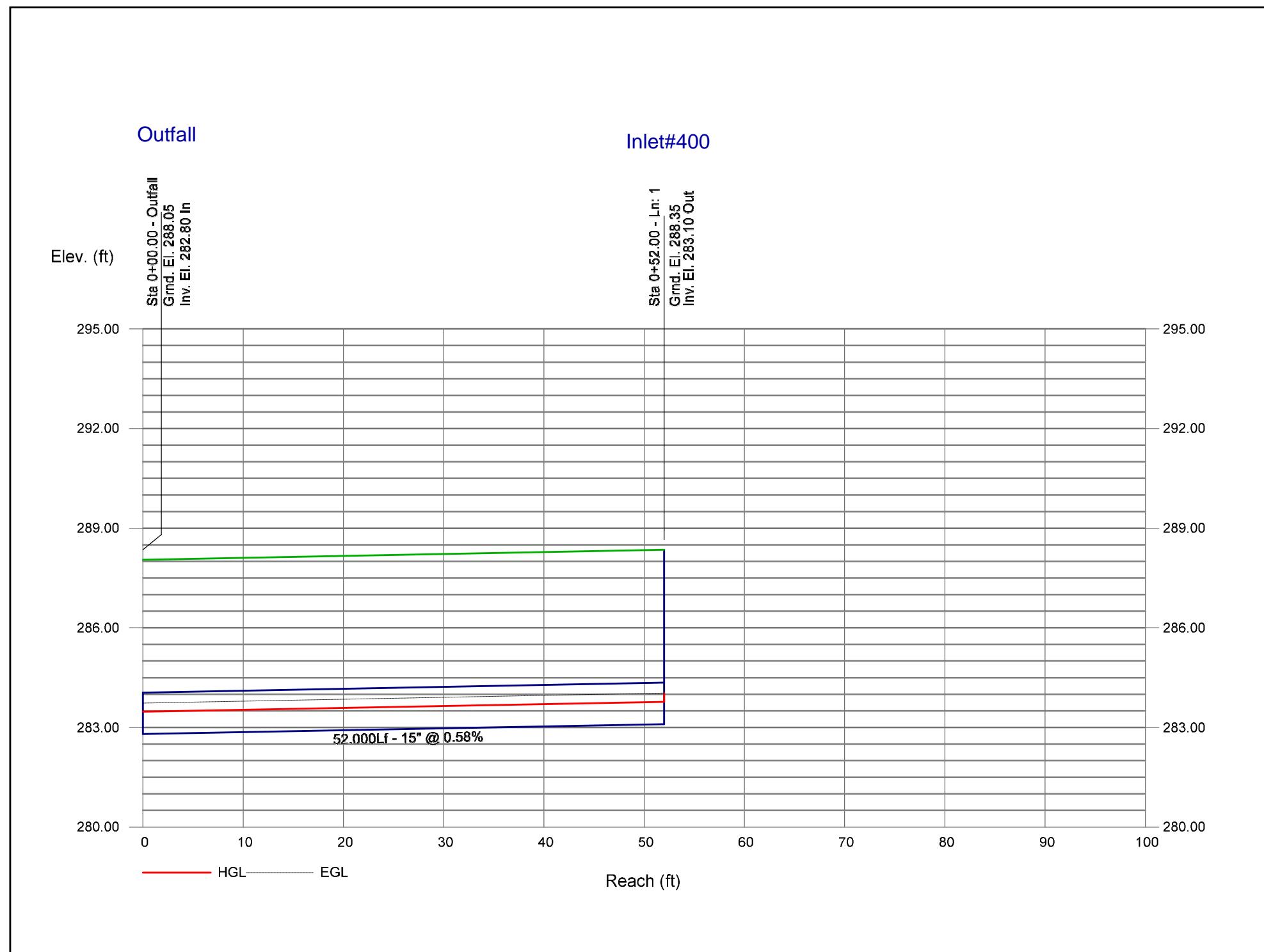
Project File: 400 System.stm

Number of lines: 1

Date: 2/8/2023

# Storm Sewer Profile

Proj. file: 400 System.stm



# Storm Sewer Inventory Report

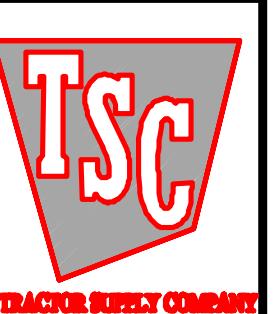
Line No.	Alignment				Flow Data				Physical Data								Line ID
	Dnstr Line No.	Line Length (ft)	Defl angle (deg)	Junc Type	Known Q (cfs)	Drng Area (ac)	Runoff Coeff (C)	Inlet Time (min)	Invert El Dn (ft)	Line Slope (%)	Invert El Up (ft)	Line Size (in)	Line Shape	N Value (n)	J-Loss Coeff (K)	Inlet/Rim El (ft)	
1	End	52.000	-35.000	Hdwl	2.76	0.00	0.00	5.0	282.80	0.58	283.10	15	Cir	0.013	1.00	0.00	
Project File: 400 System.stm												Number of lines: 1				Date: 2/8/2023	

# Storm Sewer Summary Report

Line No.	Line ID	Flow rate (cfs)	Line Size (in)	Line shape	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line Slope (%)	HGL Down (ft)	HGL Up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns Line No.	Junction Type
1		2.76	15	Cir	52.000	282.80	283.10	0.577	283.47	283.77	0.26	284.03	End	OpenHeadwall
Project File: 400 System.stm						Number of lines: 1			Run Date: 2/8/2023					
NOTES: Return period = 10 Yrs.														

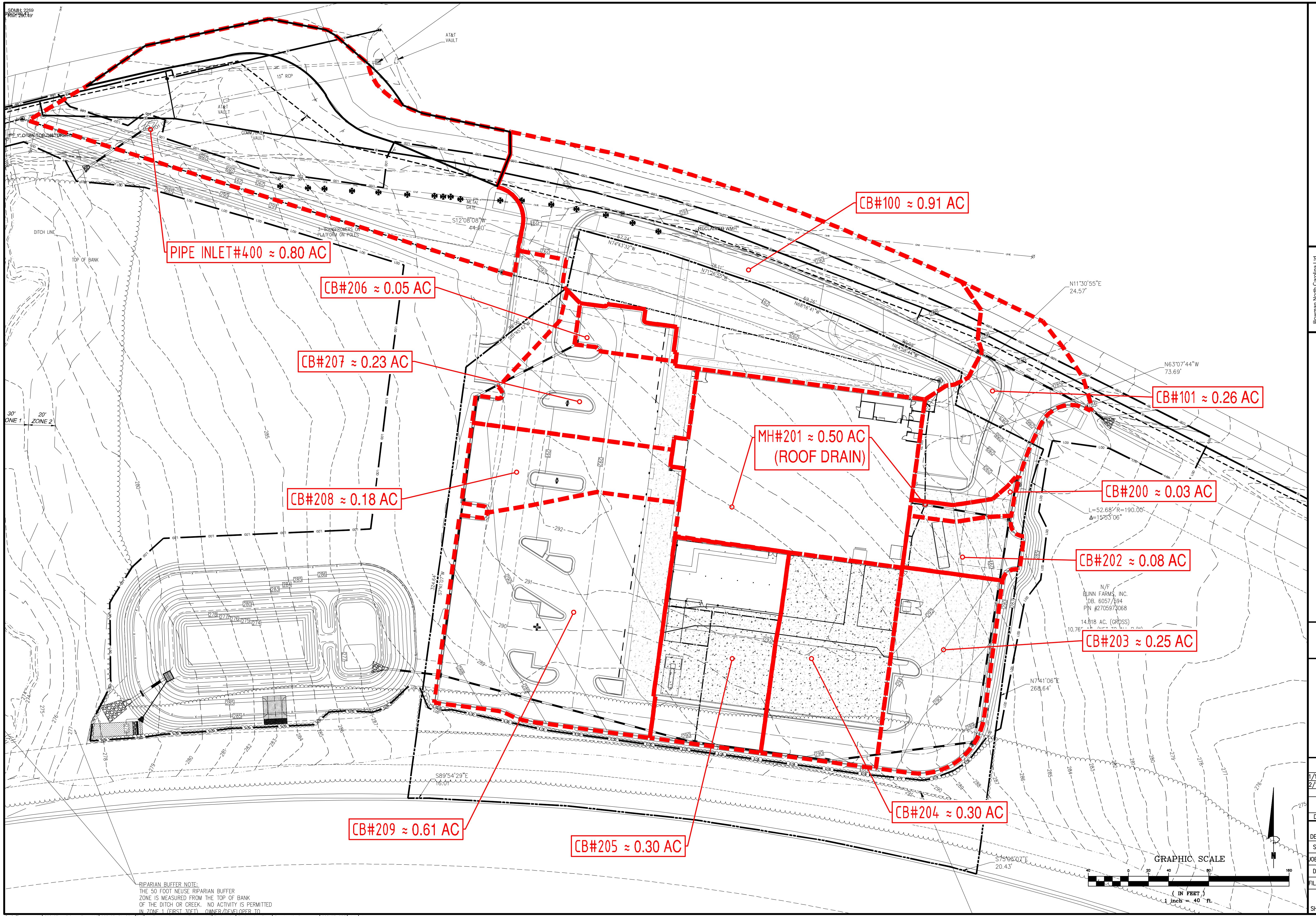
# Hydraulic Grade Line Computations

Line	Size (in)	Q (cfs)	Downstream							Len (ft)	Upstream							Check		JL coeff	Minor loss (ft)		
			Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)		Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Energy loss (ft)			
1	15	2.76	282.80	283.47	0.67	0.67	4.11	0.26	283.73	0.576	52.000	283.10	283.77	0.67**	0.67	4.12	0.26	284.03	0.581	0.579	0.301	1.00	0.26
Project File: 400 System.stm										Number of lines: 1										Run Date: 2/8/2023			
Notes: ; ** Critical depth. ; c = cir e = ellip b = box																							



POST-DEVELOPED DRAINAGE AREA TO INLETS

Tractor Supply  
Old US Highway 264  
Zebulon, NC Wake County



RIPARIAN BUFFER NOTE:  
THE 50 FOOT NEUSE RIPARIAN BUFFER  
ZONE IS MEASURED FROM THE TOP OF BANK  
OF THE DITCH OR CREEK. NO ACTIVITY IS PERMITTED  
IN ZONE 1 (FIRST 30FT). OWNER/DEVELOPER TO

## EROSION CONTROL CALCULATIONS

## EROSION CONTROL CALCS (RIP-RAP CALCULATIONS)

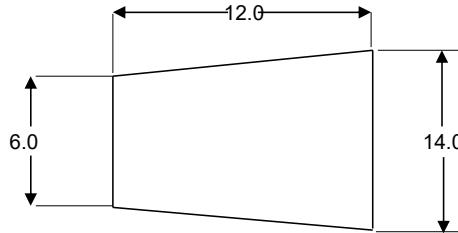
### Project Information

Project Name: Tractor Supply - Zebulon  
Project #: 220127-01  
Designed by: CB Date: 2/7/2023  
Revised by: \_\_\_\_\_ Date: \_\_\_\_\_  
Checked by: \_\_\_\_\_ Date: \_\_\_\_\_

### FES #301

Pipe Diameter  $d = 24$   
Pipe Slope  $s = 1.56 \%$   
Manning's number  $n = 0.013$   
Flow  $Q = 12.59 \text{ cfs}$   
Velocity  $V = 8.68 \text{ ft/s}$

Dissipator Dimensions \* Zone = **2**  
Stone Filling Class = **B**  
Entry Width (  $3 \times D_0$  ) = **6.0 ft**  
Length (  $6 \times D_0$  ) = **12.0 ft**  
Width (  $L_a + D_0$  ) = **14.0 ft**  
Min. Thickness = **22 inches**  
Min. Stone Diameter= **6 inches**



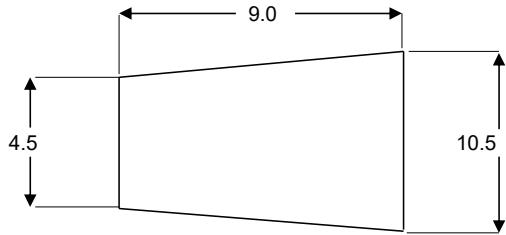
\* All units are in feet

\*\* Dissipator pad designed for full flow of pipe

FES #210

Pipe Diameter	d=	18 in
Pipe Slope	s=	4.36 %
Manning's number	n=	0.013
Flow	Q=	16.81 cfs
Velocity	V =	13.67 ft/s

Dissipator Dimensions *	Zone =	2
Stone Filling Class =	B	
Entry Width ( $3 \times D_0$ ) =	4.5 ft	
Length ( $6 \times D_0$ ) =	9.0 ft	
Width ( $L_a + D_0$ ) =	10.5 ft	
Min. Thickness =	22 inches	
Min. Stone Diameter=	6 inches	



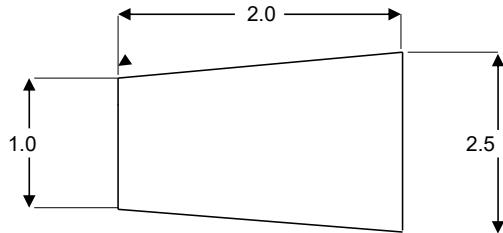
\* All units are in feet

\*\* Dissipator pad designed for full flow of pipe

FES #302

Pipe Diameter	d=	6 in
Pipe Slope	s=	3.03 %
Manning's number	n=	0.013
Flow	Q=	0.10 cfs
Velocity	V =	3.20 ft/s

Dissipator Dimensions *	Zone =	1
	A	
Stone Filling Class =		
Entry Width ( $2 \times A_0$ ) =	1.0 ft	
Length ( $4 \times A_0$ ) =	2.0 ft	
Width ( $L_a + A_0$ ) =	2.5 ft	
Min. Thickness =	12 inches	
Min. Stone Diameter=	3 inches	



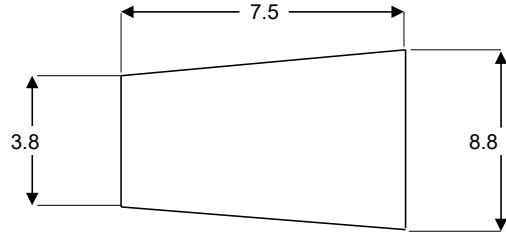
\* All units are in feet

\*\* Dissipator pad designed for full flow of pipe

FES #102

Pipe Diameter	d=	15 in
Pipe Slope	s=	1.43 %
Manning's number	n=	0.013
Flow	Q=	5.92 cfs
Velocity	V =	6.93 ft/s

Dissipator Dimensions *	Zone =	2
	B	
Stone Filling Class =		
Entry Width ( $3 \times A_0$ ) =		3.8 ft
Length ( $6 \times A_0$ ) =		7.5 ft
Width ( $L_a + A_0$ ) =		8.8 ft
Min. Thickness =		22 inches
Min. Stone Diameter=		6 inches

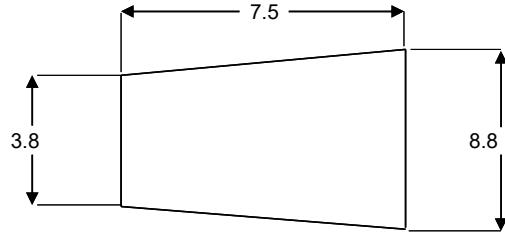


\* All units are in feet  
\*\* Dissipator pad designed for full flow of pipe

FES #401

Pipe Diameter	d=	15 in
Pipe Slope	s=	0.58 %
Manning's number	n=	0.013
Flow	Q=	2.76 cfs
Velocity	V =	4.11 ft/s

Dissipator Dimensions *	Zone =	2
	Stone Filling Class =	B
Entry Width ( $3 \times A_0$ ) =		3.8 ft
Length ( $6 \times A_0$ ) =		7.5 ft
Width ( $L_a + A_0$ ) =		8.8 ft
Min. Thickness =		22 inches
Min. Stone Diameter=		6 inches



\* All units are in feet  
\*\* Dissipator pad designed for full flow of pipe

## EROSION CONTROL CALCS (SKIMMER BASINS)

### Project Information

Project Name: Tractor Supply - Zebulon  
 Project #: 220127-01  
 Designed by: CB Date: 2/1/2023  
 Revised by: \_\_\_\_\_ Date: \_\_\_\_\_  
 Checked by: \_\_\_\_\_ Date: \_\_\_\_\_

### Skimmer Basin #1

Drainage Area

Total,  $A_T$ = **4.00** Ac  
Disturbed,  $A_D$ = **4.00** Ac

10-year Runoff (Q10)

$C$  = **0.50**  
 $T_c$  = **5.00** min  
 $I_{10}$  = **7.22** in/hr  
 $Q_{10}$  = **14.4 cfs**

Surface Area Required

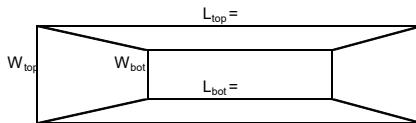
$SA = 435\text{sf} \times Q_{10}$   
**SA = 6,281 sf**

Volume Required

$V_R = 1800 \text{ cf/Ac} \times A_D$   
 **$V_R = 7,200 \text{ cf}$**

Sediment Trap Dimensions

$L$  = **114** ft (Spillway Length)  
 $W$  = **56** ft (Spillway Width)  
 $D$  = **2.0** ft (Depth of Storage)  
Side Slopes = **2.0 :1**  
 $L_{top} = 122$  ft  
 $L_{bot} = 106$  ft  
 $W_{top} = 64$  ft  
 $W_{bot} = 48$  ft



L/W Ratio= **2.0 :1** (must be 2:1 to 6:1)

Elevations

	<u>Description</u>	<u>Elevation</u>	
	Top of Berm	284.00	(allow 1ft freeboard above spillway flow height)
	Emergency Spillway	282.50	
	Sediment Storage	<b>282.00</b>	
	Cleanout Mark	281.00	(half of storage height)
	Bottom	<b>280.00</b>	

Provided

$SA_p = 6,384 \text{ sf}$  > **6,281**  
 $V_p = 11,472.0 \text{ cf}$  > **7,200**

Emergency Spillway - 10 Year Storm

$I_{10}$  = **7.22** in/hr  
 $Q_{10}$  = **14.44 cfs**  
 $h$  = **0.5** ft  
 $C_w$  = **3**  
 $L_w$  = **14** ft

<b>Calculate Skimmer Size</b>		
<b>Basin Volume in Cubic Feet</b>	11,472 Cu.Ft	<b>Skimmer Size</b>
<b>Days to Drain*</b>	3 Days	2.5 Inch
		Orifice Radius 1.0 Inch[es]
		Orifice Diameter 2.0 Inch[es]

\*In NC assume 3 days to drain

<b>Estimate Volume of Basin</b>	<b>Length</b>	<b>Width</b>	<b>VOLUME</b>	<b>11472 Cu. Ft.</b>
<b>Top of water surface in feet</b>	114	56	Feet	
<b>Bottom dimensions in feet</b>	106	48	Feet	
<b>Depth in feet</b>	2		Feet	

## EROSION CONTROL CALCS (SKIMMER BASINS)

### Project Information

Project Name: Tractor Supply - Zebulon  
 Project #: 220127-01  
 Designed by: CB Date: 1/6/2023  
 Revised by: \_\_\_\_\_ Date: \_\_\_\_\_  
 Checked by: \_\_\_\_\_ Date: \_\_\_\_\_

### Skimmer Basin #2

Drainage Area

Total,  $A_T$ = **2.36** Ac  
Disturbed,  $A_D$ = **2.36** Ac

10-year Runoff (Q10)

$C$  = **0.50**  
 $T_c$  = **5.00** min  
 $I_{10}$  = **7.22** in/hr  
 $Q_{10}$  = **8.5 cfs**

Surface Area Required

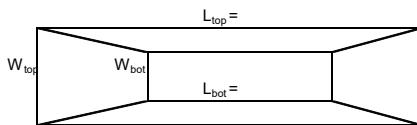
$SA = 435\text{sf} \times Q_{10}$   
**SA = 3,706 sf**

Volume Required

$V_R = 1800 \text{ cf/Ac} \times A_D$   
 **$V_R = 4,248 \text{ cf}$**

Sediment Trap Dimensions

$L$  = **95** ft (Spillway Length)  
 $W$  = **40** ft (Spillway Width)  
 $D$  = **2.0** ft (Depth of Storage)  
Side Slopes = **2 : 1**  
 $L_{top} = 103 \text{ ft}$   
 $L_{bot} = 87 \text{ ft}$   
 $W_{top} = 48 \text{ ft}$   
 $W_{bot} = 32 \text{ ft}$



L/W Ratio= **2.4 : 1** (must be 2:1 to 6:1)

Elevations

	<u>Description</u>	<u>Elevation</u>	
	Top of Berm	289.00	(allow 1ft freeboard above spillway flow height)
	Emergency Spillway	287.50	
	Sediment Storage	<b>287.00</b>	
	Cleanout Mark	286.00	(half of storage height)
	Bottom	<b>285.00</b>	

Provided

$SA_p = 3,800 \text{ sf}$  > **3,706**  
 $V_p = 6,584.0 \text{ cf}$  > **4,248**

Emergency Spillway - 10 Year Storm

$I_{10}$  = **8.06** in/hr  
 $Q_{10}$  = **9.51 cfs**  
 $h$  = **0.5** ft  
 $C_w$  = **3**  
 $L_w$  = **10 ft**

**Calculate Skimmer Size****Basin Volume in Cubic Feet**

6,584	Cu.Ft
3	Days

**Days to Drain\*****Skimmer Size**

2.0 Inch

Orifice Radius

0.8 Inch[es]

Orifice Diameter

1.6 Inch[es]

\*In NC assume 3 days to drain

**Estimate Volume of Basin****Top of water surface in feet**

95	40	Feet
87	32	Feet
2		Feet

**Bottom dimensions in feet****VOLUME**

6584 Cu. Ft.

**Depth in feet**

## EROSION CONTROL CALCS (SKIMMER BASINS)

### Project Information

Project Name: Tractor Supply - Zebulon  
Project #: 220127-01  
Designed by: CB Date: 8/10/2022  
Revised by: \_\_\_\_\_ Date: \_\_\_\_\_  
Checked by: \_\_\_\_\_ Date: \_\_\_\_\_

### Anti-Flotation Device #1

4' x 4' Outlet Structure

Area:	<u>16.0</u>	sf
Top of Basin Elev.:	<u>282.0</u>	
Bottom of Basin Elev.:	<u>280.0</u>	
Volume:	<u>32.0</u>	cf
Weight:	<u>1997</u>	lbs
Factor of Safety	<u>1.20</u>	
WT Req'd of Anti-Flotation Device:	<u>2,396</u>	lbs
Volume of Concrete Req'd:	<u>16.0</u>	cf
Volume Provided:	<u>69.5</u>	cf

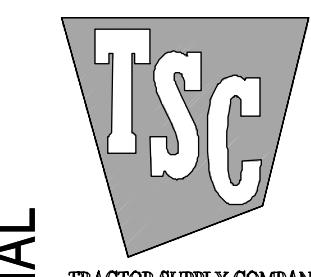
(Water Displaced - Top of Pond to Bottom of Pond)  
(Unit WT of Concrete = 150 pcf)  
(4'x4' riser x 2.0' = 32cf, 5'x5' footing x 1.5' =37.5cf)

### Anti-Flotation Device #2

4' x 4' Outlet Structure

Area:	<u>16.0</u>	sf
Top of Basin Elev.:	<u>287.0</u>	
Bottom of Basin Elev.:	<u>285.0</u>	
Volume:	<u>32.0</u>	cf
Weight:	<u>1997</u>	lbs
Factor of Safety	<u>1.20</u>	
WT Req'd of Anti-Flotation Device:	<u>2,396</u>	lbs
Volume of Concrete Req'd:	<u>16.0</u>	cf
Volume Provided:	<u>69.5</u>	cf

(Water Displaced - Top of Pond to Bottom of Pond)  
(Unit WT of Concrete = 150 pcf)  
(4'x4' riser x 2.0' = 32cf, 5'x5' footing x 1.5' =37.5cf)



EROSION CONTROL PLAN - INITIAL  
Tractor Supply  
Old US Highway 264  
Zebulon, NC Wake County



PLAN STATUS		
1/10/23	1ST CD SUBMISSION	
2/20/23	2ND CD SUBMISSION	

DATE	DESCRIPTION
MEL DESIGN	MEL DRAWN XXX CHKD

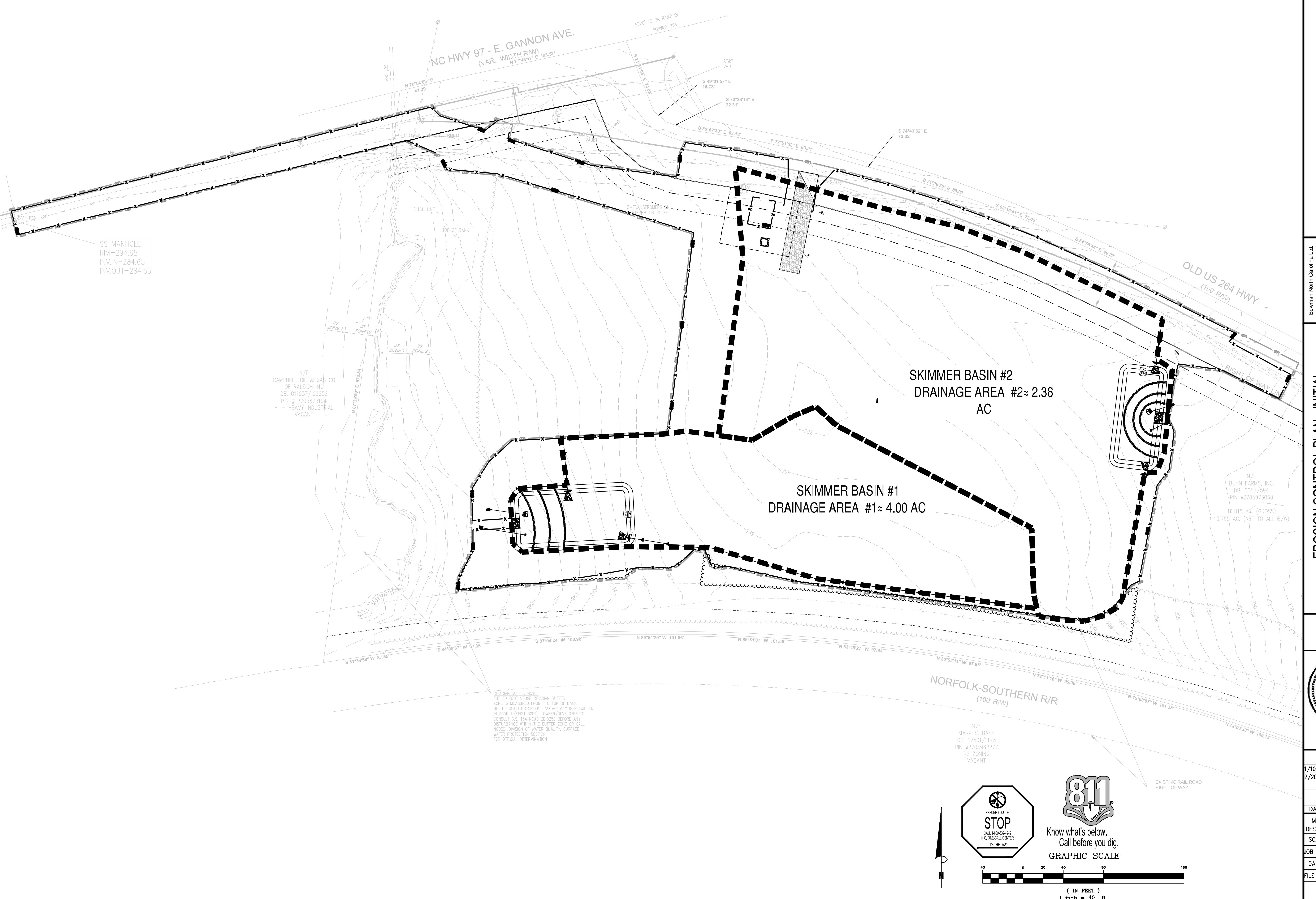
SCALE H: 1" = 40'  
V: 1" = 40'

JOB No. 220127-01-001

DATE January 10, 2023

FILE No. 220127-D-CP-001

C2.1



## **EROSION CONTROL CALCS (TEMPORARY DITCH #1)**

## **Project Information**

Project Name: Tractor Supply - Zebulon  
Project #: 220127-01  
Designed by: CB Date: 1/6/2023  
Revised by: \_\_\_\_\_ Date: \_\_\_\_\_  
Checked by: \_\_\_\_\_ Date: \_\_\_\_\_

## Temporary Ditch #1

Drainage Area                      Total,  $A_T$  =              0.21 Ac

10-year Runoff ( $Q_{10}$ )	$C =$	0.50
	$T_c =$	5.00 min
	$I_{10} =$	7.22 in/hr
	$Q_{10} =$	0.8 cfs

## Temporary Ditch #2

Drainage Area                  Total,  $A_T$  =                  0.96 Ac

10-year Runoff ( $Q_{10}$ )	$C =$	0.50
	$T_c =$	5.00 min
	$I_{10} =$	7.22 in/hr
	$Q_{10} =$	3.5 cfs

## Temporary Ditch #3

Drainage Area                  Total,  $A_T$  =                  0.27 Ac

10-year Runoff ( $Q_{10}$ )	$C =$	0.50
	$T_c =$	5.00 min
	$I_{10} =$	7.22 in/hr
	$Q_{10} =$	1.0 cfs

## Temporary Ditch #4

Drainage Area                  Total,  $A_T$  =                  0.04 Ac

10-year Runoff ( $Q_{10}$ )	$C =$	0.50
	$T_c =$	5.00 min
	$I_{10} =$	7.22 in/hr
	$Q_{10} =$	0.1 cfs



North American Green  
 5401 St. Wendel-Cynthiana Rd.  
 Poseyville, Indiana 47633  
 Tel. 800.772.2040  
 >Fax 812.867.0247  
[www.nagreen.com](http://www.nagreen.com)  
 ECMDS v7.0

## CHANNEL ANALYSIS

> > Temporary Ditch 1

Name	Temporary Ditch 1
Discharge	0.8
Channel Slope	0.0154
Channel Bottom Width	1
Left Side Slope	2
Right Side Slope	2
Low Flow Liner	
Retardence Class	C 6-12 in
Vegetation Type	None
Vegetation Density	None
Soil Type	None

## DS75

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor	Remarks	Staple Pattern
DS75 Unvegetated	Straight	0.8 cfs	1.71 ft/s	0.29 ft	0.037	1.6 lbs/ft <sup>2</sup>	0.28 lbs/ft <sup>2</sup>	5.65	STABLE	D
Underlying Substrate	Straight	0.8 cfs	1.71 ft/s	0.29 ft	0.037	0.37 lbs/ft <sup>2</sup>	0.19 lbs/ft <sup>2</sup>	1.91	STABLE	D



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## CHANNEL ANALYSIS

> > Temporary Ditch 2

Name	Temporary Ditch 2
Discharge	3.5
Channel Slope	0.0161
Channel Bottom Width	1
Left Side Slope	2
Right Side Slope	2
Low Flow Liner	
Retardence Class	C 6-12 in
Vegetation Type	None
Vegetation Density	None
Soil Type	None

## DS75

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor	Remarks	Staple Pattern
DS75 Unvegetated	Straight	3.5 cfs	2.73 ft/s	0.59 ft	0.034	1.6 lbs/ft <sup>2</sup>	0.59 lbs/ft <sup>2</sup>	2.71	STABLE	D
Underlying Substrate	Straight	3.5 cfs	2.73 ft/s	0.59 ft	0.034	0.37 lbs/ft <sup>2</sup>	0.35 lbs/ft <sup>2</sup>	1.05	STABLE	D



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## CHANNEL ANALYSIS

> > Temporary Ditch 3

Name	Temporary Ditch 3
Discharge	1
Channel Slope	0.0038
Channel Bottom Width	1
Left Side Slope	2
Right Side Slope	2
Low Flow Liner	
Retardence Class	C 6-12 in
Vegetation Type	None
Vegetation Density	None
Soil Type	None

## DS75

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor	Remarks	Staple Pattern
DS75 Unvegetated	Straight	1 cfs	0.99 ft/s	0.5 ft	0.042	1.6 lbs/ft <sup>2</sup>	0.12 lbs/ft <sup>2</sup>	13.42	STABLE	D
Underlying Substrate	Straight	1 cfs	0.99 ft/s	0.5 ft	0.042	0.37 lbs/ft <sup>2</sup>	0.07 lbs/ft <sup>2</sup>	5.06	STABLE	D



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## CHANNEL ANALYSIS

> > Temporary Ditch #4

Name	Temporary Ditch #4
Discharge	0.1
Channel Slope	0.0213
Channel Bottom Width	1
Left Side Slope	2
Right Side Slope	2
Low Flow Liner	
Retardence Class	C 6-12 in
Vegetation Type	None
Vegetation Density	None
Soil Type	None

## DS75

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor	Remarks	Staple Pattern
DS75 Unvegetated	Straight	0.1 cfs	0.95 ft/s	0.09 ft	0.041	1.6 lbs/ft <sup>2</sup>	0.12 lbs/ft <sup>2</sup>	13.58	STABLE	D
Underlying Substrate	Straight	0.1 cfs	0.95 ft/s	0.09 ft	0.041	0.37 lbs/ft <sup>2</sup>	0.1 lbs/ft <sup>2</sup>	3.75	STABLE	D